





US Army Corps of Engineers

Buffalo District

REMEDIAL INVESTIGATION, FEASIBILITY STUDY, & PROPOSED PLAN

FOR THE BLISS & LAUGHLIN SITE

BUFFALO, NEW YORK

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TABLE OF CONTENTS

REMEDIAL INVESTIGATION, FEASIBILITY STUDY, AND PROPOSED PLAN FOR THE BLISS & LAUGHLIN SITE	1
1. INTRODUCTION	3
1.1 OVERVIEW OF FUSKAF	
1.3 PURPOSE	4
2. SITE CHARACTERIZATION RESULTS	5
2.1 SURVEY AND SAMPLING ACTIVITIES	3
3. IDENTIFYING AND EVALUATING CLEANUP OPTIONS	9
$\sim 10^{-10}$	
a de la 11 11 au Delevient and Appropriate Reconficille (AlVAIVA)	/
- 4 4 O.1 D	
3.3 DESCRIPTION OF ALTERNATIVES 3.3.1 Alternative 1: No Action	11
3.3.2 Alternative 2: Continued institutional Controls	11
4. EVALUATION OF ALTERNATIVES	14
4.2 EVALUATION OF ALTERNATIVES 4.2.1 Overall Protection of Human Health and the Environment 4.2.2 Compliance with Federal and State Environmental Regulations 4.2.3 Compliance with Federal and State Environmental Regulations	
1 Cl Uthank Littactiveness will Echicalical to 1 1 1 1 1 1 1 1	
T_{-}	
4.2.6 Cost	20
5. SELECTION OF THE PREFERRED ALTERNATIVE	, ,
6. COMMUNITY ROLE IN THE SELECTION PROCESS	22
6. COMMUNITY ROLE IN THE BEEDE TOTAL	23
7. REFERENCES	23
Appendix A BLISS AND LAUGHLIN STEEL CHARACTERIZATION RESULTS	. A- 3
Appendix B COST ESTIMATE	B-1
Annendix B COST ESTIMATE	

LIST OF FIGURES

Figure	Page
 Bliss and Laughlin Steel with Reference Grids and Survey Locations	7
LIST OF TABLES	
Table	Page
1. Summary of CERCLA Evaluation Criteria	15

ACRONYMS AND ABBREVIATIONS

Atomic Energy Commission AEC

As Low As Reasonably Achievable ALARA

Applicable or Relevant and Appropriate Requirements ARAR

Bechtel National, Incorporated **BNI**

Comprehensive Environmental Response, Compensation, and Liability Act **CERCLA**

Code of Federal Regulations **CFR**

square centimeter(s) cm^2

Contaminant(s) of Concern COC

cubic yards су

Department of Energy DOE

Department of Transportation DOT disintegrations per minute dpm

Engineering Evaluation/Cost Analysis EE/CA **Environmental Protection Agency EPA**

Formerly Utilized Sites Remedial Action Program **FUSRAP**

gram(s) g hour hr

kilometer(s) km

Lake Ontario Ordnance Work LOOW

micro Roentgen(s) μR

meter(s) m

Manhattan Engineer District **MED**

millirem mrem

Nuclear Regulatory Commission **NRC**

New York Codes, Rules, and Regulations **NYCRR** New York State Department of Environmental Conservation NYSDEC

Oak Ridge Institute for Science and Education ORISE

Oak Ridge National Laboratory ORNL

Office of Solid Waste and Emergency Response **OSWER**

picoCuries pCi radium Ra

Resource Conservation and Recovery Act **RCRA**

Remedial Investigation RI

Science Applications International Corporation SAIC Technical Administrative Guidance Memorandum TAGM

To Be Considered TBC

Toxicity Characteristic Leaching Procedure TCLP

Total Effective Dose Equivalent **TEDE**

thorium Th uranium U

United States Army Corps of Engineers USACE

United States Environmental Protection Agency **USEPA**

UNITED STATES ARMY CORPS OF ENGINEERS REMEDIAL INVESTIGATION, FEASIBILITY STUDY, AND PROPOSED PLAN FOR THE BLISS & LAUGHLIN SITE BUFFALO, NEW YORK

The United States Army Corps of Engineers (USACE) is conducting the project at the Bliss & Laughlin Site in Buffalo, New York in accordance with the Comprehensive Environmental Response, Compensation, and Liability Act, 42 United States Code 9601et seq. (CERCLA).

On October 13, 1997, the Energy and Water Development Appropriations Act, 1998 was signed into law as Public Law 105-62. Pursuant to this law, the Formerly Utilized Sites Remedial Action Program (FUSRAP) was transferred from the U.S. Department of Energy to the USACE. Under its authority to conduct the Formerly Utilized Sites Remediation Program, the USACE prepared this Remedial Investigation, Feasibility Study, and Proposed Plan for the Bliss & Laughlin Site. The Remedial Investigation, Feasibility Study, and Proposed Plan addresses contamination resulting from operations conducted for the Atomic Energy Commission (AEC). Bliss & Laughlin Steel Company performed machining and straightening operations on uranium rods. The machined rods and turnings were then shipped off-site.

Three alternatives were considered for addressing residual radioactive contamination at the Bliss and Laughlin site. The first Alternative, No Action, assumes the site is abandoned and current institutional controls to limit exposure are lifted. The second alternative, Continuation of Institutional Controls, includes no remediation but continues the use of the site as an industrial facility with periodic monitoring and review. The third, Decontamination of Buildings, would use various decommissioning technologies to remove contamination from the surfaces inside of the buildings to preclude human exposure in areas of elevated radioactivity. Building rubble that exceeded the release criteria would be shipped to an appropriate licensed or permitted disposal facility. Material that does not exceed the release criteria would be left on site or sent to an appropriate disposal facility.

USACE does hereby propose that the final remedial action for the Bliss & Laughlin Site be Alternative 3, Decontamination of Buildings. The alternative is fully protective of human health and the environment, complies with the applicable or relevant and appropriate requirements, and is considered by the USACE to best meet the criteria prescribed by CERCLA, as amended, and the National Contingency Plan (NCP).

USACE invites members of the public to review the proposed plan and the supporting documents which further describe the conditions at the Bliss & Laughlin Site and the basis for the proposal. Those documents may be found in the administrative record for the Bliss & Laughlin Site at the Buffalo and Erie County Public Library-Dudley Branch, 2010 South Park Avenue, Buffalo, New York, 14220, and at the USACE FUSRAP Public Information Center, 1776 Niagara Street, Buffalo, NY, 14207. Members of the public who wish to comment upon this proposed plan may submit their comments to USACE at the following address:

U.S. Army Corps of Engineers Buffalo District FUSRAP Public Information Center 1776 Niagara Street Buffalo, NY 14207-3199

Please refer to this proposed plan or to the Bliss & Laughlin Site in the comments. All comments will be reviewed and considered by USACE in determining the final remedy for the Bliss & Laughlin Site. Comments should be submitted no later than 30 days after the date of this proposed plan.

After the close of the comment period, USACE will review all public comments, as well as the information contained in the Administrative Record file for this site, and any new information developed or received during the course of this comment period, in light of the requirements of CERCLA and the NCP. An authorized official of USACE will then make a final selection of the remedial action to be conducted at this site. This decision will be documented in a Record of Decision, which will be issued to the public, along with a response to all comments submitted regarding this proposed plan.

1. INTRODUCTION

1.1 OVERVIEW OF FUSRAP

This document describes the results of testing and analysis performed and cleanup options for the Bliss & Laughlin site. The site is being addressed under the United States Army Corps of Engineers (USACE) Formerly Utilized Sites Remedial Action Program (FUSRAP). The U.S. Atomic Energy Commission (AEC), a predecessor of the Department of Energy (DOE), established FUSRAP in 1974 to identify, investigate, and remediate or control sites contaminated as a result of activities performed as part of the nation's early atomic energy program. On October 13, 1997, the Energy and Water Development Appropriations Act was signed into law, transferring the responsibility for the administration and execution of FUSRAP from the DOE to the United States Army Corps of Engineers (USACE).

1.2 BACKGROUND

Bliss & Laughlin is located at 110 Hopkins Street, Buffalo, New York. The site consists of a single large building. In 1952, Bliss & Laughlin Steel Company performed machining and straightening operations on uranium rods for National Lead Company of Ohio, a prime contractor for Atomic Energy Commission (AEC). Uranium rods were shipped from Lake Ontario Ordnance Works (LOOW) to Bliss & Laughlin for machining. Bliss & Laughlin shipped the machined rods directly to Fernald, Ohio, and the turnings from the operations were returned to LOOW for packaging and subsequent shipment to Fernald. In 1972, Ramco Steel, Inc., purchased Bliss & Laughlin Steel Company. Currently, Niagara Cold Drawn Corporation owns and operates the facility.

Based on the nature of operations performed at Bliss & Laughlin, the primary radiological constituent of concern for the site is uranium from the metal rods. Eighteen samples were analyzed to determine the relative abundance of radioisotopes. All samples showed ratios among the uranium isotopes that were similar to natural uranium.

1.3 PURPOSE

The purpose of this Remedial Investigation, Feasibility Study, and Proposed Plan is to document the assessment of the environmental impacts for various actions at the Bliss and Laughlin site in Buffalo, New York. This documentation is required by the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA) as a vehicle to inform the public of intended cleanup actions and solicit public input into cleanup decisions. Because this is a small site with only a small amount of contaminated materials the documentation for the cleanup is being combined into a single short document which describes the results of the investigation, the identification and evaluation of alternatives, and the plan proposed by the USACE. Characterization results are described in Appendix A of this report and in the administrative record described in Section 6 of this report.

1.4 SITE DESCRIPTION AND SETTING

Historical records indicate that machining operations were performed in a section of the building called the "Special Finishing Area," which occupies approximately 3,230 square ft of floor space. The floor of the "Special Finishing Area" is concrete and contains several shallow utility trenches. There are no floor drains. The floor surfaces are generally rough and pitted and are covered with a thin layer of oil absorbent material and dried oil and grease. Machining equipment and material storage racks prevent access to some floor areas. The ceiling is approximately 37 feet high and is supported by a framework of steel trusses. The machining area of the building does not have any partition or interior walls. The site is currently used for the forming of steel products and is an active industrial site with equipment such as rolling mills and lots of machine oil.

2. SITE CHARACTERIZATION RESULTS

2.1 SURVEY AND SAMPLING ACTIVITIES

The results of the radiological and chemical characterization of the Bliss & Laughlin site are described in a 1995 Technical Memorandum (BNI, 1995). Historically, the facility was the site of uranium metal machining. Therefore, the primary radiological constituent of concern is uranium including the radioactive decay products. The site was assigned to FUSRAP based upon a designation survey preformed by the Oak Ridge Institute for Science and Education (ORISE). Using the data reported by ORISE, a survey of the floor area and the overheads in the vicinity of the Special Finishing Area was conducted, and a less intensive survey was performed throughout the rest of the building, with emphasis on areas adjacent to the Special Finishing Area, high traffic areas, and likely areas of material transfer such as locker rooms. Six core samples were drilled through the slab in areas where the potential for constituent migration was the greatest. Additional samples were taken from the dust on overhead beams and material on the floor. One composite sample of floor material was collected and analyzed for Toxicity Characteristic Leaching Procedure (TCLP) characteristics, which included metals, volatile organics, semi-volatile organics, pesticides and herbicides. Some areas were identified that have radioactive material that could result in exposure to radioactivity that exceeds the applicable or relevant and appropriate requirements (ARARs) which are described in the next section.

2.2 SURVEY RESULTS

Several areas on the floor and on the rafters were identified where radioactivity exceeds the ARARs described in Section 3.1. Some areas of a filled in trench are suspect and will require further characterization as part of the remediation activities. The characterization tried to identify areas significantly different from background levels and compared the results with criteria in the DOE Orders. The results are shown in Figures 1, 2, and 3 which are reproduced from the Technical Memorandum (BNI, 1995) and summarized below. A copy of this Technical Memorandum (BNI, 1995) is included in Appendix A.

- Two locations out of 45 surveyed on the overheads above the special finishing area were above 5000 dpm/100 sq cm beta/gamma. The highest reading of those two locations was 6318 dpm/100 sq cm beta/gamma.
- The surface contamination on the floor in the special finishing area is limited to approximately 19 meters by nine meters of floor, some of it obstructed by machinery. Ten locations exceeded 15,000 dpm/100 sq cm direct beta/gamma with a range from 17,000 to 280,000 dpm/100 sq cm.
- No subsurface soil samples showed evidence of contamination. One sample from a core taken through a filled-in trench showed elevated uranium levels. This material appears to be limited to debris deposited in the trench prior to sealing with concrete. The soil collected below this material was not above criteria.
- The remainder of the building was surveyed as extensively as building conditions allowed, and showed no evidence of additional contaminated areas.
- A composite TCLP sample from the floor in the Special Finishing Area showed no RCRA hazardous constituents.

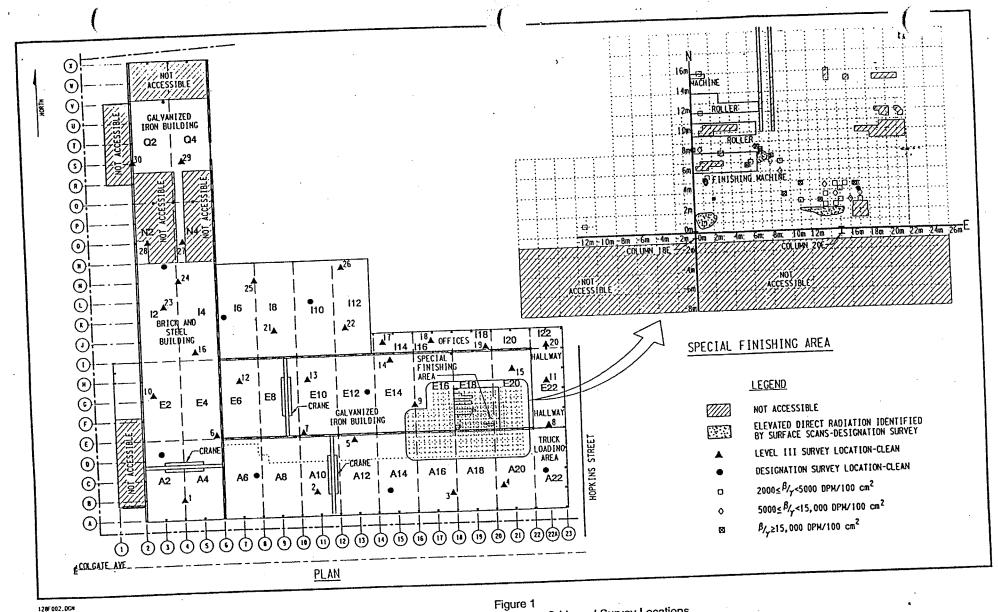
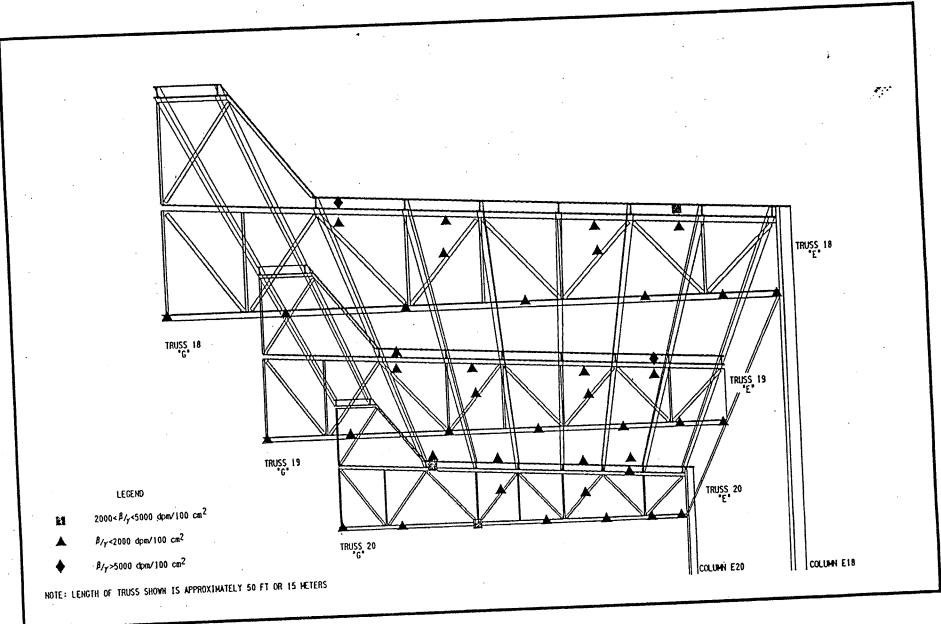
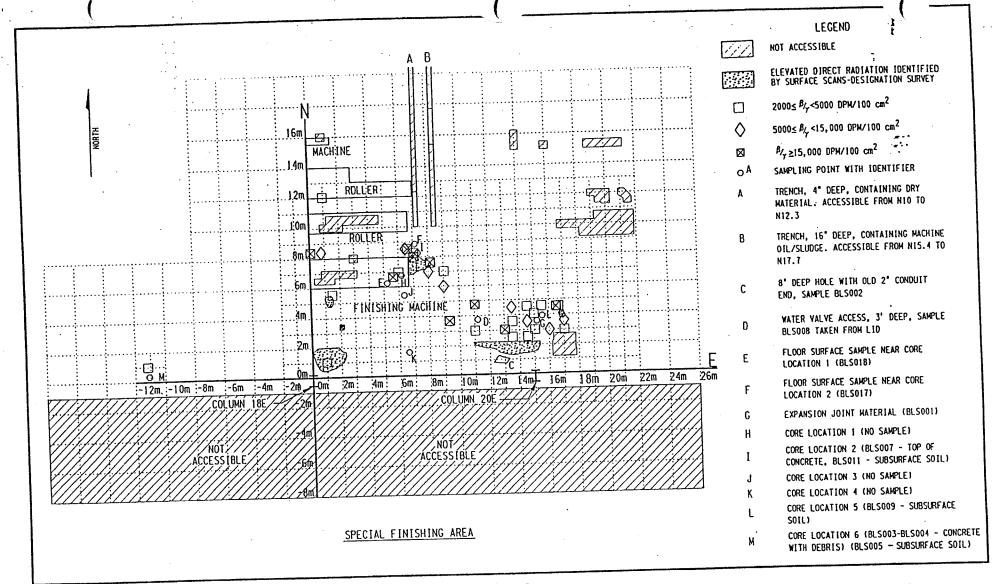


Figure 1
Bliss and Laughlin Steel with Reference Grids and Survey Locations



128F004.DGN

Figure 2
Overheads Above Special Finishing Area
with Survey Locations



1281003.0CM

Figure 3
Detail of Special Finishing Area with
Survey Results and Sampling Locations

3. IDENTIFYING AND EVALUATING CLEANUP OPTIONS

Three alternatives were considered. The first, No Action, is required by CERCLA to establish a baseline for comparison to the other alternatives. The second alternative is Continued Use of Institutional Controls. The third alternative is Decontamination of Buildings. This section describes the ARARs and TBCs, describes the alternatives in detail, and evaluates the alternatives for effectiveness, implementability, and cost.

3.1 DESCRIPTION OF ARARs AND TBCs.

3.1.1 Authority

Authority for responding to releases or threats of release from an impacted site is provided by Section 104 of CERCLA. In 1997, Congress authorized the USACE to manage FUSRAP. This includes authorization to undertake such investigation, surveys, testing, or other data gathering deemed necessary to identify the existence, extent, and nature of contaminants of concern (COC) present at the Bliss and Laughlin site including the extent of threats to human health and the environment. In addition, USACE is authorized to undertake planning, engineering, and other studies and investigations appropriate to direct response actions to prevent, limit, or mitigate potential risks associated with this site.

3.1.2 Applicable or Relevant and Appropriate Requirements (ARARs)

Applicable requirements are those cleanup standards, standards of control, and other substantive environmental protection requirements, criteria, or limitations promulgated under federal environmental or state environmental or facility siting laws that specifically address a hazardous substance, pollutant, contaminant, remedial action, location or other circumstance at a CERCLA site. An applicable requirement directly and fully addresses an element of the remedial action.

Relevant and appropriate requirements are those cleanup standards, standards of control, and other substantive environmental protection requirements, criteria or limitations promulgated under federal environmental or state environmental or facility siting laws that while not "applicable" to a hazardous substance, pollutant, contaminant, remedial action, location or other circumstance at a CERCLA site, address problems or situations sufficiently similar to those encountered at the CERCLA site that their use is suited to the particular site.

Only those state standards that are promulgated, are identified by the state in a timely manner, and are more stringent that federal requirements may be applicable or relevant and appropriate.

USACE has determined that the following regulation is an ARAR, as that term is defined in CERCLA.

Subpart E of 10 CFR 20 is considered relevant and appropriate to the removal action. This CFR provides standards for determining the extent to which sites must be remediated before decommissioning of a site can be considered complete and the license terminated. The standards for human exposure for both unrestricted use (workers and members of the public) and for restricted use with institutional controls are: 25 mrem/yr total effective dose equivalent (TEDE) and as low as reasonably achievable (ALARA). The amount (or concentration) of radioactive materials which would result in this dose depends on the future land use and exposure scenario. This requirement would be applicable if the uranium machining was done commercially with a license issued by the NRC. For the Bliss and Laughlin site, a license was not required because the work was done for the government. Therefore, the standards in Subpart E of 10 CFR 20 are considered relevant and appropriate to the removal action because the activities and contaminants are similar to those which require a license under 10 CFR 40 from the Nuclear Regulatory Commission or an agreement state and therefore subject to the license termination criteria in 10 CFR Part 20. The proposed approach to meet the 25 mrem/yr total effective dose equivalent and as low as reasonably achievable standard for unrestricted future use is described in section 3.3.3.

Standards for the tailings from uranium mills in 40 CFR 192 were considered, but are not considered ARARs because the contaminant at the Bliss & Laughlin site is uranium from the machining of uranium metal and is not similar to the mill tailings which contain large quantities of radium and other materials.

3.1.3 To be Considered (TBCs)

To-be-Considered (TBCs) are non-promulgated advisories, criteria, or guidance issued by a federal or state government that may be useful in developing CERCLA remedies that are not legally binding and do not have the status of potential ARARs. Because an ARAR has been identified, no TBCs are designated for this action.

3.1.4 Other Requirements

While not ARARS or TBCs, other environmental, safety, and occupational health standards will be followed when implementing this removal action. Examples include Occupational Safety and Health Administration Standards, and Resource Conservation and Recovery Act (RCRA) Land Disposal Restrictions.

3.2 SUMMARY OF SITE RISKS

The contamination at the Bliss & Laughlin Site could result in adverse health effects if the building is used without restrictions to minimize exposures. The levels of contamination at the Bliss & Laughlin site are high enough to exceed the 25 mrem/yr standard in the ARAR for a typical building occupancy scenario. Therefore, scenarios are possible where individuals could be exposed to this material for extended periods of time resulting in an unacceptable risk. If the institutional controls were not continued, there would be no restrictions on the uses that could be made of the buildings and the materials in the buildings and scenarios resulting in higher doses would be possible.

As long as the use of the property is used as an industrial facility and provisions are made for periodic monitoring and reviews, the potential for adverse health effects would be mitigated. The typical scenarios for building occupancy used by the Nuclear Regulatory Commission result in the primary exposure path being inhalation with ingestion being a significant pathway. At the Bliss & Laughlin Site, the potential for exposure through these pathways is greatly reduced because of the large amount of oil and oil adsorbent used in the steel processing. Without remediation, scenarios are possible where the risk of cancer could exceed the risk range, i.e., be larger than 1 chance in 10,000. Again, inhalation is a possible pathway of concern even though current building use limits exposures via this pathway. Without remediation, the dose via the inhalation pathway could be as much as 100 mrem/yr or more. With remediation, the dose would be well below the ARAR and within the CERCLA risk range.

3.3 DESCRIPTION OF ALTERNATIVES

3.3.1 Alternative 1: No Action

This alternative assumes that the facility is abandoned and institutional controls are discontinued. Under this alternative, it is assumed that there are no impediments to access. The controls would no longer exist and there would be no security guards or fences to exclude intruders. No signs warning of the hazards would be posted.

3.3.2 Alternative 2: Continued Institutional Controls

This alternative would continue the use of institutional controls at the site. These would include:

- Continued use of this site as an industrial facility,
- Maintaining signs and fencing,
- Continued maintenance and monitoring,
- Restriction of future use by acquisition of real estate interest or other means, and
- Periodic inspections by the Government to enforce any such restrictions.

The continued use of the site as an industrial facility with periodic monitoring and reviews would control the amount and duration of potential exposures. This alternative includes compliance with the controls by current and future building owners, including possible use of a restrictive covenant or other deed restriction to meet the restricted use criteria in the ARARs.

3.3.3 Alternative 3: Decontamination of Buildings.

Under this alternative the contamination on the floors, walls, and overhead appurtenances will be removed using appropriate decontamination technologies to a level sufficient to meet the ARAR. The technologies that may be employed include vacuuming, CO₂ blasting, soft media blasting, etc. Contamination can be removed using either aggressive (Blastrac, VacuBlast, needle

guns, scabblers, chipping hammers, etc.) or non-aggressive (absorbent cloth and vermiculite, nuclear grade vacuum cleaners, paint remover, etc.) techniques.

Dust would be controlled during the performance of decontamination activities by spraying water or using other methods. Air monitors would be installed for work area monitoring. Any water generated or collected during the performance of work would be contained, sampled, analyzed, and disposed appropriately.

A licensed/permitted disposal facility would be used. Waste packaging would be performed in accordance with all applicable federal, state, and local laws and regulations. Shipping containers shall meet Department of Transportation (DOT) requirements. Only a few shipments are anticipated because of the small volume expected. Any lead-based paint removed from the building surfaces would be stored, handled, and disposed in accordance with all applicable regulations. Surveys would be conducted to check for cross contamination and to verify that the release criteria have been met.

The USACE proposes to (1) remove contamination above the levels in Regulatory Guide 1.86, (2) for ALARA purposes, to perform an additional attempt at decontamination of areas greater than 2,000 dpm/100 cm2 (averaged over not more than 1 m2), and (3) to perform post remedial surveys and analyses to assure compliance with the ARAR. These three steps are discussed below.

The first step is to determine removals that will meet the 25 mrem/yr standard. Uranium contamination would be removed to levels that meet the ARAR for unrestricted use of 25 mrem/yr TEDE. Calculations were made to correlate the 25 mrem/yr in the ARAR with the uranium measurements at the Bliss and Laughlin facility. The standard scenarios used by the NRC for building occupancy (NUREG-1500 and NUREG-5512) show that average levels of 1500 dpm/100 cm² over large areas could result in exposures equal to the ARAR of 25 mrem/yr. For this scenario, the inhalation pathway contributes 84% of the dose. The ingestion pathway contributes 14% and the external gamma pathway contributes less than 1%. The inhalation and ingestion are likely very conservative in terms of current operations, but allow for possible changes in operations in the future. An evaluation was also made to compare the standards in Regulatory Guide 1.86 which are for much smaller areas. Decontamination to the levels in Regulatory Guide 1.86 should result in average levels in the special finishing area below the 1500 dpm/100 cm² large area average and below the 25 mrem/yr ARAR level. Regulatory Guide 1.86 recommends the following as acceptable surface contamination levels:

- 5,000 dpm/100 cm² averaged over not more than 1 m²,
- 15,000dpm/100 cm² maximum for any 100 cm² area, and
- 1,000 dpm/100 cm² removable contamination averaged over not more than 1 m².

The second step is to evaluate as low as reasonably achievable levels. The USACE proposes to conduct an additional decontamination to achieve as low as reasonably achievable levels. This additional decontamination will be done as part of the cleanup action. The cleanup team will attempt removal of contamination from areas with levels above 2,000 dpm/cm² (i.e., 2,000 dpm/cm² averaged over not more than 1 m² versus the 5,000 dpm/cm² in the Regulatory Guide). The decontamination efforts are anticipated to remove most of the contamination and result in dose levels well below the 25 mrem/yr level.

The third step is to assure compliance with the ARAR. The compliance with the ARAR will be confirmed by measurements and a final calculation using the measurements from the site after the remediation is completed. In the unlikely event that post-remediation analysis indicates the potential for exposures above the 25 mrem/yr TEDE level, additional decontamination will be performed.

4. EVALUATION OF ALTERNATIVES

4.1 EVALUATION CRITERIA

The alternatives described above were evaluated using CERCLA criteria to determine the most favorable actions for cleanup of the Bliss & Laughlin Site. These criteria are described below. They were established to ensure that the remedy is protective of human health and the environment, meets regulatory requirements, is cost effective, and uses permanent solutions and treatment to the maximum extent practicable. The results of the evaluation of alternatives to remediate the Bliss & Laughlin Site are described below.

Table 1. Summary of CERCLA Evaluation Criteria

Overall Protection of Human Health and the Environment	addresses whether an alternative provides adequate protection and describes how risks are eliminated, reduced, or controlled through treatment, engineering controls, or institutional controls	
Compliance with Federal and State Environmental Regulations	addresses if a remedy would meet all of the ARARs of other Federal and State environmental laws	
Long-Term Effectiveness and Permanence	addresses the impacts of an alternative to protect human health and the environment over time, once the cleanup goals have been met	
Short-Term Effectiveness and Environmental Impacts	addresses the impacts to the community and site workers during cleanup including the amount of time it takes to complete the action	
Reduction in Toxicity, Mobility, or Volume through Treatment	addresses the anticipated performance of treatment tant permanently and significantly reduces toxicity, mobility, or volume of waste	
Implementability	addresses the technical and administrative feasibility of an alternative, including the availability of materials and services required for cleanup	
Cost	compares the differences in cost, including capital, operation, and maintenance costs	
State Acceptance	evaluates whether the State agrees with, opposes, or has no comment on the preferred alternative.	
Community Acceptance	addresses the issues and concerns the public may have regarding each of the alternatives	

4.2 EVALUATION OF ALTERNATIVES

4.2.1 Overall Protection of Human Health and the Environment

Potential Health Effects

Alternative 1, No Action, could result in adverse health effects if the building is used without restrictions to minimize exposures. Radioactivity exceeds the ARARs in several areas of the building. With No Action scenarios are possible where individuals could be exposed to this material for extended periods of time resulting in an unacceptable risk. Because the No Action alternative assumes no institutional controls remain in place, there would be no restrictions on the uses that could be made of the buildings and the materials in the buildings.

Alternative 2, Continued Use of Institutional Controls, would continue to control the risks by restricting the use of the property as an industrial facility and provide for periodic monitoring and reviews. As long as these controls remain effective, the potential for adverse health effects could be controlled. In a few isolated areas of the building, the potential would continue to exist for an employee to receive doses above the ARARs.

Alternative 3, Building Decontamination of Buildings, would eliminate the potential for exposure. However, the potential for exposure to workers during remedial activities increases due to the handling of the radioactive material. Remediation workers may be directly exposed to radioactive materials, and radioactive dust could become airborne, allowing it to be inhaled by workers. These effects can be mitigated, however, by requiring remediation workers to wear protective equipment and by using appropriate dust suppression measures. These techniques have been very effective in controlling the spread of radioactive materials in previous work. The USACE plans to perform the decontamination on weekends and other times that would limit the impact to workers and operations of the plant. Monitoring would also be performed inside the construction area to ensure adequate protection of the remediation workers.

Shipment of the debris to a disposal facility will entail some risk to the community due to the potential for transportation accidents. The risks are principally associated with vehicle operation and not the characteristics of the material being shipped. The risks to the community from exposure to the contaminated wastes during transport are negligible compared with the risk of traffic accidents.

Transportation risks for this removal action are due to the potential for injuries or fatalities due to truck or rail accidents. Cashwell et al. (1986) have compiled the risks per kilometer. Risks are reduced by using shorter shipping distances. Because only a small volume of material is anticipated, only a few shipments will be required for Alternative 3.

Potential Environmental Impacts

Under the No Action alternative, minor additional environmental impacts are expected due to building deterioration which may result in the uncontrolled release of radioactive material to the environment. These impacts are expected to be minor because, although surfaces in the building exceed criteria, the actual volume of radioactive materials is likely to be very low. These impacts would be controlled for the short term by using the institutional controls of Alternative 2.

Under the Building Decontamination alternative, no additional environmental impacts are expected from decontamination activity inside the building. These impacts would be reduced by employing dust control and other preventative measures during implementation.

4.2.2 Compliance with Federal and State Environmental Regulations

No Action would not comply with ARARs. Alternative 2, Continued Use of Institutional Controls, would provide compliance by continuing the industrial use of the site and providing monitoring and periodic reviews. However, the potential would continue to exist for a few workers to receive doses above the ARARs. Alternative 3, Decontamination, would be conducted in a manner that complies with ARARs. Post remedial surveys and analyses would be performed to assure compliance with the ARARs.

All alternatives would be conducted in accordance with other applicable environmental, safety, and occupational health requirements.

4.2.3 Long-Term and Short-Term Effectiveness and Permanence

Alternative 1, No Action, would not involve any reduction in the amount of radioactivity at the site. In addition, it would increase potential for human exposure or environmental release. The potential for human exposure to radiation would persist in the short and long term in Alternative 1. In the long term, and in the absence of any additional maintenance work, migration of the radioactive materials to the environment is possible because the radioactive surfaces in the building may not be adequately controlled in the future to prevent migration. Radioactive materials could eventually become airborne as dust, as the building deteriorates or in the event of a fire. The potential risk to human health from the building could also increase in the future if adequate safeguards are not maintained.

Alternative 2, Continued Institutional Controls would be effective in the short term. However, providing effective institutional controls for long periods (e.g. greater than 100 years) is difficult. Alternatives 3 would be effective in reducing short and long term health risks and would eliminate radioactive materials at the site. Alternatives 3 would comply with current ARARs. Radioactive wastes would be shipped to appropriately licensed or permitted facilities. This alternative would also eliminate the potential for migration to the environment.

4.2.4 Reduction in Toxicity, Mobility, or Volume through Treatment

None of the alternatives provides treatment on site for the materials to be removed. Materials which are removed will include treatment to meet the standards of any off-site disposal facility.

4.2.5 Implementability

All Alternatives are implementable. Although Alternative 3, Decontamination of Buildings, is technically more complex than Alternatives 1 and 2, similar projects have been successfully completed at other sites throughout the country; therefore, no technical barriers to implementation of Alternative 3 are foreseen. Radioactive wastes generated during the activities would be disposed at currently existing licensed/permitted disposal facilities. The decontamination technologies called for in Alternative 3 are readily available. These include processes such as blasting, Blastrac, needle guns scabblers, vacuums, paint remover, and cloth cleaning.

Technical Feasibility

Technical feasibility is not applicable to the No Action Alternative. For alternative 2, institutional controls are already implemented. Although no technical impediments to implementation exist, the use of the area as an industrial facility with proper health and safety programs would need to be continued.

Radiological decontamination technologies called for in Alternative 3, Decontamination of Buildings, are available. Many standard decontamination procedures exist and have been used at FUSRAP and other cleanup sites. Consideration will be given to decommissioning equipment and procedures that would reduce waste and improve worker safety. Processes such as CO₂ blasting, media blasting, Blastrac, needle guns, scabblers, vacuums, paint remover, and cloth cleaning are readily available. One complexity for alternative 3 is due to the need to work around ongoing activities. Thus, the work will likely be done on holidays or weekends.

Availability of Services and Materials

All of the services and materials required to implement Alternatives 2 and 3 are readily available. Adequate commercial disposal capacity for the radioactive waste generated is available. No services or materials are required for Alternative 1.

Administrative Feasibility

Alternative 1, No Action, would not require any permits and no activities are included for coordination. Alternative 2 continues the use of institutional controls which provides for the use of the buildings as an industrial facility.

Alternative 3, Decontamination of Buildings, would be readily implementable. Shipment of any waste generated and excavated soils would comply with any requirements for manifests, advance notification, and permitting in a timely manner.

4.2.6 Cost

Alternative 1, No Action, would have no cost. Alternative 2, Continued Institutional Controls, is estimated to cost about \$350,000 (mainly for monitoring and reviews over the next 30 years). Alternative 3, Building Decontamination, is estimated to cost approximately \$400,000 (\$350,000 to \$430,000). Costs are in 1998 dollars. Costs could vary due to uncertainty in the amount of material, the actual disposal location and transportation distances, and other factors. However, the cost estimates represent a reasonable comparison of the alternatives. The cost range for Alternative 3, Building Decontamination, reflects cleanup volumes ranging from 6 cubic yards (the current best estimate) to 20 cy. The larger volume allows for possible volume increases if material is found in the trench or other areas.

Under Alternative 1, No Action, USACE would not incur any cost for implementation. Although Alternative 2, Continued Institutional Controls, would have limited costs in addition to normal operation as an industrial facility the costs continue for a long period. The cost estimate of \$350,000 includes six 5-year reviews at about \$15,000 each; Institutional controls, surveillance and monitoring for 30 years at about \$530/month, and project management at about \$750/yr. Alternative 3 would cost approximately \$400,000. The cost for alternative 3 will vary depending on if additional contamination is found during remediation. For a cleanup volume of 6 cy (the current best estimate) the cleanup is estimated to cost approximately \$350,000. The higher estimate of \$430,000 assumes 20 cy of material which allows for possible volume increases if material is found in the trench or other areas. Principle costs include:

	XXTDG* A skiniking	Cost (rounded to thousands)
	WBS*, Activities	\$64,000
•	32XX, studies and design	\$10,000
•	331XX01 & 331XX21, mob and demobilization	\$18,000
•	331XX02, monitoring, sampling and analysis	\$68,000
•	331XX03, site work including equip relocation, & office	\$ 4,000
•	331XX17, D&D	\$15,000
•	221VV10 transportation and disposal	
•	221 VV2201 supervision, safety & health, eng., waste ingli	nt. \$67,000
•	331XX9X, other including mgr., data, CR, permits	Ψ120,000
•	333XX, construction management	\$31,000
•	333XX, construction management	\$18,000
•	34XXX, HTRW (post construction)	

^{*} The Work Breakdown Structure (WBS) and the cost estimate are shown in Appendix B.

4.2.7 State and Community Acceptance

The last two criteria, acceptability to the state and local community, will be evaluated after public input is received.

5. SELECTION OF THE PREFERRED ALTERNATIVE

The USACE prefers Alternative 3, Decontamination of Buildings. This alternative is protective of human health and the environment and eliminates the continuing costs for monitoring and periodic reviews. Radioactive materials generated during remedial activities will be disposed at appropriate existing licensed or permitted disposal facilities. Samples would be collected from the materials for analysis to ensure that materials meet the acceptance criteria of the disposal facility(ies). Decontamination to as low as reasonably achievable levels will be conducted by (1) removal of contamination at levels above those in Regulatory Guide 1.86, (2) performing additional decontamination attempts for areas with levels above 2,000 dpm/100 cm2 (i.e., 2,000 dpm/cm2 averaged over not more than 1 m² versus the 5,000 dpm/100 cm² in the Regulatory Guide), and (3) post remediation measurements and calculations to assure that the remediated site meets the 25 mrem/yr ARAR. This action would complete the remediation of the Bliss and Laughlin site.

Radioactive materials would be packaged and shipped according to the acceptance criteria of the disposal facility as well as applicable Department of Transportation requirements. Materials would be shipped from the facility by rail or truck. The disposal location(s) will be selected after bids have been evaluated.

Engineering controls will be used during the decontamination activities to prevent the spread of radioactivity and to facilitate collection of any spilled material.

The proposed alternative will include:

- preparation of detailed work instructions and a health and safety plan; (1)
- characterization of suspect areas including the filled in trench to confirm the presence or (2) absence of contamination;
- site preparation including construction of lay-down areas and preparation of designated storage areas for managing wastes generated during building decontamination activities; (3)
- decontamination of specified areas using techniques such as vacuuming, media blasting, (4) cleaning, and/or chemical methods;
- sampling and analysis of wastes generated during remedial activities to demonstrate (5) compliance with waste acceptance criteria;
- loading and packaging of radioactive materials for shipment to the disposal facilities; (6)
- shipment of the materials to the disposal facility(ies); (7)
- restoration activities, as required; and (8)
- post remedial surveys and analyses to assure compliance with the unrestricted release criteria (9) in the ARARs and to evaluate if the action meets the TBCs.

6. COMMUNITY ROLE IN THE SELECTION PROCESS

USACE invites members of the public to review the proposed plan and the supporting documents which further describe the conditions at the Bliss & Laughlin Site and the basis for the proposal. Those documents may be found in the administrative record for the Bliss & Laughlin Site at the Buffalo and Erie County Public Library-Dudley Branch, 2010 South Park Avenue, Buffalo, New York, 14220, and at the USACE FUSRAP Public Information Center, 1776 Niagara Street, Buffalo, New York, 14207. Members of the public who wish to comment upon this proposed plan may submit their comments to USACE at the following address:

U.S. Army Corps of Engineers Buffalo District FUSRAP Public Information Center 1776 Niagara Street Buffalo, NY 14207-3199

Please refer to this proposed plan or to the Bliss & Laughlin Site in the comments. All comments will be reviewed and considered by USACE in determining the final remedy for the Bliss & Laughlin Site. Comments should be submitted no later than 30 days after the date of this proposed plan.

After the close of the comment period, USACE will review all public comments, as well as the information contained in the Administrative Record file for this site, and any new information developed or received during the course of this comment period, in light of the requirements of CERCLA and the NCP. An authorized official of USACE will then make a final selection of the remedial action to be conducted at this site. This decision will be documented in a Record of Decision, which will be issued to the public, along with a response to all comments submitted regarding this proposed plan.

7. REFERENCES

10 CFR (Code of Federal Regulations) 835. Occupational Radiation Protection; Final Rule.

40 CFR 192. Health and Environmental Protection Standards for Uranium and Thorium Mill Tailings.

AEC (Atomic Energy Commission) Regulatory Guide 1.86. Termination of Operating Licenses for Nuclear Reactors.

BNI, 1995. FUSRAP Technical Memorandum: Bliss and Laughlin Steel Characterization Results, May 11.

Cashwell, J.W., et al., 1986. Transportation Impacts of the Commercial Radioactive Waste Management Program, SAND-85-2715, Albuquerque, New Mexico, April.

NYSDEC, 1993. New York Department of Environmental Conservation Technical Administrative Guidance Memorandum (TAGM) 4003.

NUREG-1500. Dailey, M.C., et al., Working Draft Regulatory Guide on Release Criteria for Decommissioning: NRC Staff's Draft for Comment, Nuclear Regulatory Commission, Appendix A-2.

NUREG-5512. Kennedy, W. E. and Strenge, D. L., Residual Radioactive Contamination from Decommissioning, U.S. Nuclear Regulatory Commission, October 1992.

Appendix A BLISS AND LAUGHLIN STEEL CHARACTERIZATION RESULTS



128.95 - NO <u>[12</u> Rev. No.	X

DATE:

FUSRAP TECHNICAL MEMORANDUM

TO: Eric T. Newberry

FROM: Laura M. Artates

DATE: May 11, 1995

SUBJECT: Bliss and Laughlin Steel Characterization Results

Prepared By

Taam Lead Approval

Project Engineer Approval

Project Manager Approval

Rule Control

Siring

SCOPE

This Technical Memorandum presents the results of the radiological and chemical characterization of the Bliss and Laughlin Steel site. Historically, the facility was the site of uranium metal machining; therefore, the primary radiological constituent of concern is U-238. The site was assigned to FUSRAP based upon a designation survey performed by the Oak Ridge Institute for Science and Education. Using the data reported in the ORISE designation survey (ORISE, 1992) a survey of the floor area and the overheads in the vicinity of the Special Finishing Area was conducted, and a less intensive survey was performed throughout the rest of the building, with emphasis on areas adjacent to the Special Finishing Area, high traffic areas, and likely areas of material transfer such as locker rooms. Six core samples were drilled through the slab in areas where the potential for constituent migration was the greatest. Additional samples were taken from the dust on overhead beams and material on the floor. One composite sample of floor material was collected and analyzed for TCLP Total, which included metals, volatile organics, semi-volatile organics, pesticides, and herbicides.

PROCEDURES

To aid in identification of areas within the building the north-south support column lines were numbered 1 to 23 from west to east and the east-west column lines were labeled A to X from south to north (Figure 1). Each section of the floor is designated by the letter and number of the SW corner

column of that section. All sampling locations and areas of significant findings were identified such that the location can be referenced to the SW corner of a section. All fixed point measurements were performed to measure levels of alpha and beta-gamma radiation, although the conditions in the building (i.e. oil-covered floors) were expected to cause significant shielding of alpha radiation.

Three different levels of survey were performed on different areas of the floor. A Level I survey consisting of a 1-meter² five-point survey was conducted in the areas where elevated surface readings were identified (the Special Finishing Area). This survey was to clearly define the areas of elevated surface activity. A Level II survey consisting of a 100% scan using a floor monitor was conducted over a six-meter wide area surrounding all Level I survey areas. This survey was to verify that all elevated areas were bounded. A Level III survey, covering at least 50% of the floors in the remainder of the building, was performed to verify that no other areas of the building floors were radiologically elevated. Surface scan readings were considered to be elevated if they were twice background (Table 1) as used in the Level II and Level III surveys. Additional surveys were performed and samples were collected in the Special Finishing Area to determine the scope for potential remediation planning.

RESULTS

75% of the alpha readings on the floors were at or below background (<Lc), as compared to 31% of the beta-gamma readings, indicating that the majority of the alpha radiation was shielded by the material on the surfaces being scanned or measured. Because of this, both alpha and beta gamma results will be reported in the data tables, but only beta-gamma results will be discussed. The alpha results from the overheads correlated slightly better with the beta/gamma results, indicating that the overhead contamination is probably not being shielded by paint. References to all original data can be found in the Work Instruction (BNI WI-95-073).

Ceiling and Overhead Trusses

The overhead trusses above the Special Finishing Area were scanned to determine if they were above guidelines for beta-gamma contamination (Attachment 3). The survey results are presented in Figure 2 and Table 2.

- At a minimum, 50% of the surfaces of the bottom horizontal chords and the bottom two feet of the vertical members in the trusses were scanned. Twenty-one direct point measurements were recorded. There were no locations above fixed criteria, and only three locations where the direct readings were above transferable criteria (Table 2). Three composite dust samples were also collected and analyzed for radiological parameters: BLS014 from truss 19, BLS015 from truss 20, and BLS016 from truss 18 (Attachment 1). These samples had slightly elevated levels of uranium contamination, with the highest value at 15.6 pCi/g U-238. No samples were above criteria. No chemical characterization samples were collected from the overheads.
- The ceiling and upper sections of the trusses above the Special Finishing Area were surveyed by taking four direct readings on each truss and four readings on the ceiling areas near each truss. Six locations on the upper chords were smeared due to elevated readings. There were

two locations where direct measurements were above fixed criteria, and no locations where transferable measurements were above criteria (Table 2). It was not possible to access the roof vents, or to collect samples from the top portions of the trusses. There were no roof vents directly above the special finishing area.

Accessible areas of the crane were scanned, and showed no elevated readings.

Floors

Three different levels of survey were performed on different areas of the floor. Much of the floor throughout the building was obstructed by storage racks filled with steel stock or operations equipment, and was not accessible.

Level I Survey

A Level I survey consisting of a 1-meter² five-point survey and a floor monitor scan was conducted in the area where contamination was previously identified in the designation report Elevated locations identified as part of the floor monitor scan were then defined and measured using hand-held instruments. The areas of Level I survey are indicated in Figure 3 by the smaller square grid. Complete 5-point survey data for the Level I survey is presented in Attachment 4.

- Figure 3 shows the area encompassed by the Level I survey and the locations identified as not accessible (NA), elevated but below criteria (2,000-5,000 dpm/100cm²), above average criteria but below hotspot criteria (5,000 15,000 dpm/100cm²), and above hotspot criteria (15,000 dpm/100cm²).
- There were a total of ten locations above hotspot criteria. The direct beta/gamma readings for these locations ranged from approximately 17,000 to 280,000 dpm/100cm² (Table 3) and are indicated in Figure 3 by boxed X symbols.
- Eight locations fell between the average and hotspot criterias (5,000 15,000 dpm/100cm²). These locations are indicated in Figure 3 by diamond symbols. The data for these locations is presented in Table 4.
- To aid in remedial design an additional 17 locations were identified as elevated, although none of these locations is above criteria (Table 5). These locations are indicated Figure 3 by open square symbols.

Level II Survey

A Level II survey consisting of a 100% scan of accessible areas using a floor monitor and/or hand held instruments was conducted over a six-meter-wide area around the Level I survey areas. The area included is indicated in Figure 3 by the larger square grid.

This survey was used to verify that all elevated areas were bounded within the Level I survey area. No direct readings were taken in this survey. No areas at or above twice background were encountered in this survey.

Level III Survey

A Level III survey was conducted throughout the remainder of the building. The accessible floors in all areas outside the Level I and Level II areas were scanned using a floor monitor, based on the data quality objectives for this characterization. Large areas which were not accessible are indicated in Figure 1. The remainder of the floors were estimated to be accessible for survey on an average of 40% of the surface. 30 additional point measurements were taken throughout the building based on field observations (Figure 1).

- All 30 point measurements were well below criteria, showing no evidence of contamination. The results from this survey are presented in Table 6.
- Floor monitor surveys did not indicate the presence of any hotspots or elevated areas.

TCLP Results

One composite sample was collected from the floors in the Special Finishing Area and analyzed for TCLP Total. No RCRA hazardous constituents were identified (Attachment 2).

Trenches

Shallow drainage trenches in the vicinity of the special finishing area were surveyed using handheld instruments. No trenches were located in areas of elevated surface activity. The accessible sections of trenches surveyed showed no elevated readings, so no samples were collected. The trenches have been added to the as-built drawing (Figures 1 and 3).

Support columns/Equipment/etc.

- Support columns E18 and E20 were surveyed with hand-held meters to 2 meters high to determine if they were above guidelines for beta-gamma surface contamination. Results show no elevated readings (Table 7).
- The equipment in the Special Finishing Area did not show evidence of contamination. Floor surfaces underneath equipment were surveyed as part of the Level I survey. One sample of floor material from under a piece of equipment was taken where radiological analysis results above guidelines were present (Attachment 1: BLS018 and Figure 3:E).

Subsurface Floor Sampling

Six core locations in the Level 1 survey area were selected based on surface features and floor scan results. These locations were in areas where the potential for downward contamination migration was the greatest, either near expansion joints, resurfaced or repaired floor areas, or irregular areas of the floor (Figure 3). Sample results are presented in Attachment 1.

- Core location 1 (Figure 3:H) was partially under one of the pieces of equipment, at an irregular area of the floor. The drilling location was approximately 2.5 ft. E of a location which showed elevated surface readings. The concrete extended deeper than the drill could reach, so no subsurface sample was obtained. The surface of the core showed no elevated readings. A surface sample from the nearby elevated location (Figure 3:E) was collected, and showed U-238 at 1,215 pCi/g (BLS018).
- Core location 2 was taken along the surface of an old equipment stand which had apparently been demolished to the floor surface (Figure 3:I). The first attempt was directly on the broken concrete on an elevated location, but refusal was met at a few inches in depth. A sample of the top of the concrete (BLS007) was below radiological criteria. A second hole approximately 6 inches over reached soil at seven inches deep. A soil sample was collected from the top seven inches of soil (BLS011), that was below radiological criteria.
- Two attempts were made to reach soil at core location 3, which was in a repoured area near the center of the Special Finishing Area (Figure 3:J). A vertical metal bolt was encountered in the first hole, and the second one reached the furthest extent of the drill (approximately 15 inches) without encountering soil. The cores and holes were scanned and showed no elevated direct readings, and no samples were collected.
- Core location 4 was in a repoured area between columns E18 and E20 (Figure 3:K). One core was drilled, and refusal was encountered at approximately 6 inches. The core was removed, revealing gravel and the open end of a section of pipe, indicating that a trench had been filled with debris and then sealed with concrete. The core and hole were scanned and showed no elevated readings, and no samples were collected.
- Core location 5 was adjacent to an expansion joint north of column E20, where elevated readings were measured on the floor (Figure 3:L). A core was removed (approximately 6 inches), and soil samples were collected. The top six inches of soil were sent for analysis (BLS009), and the next six inches were archived. Analysis results showed that the soil was below criteria. A scan of the core and the hole showed no elevated readings.
- Core location 6 was located in the additional level I survey area between columns E16 and E18, in the center of a filled-in trench (Figure 3:M). Approximately four inches of concrete core was removed, revealing old pipe debris, gravel, and black sediment-like material. This material showed elevated readings, and two samples were collected (BLS003 & BLS004). These samples showed 23.5 and 86.7 pCi/g of U-238, respectively. A subsurface soil sample was collected using a hand-auger for analysis (BLS005) which was not above criteria, indicating that the contaminated material is isolated in the debris used to fill in the trench prior to sealing with concrete.

All of the cores which scanned clean were either placed back in the holes or disposed of as clean trash, and all of the boreholes were filled with quick-setting concrete.

Open buried conduit

There is an eight inch deep irregular hole in the floor near Column E-20 in the Special Finishing Area which contains the open end of a buried two inch conduit from which the wires have been cut and removed (Figure 3:C). The hole and the end of the conduit were scanned and a sample of the material around the conduit was collected. The hole and conduit showed no elevated readings, and analysis results of material collected from the hole were below criteria.

Water Valve Access

There is a three-foot deep water valve access shaft with a 10-inch lid near E18; N4, E11 (Figure 3:D). The interior sides and bottom of the shaft surfaces were not elevated. A sample (Attachment 1: BLS008) was taken from the material in the top of the lid, which showed U-238 at 128 pCi/g.

SUMMARY

- Two locations out of 45 surveyed on the overheads above the special finishing area were above 5000 dpm/100 sq cm beta/gamma.
- The surface contamination on the floor in the special finishing area is limited to approximately 19 meters by nine meters of floor, some of it obstructed by machinery.
- No subsurface soil samples showed evidence of contamination. One sample from a core taken through a filled-in trench showed elevated uranium levels. This material contained no long-lived daughters, and appears to be limited to debris deposited in the trench prior to sealing with concrete. The soil collected below this material was not above criteria.
- The remainder of the building was surveyed as extensively as building conditions allowed, and showed no evidence of additional contaminated areas.
- A composite TCLP total sample from the floor in the Special Finishing Area showed no RCRA hazardous constituents.

WASTE

PPE and equipment was surveyed for release to minimize the volume of radiologically contaminated waste generated. Waste water generated from cooling the core drill was used to mix the concrete used to backfill the boreholes, and the remainder will be evaporated and the residues surveyed for radiological contamination.

Figures:

Map of building with detail showing survey locations and reference grid. Figure 1.

Overheads above Special Finishing Area with Survey Locations Figure 2.

Detail of Special Finishing Area with Survey Results and Sampling Locations Figure 3.

Attachments:

1. Bliss and Laughlin Radiological Data

2. Bliss and Laughlin Chemical Data

3. DOE 5400.5 Figure IV-1, Surface contamination Guidelines

4. Bliss and Laughlin Steel 5-point Survey Data

References:

ORISE 1992, Radiological Survey of the Former Bliss and Laughlin Steel Company Facility, Buffalo, New York, ORISE 92/G-6

BNI WI, Bliss and Laughlin Steel Characterization, WI-95-073

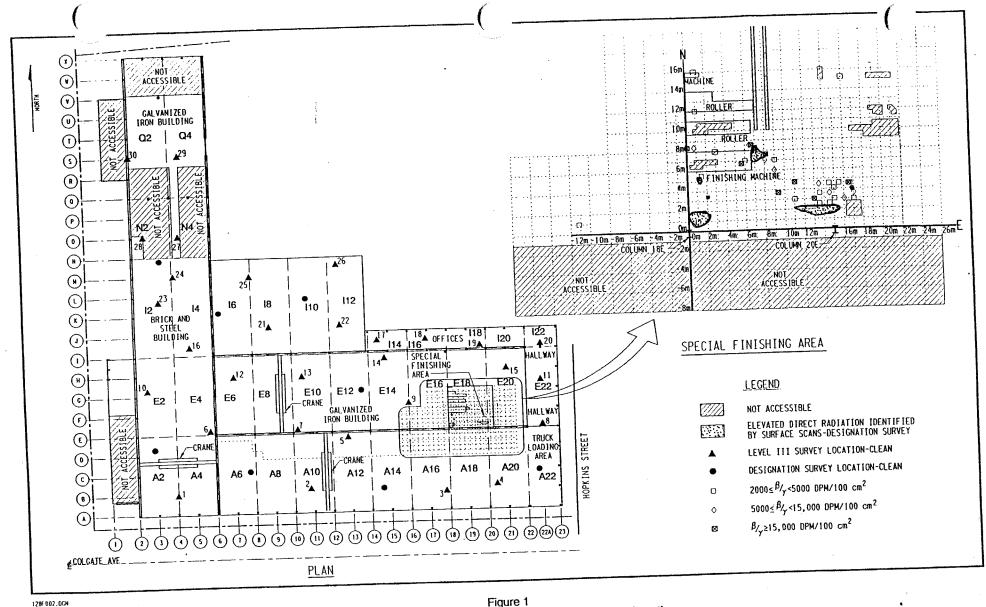
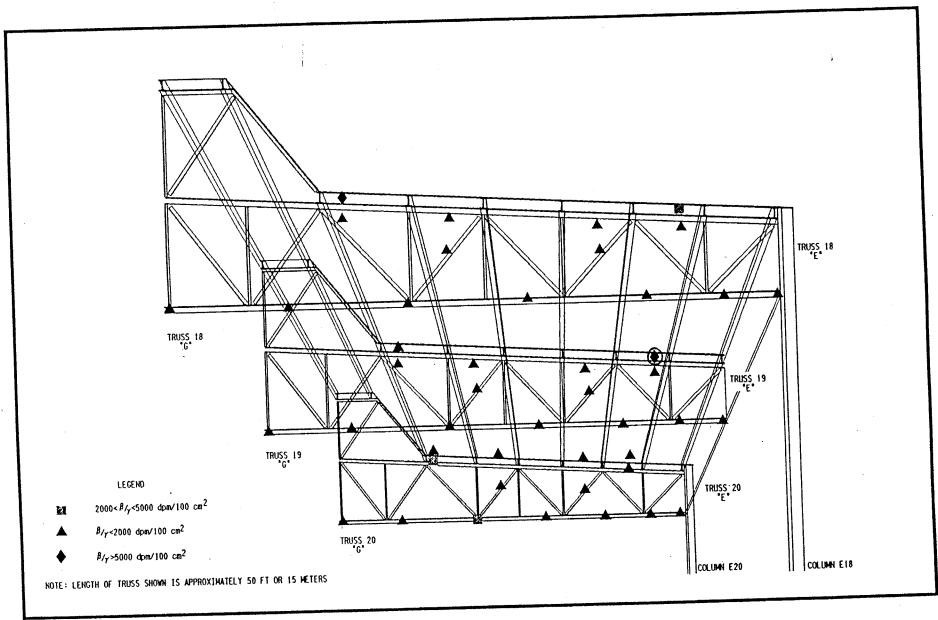
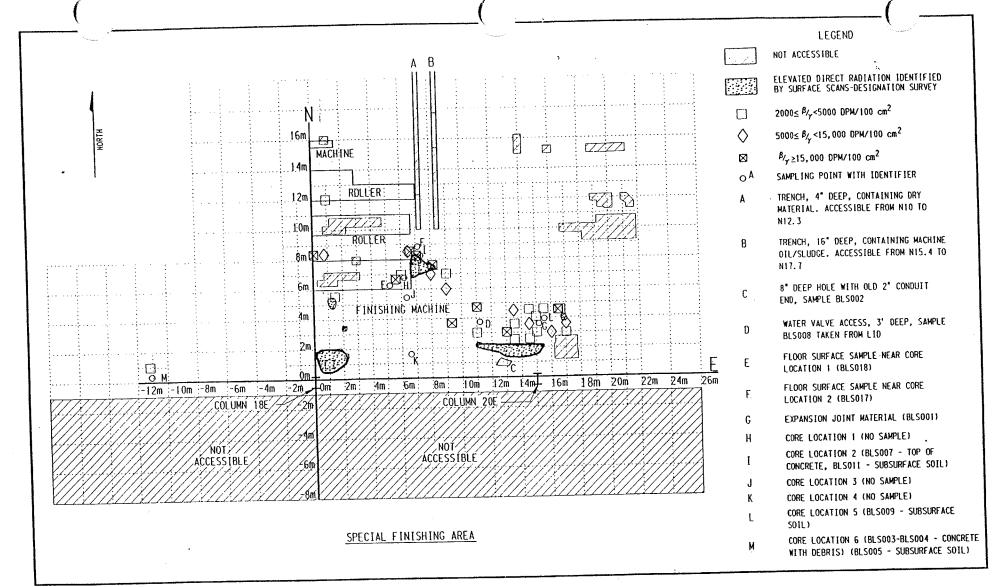


Figure 1
Bliss and Laughlin Steel with Reference Grids and Survey Locations



128F 004.DGN

Figure 2
Overheads Above Special Finishing Area
with Survey Locations



128f003.06N

Figure 3
Detail of Special Finishing Area with
Survey Results and Sampling Locations

Table 1: Bliss and Laughlin Steel Characterization Background Values

•				<u></u>		TRA	NSFERABLE		
			DIRECT	BETA-GAMM	1/100 SO CM			BETA-GAMMA	
50000000000000000000000000000000000000	ALPHA/			SMPL	STD	SMPL	STD	SMPL	STD
LOCATION/ITEM	SMPL		STD	DPM	DEV	DPM	DEV	DPM	DEV
COORDINATES	DPM		DEV	455		NA		NA	
GRID E-9		15	26			NA	1	NA `	
GRID E-9		15	26			NA	 	NA	
GRID E-9	<lc< td=""><td>6</td><td>19</td><td><lc 187<="" td=""><td></td><td>NA</td><td>†</td><td>NA</td><td></td></lc></td></lc<>	6	19	<lc 187<="" td=""><td></td><td>NA</td><td>†</td><td>NA</td><td></td></lc>		NA	†	NA	
GRID E-9		24	32	455		NA	+	NA	
GRID E-9	<lc< td=""><td>6</td><td>19</td><td></td><td></td><td>NA NA</td><td> </td><td>NA</td><td></td></lc<>	6	19			NA NA	 	NA	
GRID E-9	<u> </u>	19	34	55		NA.	 	NA	
GRID E-9		19		<lc 32<="" td=""><td></td><td></td><td></td><td>NA</td><td></td></lc>				NA	
GRID E-9	<lc< td=""><td>0</td><td>21</td><td>42</td><td></td><td></td><td>+</td><td>NA</td><td></td></lc<>	0	21	42			+	NA	
GRID E-9	<lc< td=""><td>10</td><td>28</td><td><lc 35<="" td=""><td></td><td></td><td>+</td><td>NA.</td><td></td></lc></td></lc<>	10	28	<lc 35<="" td=""><td></td><td></td><td>+</td><td>NA.</td><td></td></lc>			+	NA.	
GRID E-9	<lc< td=""><td>10</td><td>28</td><td>610</td><td>5 572</td><td>II INA</td><td></td><td><u>. J </u></td><td></td></lc<>	10	28	610	5 572	II INA		<u>. J </u>	

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

Table 2: Bliss and Laughlin Steel Characterization Survey of Overheads

								TRAN	SFERABLE				
			ECT	DETA A	GANANA/1	00 SQ CM	ALPHA	V100 S	Q CM	BET			00 SQ CM
	ALPHA	/100 SC				STD		1PL	STD		SMP	L	STD
LOCATION/ITEM	SMPL	.	STD		MPL	DEV		PM	DEV		DPN	1]_	DEV_
COORDINATES	DPM		DEV	<u> </u>	PM	DEV	- 5.	-,,					
RUSS 20E-G						420	 -			1			
EILING @ 4M	<lc< td=""><td>6</td><td>19</td><td><lc< td=""><td>54</td><td>420</td><td> </td><td></td><td></td><td>╂</td><td></td><td></td><td></td></lc<></td></lc<>	6	19	<lc< td=""><td>54</td><td>420</td><td> </td><td></td><td></td><td>╂</td><td></td><td></td><td></td></lc<>	54	420	 			╂			
EILING @ 7M	<lc< td=""><td>-4</td><td>5</td><td></td><td>348</td><td>454</td><td> </td><td></td><td></td><td>\dagger</td><td></td><td></td><td><u>,</u></td></lc<>	-4	5		348	454	 			\dagger			<u>,</u>
CEILING @ 7M		24	32	<lc< td=""><td>134</td><td>429</td><td> </td><td></td><td></td><td>-</td><td></td><td></td><td></td></lc<>	134	429	 			-			
CEILING @ 13M	<lc< td=""><td>6</td><td>19</td><td></td><td>482</td><td>469</td><td>ļ</td><td></td><td></td><td><lc< td=""><td></td><td>0</td><td>74</td></lc<></td></lc<>	6	19		482	469	ļ			<lc< td=""><td></td><td>0</td><td>74</td></lc<>		0	74
SELING @ 15M	<lc< td=""><td>6</td><td>19</td><td></td><td>1874</td><td>603</td><td><lc< td=""><td>0</td><td><u>_</u></td><td>1</td><td></td><td>_+</td><td></td></lc<></td></lc<>	6	19		1874	603	<lc< td=""><td>0</td><td><u>_</u></td><td>1</td><td></td><td>_+</td><td></td></lc<>	0	<u>_</u>	1		_ +	
OP OF TRUSS @ 13M	<lc< td=""><td>6</td><td>19</td><td></td><td>509</td><td>472</td><td></td><td></td><td></td><td>₩</td><td></td><td></td><td></td></lc<>	6	19		509	472				₩			
OP OF ANGLE @ 11M	1	24	32	<lc< td=""><td>-107</td><td>400</td><td></td><td></td><td><u> </u></td><td>١</td><td></td><td>37</td><td>78</td></lc<>	-107	400			<u> </u>	١		37	78
TOP OF ANGLE @ 7M	100	6	19		2838	680	L	2	6	<l(< td=""><td><u> </u></td><td>-3/</td><td></td></l(<>	<u> </u>	-3/	
TOP OF TRUSS @ 4M	<lc< td=""><td>24</td><td>32</td><td></td><td>518</td><td>454</td><td></td><td></td><td></td><td>↓_</td><td></td><td></td><td></td></lc<>	24	32		518	454				↓_			
TRUSS 19E-G	ļ.,	-4		<Ŀc	294	448							
CEILING @ 4M	<lc< td=""><td></td><td></td><td><lc< td=""><td>0</td><td>413</td><td></td><td></td><td></td><td>Ш_</td><td></td><td></td><td></td></lc<></td></lc<>			<lc< td=""><td>0</td><td>413</td><td></td><td></td><td></td><td>Ш_</td><td></td><td></td><td></td></lc<>	0	413				Ш_			
CEILING @ 7M	<lc< td=""><td>-4</td><td>32</td><td><lc< td=""><td>214</td><td>439</td><td></td><td></td><td>·</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-4	32	<lc< td=""><td>214</td><td>439</td><td></td><td></td><td>·</td><td></td><td></td><td></td><td></td></lc<>	214	439			·				
CEILING @ 11M	J	24		- LC	375	457				1			
CEILING @ 13M	<lc< td=""><td>6</td><td>19</td><td>-</td><td>5943</td><td>884</td><td></td><td>2</td><td>6</td><td><l< td=""><td>.с</td><td>49</td><td>80</td></l<></td></lc<>	6	19	-	5943	884		2	6	<l< td=""><td>.с</td><td>49</td><td>80</td></l<>	.с	49	80
TOP OF TRUSS @ 13M		24	32	ļ	562	478			T				
TOP OF ANGLE @ 11M	1	15	26	 	455	466			1				
TOP OF ANGLE @ 7M	<lc< td=""><td>-4</td><td>5</td><td></td><td>1365</td><td>558</td><td></td><td>2</td><td><u> </u></td><td></td><td></td><td>86</td><td>83</td></lc<>	-4	5		1365	558		2	<u> </u>			86	83
TOP OF TRUSS @ 4M		24	32	↓	1365	330			 	1			
TRUSS 18E-G						439			-	1			
CEILING @ 4M	<lc< td=""><td>-4</td><td>5</td><td>4</td><td>214</td><td>1</td><td></td><td></td><td>+</td><td></td><td></td><td></td><td></td></lc<>	-4	5	4	214	1			+				
CEILING @ 7M	<lc< td=""><td>6</td><td>19</td><td><lc< td=""><td>294</td><td>448</td><td></td><td></td><td></td><td>+</td><td></td><td></td><td></td></lc<></td></lc<>	6	19	<lc< td=""><td>294</td><td>448</td><td></td><td></td><td></td><td>+</td><td></td><td></td><td></td></lc<>	294	448				+			
CEILING @ 11M	1	15	- 26	<lc< td=""><td>-27</td><td>410</td><td></td><td></td><td> </td><td></td><td></td><td></td><td></td></lc<>	-27	410			 				
CEILING @ 13M	<lc< td=""><td>6</td><td>19</td><td><lc< td=""><td>54</td><td>420</td><td></td><td>- 44</td><td>1</td><td>1 2</td><td>Lc</td><td>41</td><td>79</td></lc<></td></lc<>	6	19	<lc< td=""><td>54</td><td>420</td><td></td><td>- 44</td><td>1</td><td>1 2</td><td>Lc</td><td>41</td><td>79</td></lc<>	54	420		- 44	1	1 2	Lc	41	79
TOP OF TRUSS @ 13M	+	42	41		4149	773		11	 '	<u>' </u>			
TOP OF TRUSS @ 15M	<lc< td=""><td>6</td><td>19</td><td><lc< td=""><td>-80</td><td>403</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	6	19	<lc< td=""><td>-80</td><td>403</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-80	403							
TOP OF ANGLE @ 11M	-	24	32		616	484				1		0	74
TOP OF ANGLE @ 7M		52	45		6318	906	3				<u>Lc</u>	25	77
TOP OF TRUSS @ 4M		33	36	_	5702	870) <lc< td=""><td></td><td>) </td><td>0 <</td><td>Lc</td><td>25</td><td> </td></lc<>)	0 <	Lc	25	
QC	DUCCE			-						_#_			
BOTTOM HORIZONTAL T	RUSSE	>		<lc< td=""><td>285</td><td>42</td><td>8</td><td></td><td></td><td>_ _</td><td></td><td></td><td>ļ</td></lc<>	285	42	8			_ _			ļ
TRUSS #20 Om	<lc< td=""><td>-4</td><td>26</td><td></td><td>207</td><td></td><td>9</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-4	26		207		9						
TRUSS #20 3m	_	15	26		2228		4	NA					
TRUSS #20 6m		15											<u> </u>
TRUSS #20 9m		15	26		700								
TRUSS #20 12m		15	26		544								
TRUSS #20 15m	<lc< td=""><td>-4</td><td></td><td>5</td><td>466</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	-4		5	466								<u> </u>
TRUSS #20 18m		15	20		518					1			
TRUSS #19 0m		24		2									
TRUSS #19 3m	<lc< td=""><td>-4</td><td>l</td><td>5 <lo< td=""><td></td><td></td><td></td><td>NA</td><td>_</td><td>-</td><td></td><td></td><td></td></lo<></td></lc<>	-4	l	5 <lo< td=""><td></td><td></td><td></td><td>NA</td><td>_</td><td>-</td><td></td><td></td><td></td></lo<>				NA	_	-			
TRUSS #19 6m		15	2		1036			NA					
TRUSS #19 9m		33		6	1062			INA		-+			
		24	3	2	440		16						1
111000 1110		24	3	2 <lc< td=""><td></td><td></td><td>97</td><td></td><td></td><td></td><td></td><td></td><td>1</td></lc<>			97						1
1111000 11 1-	<lc< td=""><td>6</td><td></td><td>9 <l< td=""><td></td><td></td><td>28</td><td></td><td></td><td></td><td></td><td></td><td></td></l<></td></lc<>	 6		9 <l< td=""><td></td><td></td><td>28</td><td></td><td></td><td></td><td></td><td></td><td></td></l<>			28						
TRUSS #19 18m	<lc< td=""><td>- 6</td><td></td><td>9</td><td>518</td><td></td><td>54</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	- 6		9	518		54						
TRUSS #18 0m	<lc< td=""><td>6</td><td></td><td>9 <l< td=""><td>52</td><td>2 40</td><td>00 </td><td></td><td></td><td>∦</td><td></td><td></td><td></td></l<></td></lc<>	6		9 <l< td=""><td>52</td><td>2 40</td><td>00 </td><td></td><td></td><td>∦</td><td></td><td></td><td></td></l<>	52	2 40	00			∦			
TRUSS #18 3m	- INC	42		11	596		63			#			
TRUSS #18 6m		24		2 <l< td=""><td></td><td></td><td>19</td><td></td><td></td><td>∦</td><td></td><td></td><td> </td></l<>			19			∦			
TRUSS #18 9m				9 <l< td=""><td></td><td></td><td>28</td><td></td><td></td><td></td><td></td><td></td><td></td></l<>			28						
TRUSS #18 12m	<lc< td=""><td>6</td><td></td><td></td><td>36</td><td></td><td>37</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	6			36		37						
TRUSS #18 15m		24		32	82		87						
TRUSS #18 18m	<u> </u>	24	1 3	32	02	<u> </u>							

Comments:

0 is the center of the truss ("G"). Measurements are in meters moving south (towards "E").

Table 3:

Bliss and Laughlin Steel Characterization

Special Finishing Area - Survey locations above 15000 dpm/100 sq cm beta/gamma

						ANCEER	ADIE		
1		DIRECT				ANSFER	DET	A-GAMMA/	100 SQ CM
	ALPHA/100	SQ CM	BETA-GAMMA/10		ALPHA/100			SMPL	STD
LOCATION/ITEM		STD DEV	SMPL DPM	STD DEV	SMPL DPM	STD DEV		DPM	DEV
COORDINATES	<lc -4<="" td=""><td></td><td></td><td>3303</td><td></td><td></td><td></td><td></td><td>73</td></lc>			3303					73
N3.0 E13.0	48			2670		11		-21	76
N8.0 E7.0 N3.7 E9.35	15	26	42270	2126	5	8	<lc< td=""><td>12 1734</td><td>181</td></lc<>	12 1734	181
N7.6 E8.1	3165	335	135430	3755	224	50		258	98
N8.1 E7.2	181	81	280257	5384	72	28		152	89
N8.5 E6.7	1129	200	29019	1776	17	14		184	1
N6.7 E5.7	42	41	17213	1393	23	10	<lc< td=""><td>33</td><td></td></lc<>	33	
N8.2 E0.1	98	60	218953	4763	<lc 0<="" td=""><td>0</td><td><lc< td=""><td>25</td><td></td></lc<></td></lc>	0	<lc< td=""><td>25</td><td></td></lc<>	25	
N4.8 E11.0	33	36	55387	2422	< <u>Lc 0</u> 2	1	<lc< td=""><td>20</td><td></td></lc<>	20	
N4.5 E16.5	88	57	71985	2752	<u> </u>	<u> </u>	1		<u></u>

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

Table 4:

Bliss and Laughlin Steel Characterization

Special Finishing Area - Survey locations between 5000 and 15000 dpm/100 sq cm beta/gamma

								ANIOSES	ADI E		
			DIRECT					ANSFER	ABLE		00.00.014
	ALPHA	100		BETA-GAMMA/10	0 SQ CM	ALPHA/10	00	SQ CM	BET	A-GAMMA/	
LOCATION/ITEM		-	STD		STD	SMPL		STD			STD
	DPM		DEV	DPM	DEV	DPM_		DEV		DPM	DEV
COORDINATES	DEIVI	24		6063	871	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-54</td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>-54</td><td></td></lc<>	-54	
N3.0 E16.0	<u> </u>				969	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-50</td><td>70</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-50</td><td>70</td></lc<>	-50	70
N3.5 E14.5	<lc< td=""><td>28</td><td></td><td>H</td><td></td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>4</td><td>76</td></lc<></td></lc<></td></lc<>	28		H		<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>4</td><td>76</td></lc<></td></lc<>	-1		<lc< td=""><td>4</td><td>76</td></lc<>	4	76
N4.5 E13.5	<lc< td=""><td>9</td><td></td><td><u> </u></td><td>1</td><td></td><td>5</td><td></td><td><lc< td=""><td>-13</td><td>76</td></lc<></td></lc<>	9		<u> </u>	1		5		<lc< td=""><td>-13</td><td>76</td></lc<>	-13	76
N6.0 E9.0	1	33					- 5		<lc< td=""><td>46</td><td></td></lc<>	46	
N7.0 E8.0		77	74							59	
N8.5 E6.5		64	62	6130	901		5		<lc< td=""><td></td><td>78</td></lc<>		78
	1	15	26	14777	1300	<lc< td=""><td>0</td><td>0</td><td><lc< td=""><td>33</td><td></td></lc<></td></lc<>	0	0	<lc< td=""><td>33</td><td></td></lc<>	33	
N8.3 E0.9	<lc< td=""><td>6</td><td>19</td><td>6559</td><td>919</td><td></td><td>2</td><td>6</td><td><lc< td=""><td>-12</td><td>73</td></lc<></td></lc<>	6	19	6559	919		2	6	<lc< td=""><td>-12</td><td>73</td></lc<>	-12	73
N3.4 E17.0	\		1, ,,,	<u> </u>							

Lc indicates less than the critical level of activity which can be said to be above background.
A negative value is the calculated result of a reading which is below the instrument-specific background.

Table 5:

Bliss and Laughlin Steel Characterization

Special Finishing Area - Survey locations between 2000 and 5000 dpm/100 sq cm beta/gamma

							o E E D	A DI E		
[DIRECT					ANSFER	ABLE	A-GAMMA/1	no so cM
1	ALPHA/100	SQ CM	BETA-GAMMA/10		ALPHA			DEI	SMPL	STD
LOCATION/ITEM		STD	SMPL	STD	SMF	- 1	STD DEV		DPM	DEV
COORDINATES	DPM	DEV	DPM	DEV	DPI	<u>vi</u>	DEV		D; 14.	
N1.0 E1.0	24			805			6	<lc< td=""><td>-33</td><td>71</td></lc<>	-33	71
N12.0 E1.0	<lc -10<="" td=""><td></td><td></td><td></td><td><lc< td=""><td>2 -1</td><td></td><td><lc< td=""><td>17</td><td>77</td></lc<></td></lc<></td></lc>				<lc< td=""><td>2 -1</td><td></td><td><lc< td=""><td>17</td><td>77</td></lc<></td></lc<>	2 -1		<lc< td=""><td>17</td><td>77</td></lc<>	17	77
N2.5 E13.5	<lc -9<="" td=""><td></td><td></td><td></td><td><lc< td=""><td><u>-1</u> -1</td><td>0</td><td></td><td>-8</td><td></td></lc<></td></lc>				<lc< td=""><td><u>-1</u> -1</td><td>0</td><td></td><td>-8</td><td></td></lc<>	<u>-1</u> -1	0		-8	
N2.5 E14.5	<lc -9<="" td=""><td>35</td><td></td><td></td><td><lc< td=""><td></td><td>6</td><td><lc< td=""><td>-8</td><td></td></lc<></td></lc<></td></lc>	35			<lc< td=""><td></td><td>6</td><td><lc< td=""><td>-8</td><td></td></lc<></td></lc<>		6	<lc< td=""><td>-8</td><td></td></lc<>	-8	
N3.0 E11.0	24	37				2		VLC	-8	
N3.0 E15.0	24	37			<lc_< td=""><td>-1</td><td></td><td><lc< td=""><td></td><td></td></lc<></td></lc_<>	-1		<lc< td=""><td></td><td></td></lc<>		
N3.0 E17.0	<lc (<="" td=""><td>27</td><td></td><td></td><td></td><td>8</td><td></td><td><lc< td=""><td>8</td><td><u> </u></td></lc<></td></lc>	27				8		<lc< td=""><td>8</td><td><u> </u></td></lc<>	8	<u> </u>
N3.5 E13.5	<lc '<="" td=""><td>43</td><td></td><td></td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-33</td><td></td></lc<></td></lc<></td></lc>	43			<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-33</td><td></td></lc<></td></lc<>	-1		<lc< td=""><td>-33</td><td></td></lc<>	-33	
N4.0 E15.0	<lc 1:<="" td=""><td>33</td><td></td><td></td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>8-</td><td></td></lc<></td></lc<></td></lc>	33			<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>8-</td><td></td></lc<></td></lc<>	-1		<lc< td=""><td>8-</td><td></td></lc<>	8-	
N4.5 E14.5	5	5 59			<lc< td=""><td><u>-1</u></td><td></td><td><lc< td=""><td>-8</td><td></td></lc<></td></lc<>	<u>-1</u>		<lc< td=""><td>-8</td><td></td></lc<>	-8	
N4.5 E15.5	<lc -<="" td=""><td>35</td><td></td><td></td><td><lc< td=""><td>2</td><td></td><td></td><td></td><td></td></lc<></td></lc>	35			<lc< td=""><td>2</td><td></td><td></td><td></td><td></td></lc<>	2				
N4.5 E16.5	11	9 43			<lc< td=""><td>2</td><td></td><td></td><td></td><td></td></lc<>	2				
N5.5 E1.5	<lc -2<="" td=""><td>8 24</td><td></td><td></td><td><lc< td=""><td>-1</td><td><u> </u></td><td>4</td><td></td><td></td></lc<></td></lc>	8 24			<lc< td=""><td>-1</td><td><u> </u></td><td>4</td><td></td><td></td></lc<>	-1	<u> </u>	4		
N7.0 E6.0		0 54				5		4		
N7.0 E9.0	<lc -2<="" td=""><td>9 39</td><td></td><td>4</td><td>/CLC</td><td>2</td><td></td><td>1</td><td></td><td></td></lc>	9 39		4	/CLC	2		1		
N7.5 E7.5		9 43			<lc< td=""><td>2</td><td></td><td><lc< td=""><td></td><td>78</td></lc<></td></lc<>	2		<lc< td=""><td></td><td>78</td></lc<>		78
N1.0 E-11.1	15	26	3641	738	1	2	1 0	I/LC	31	1

Lc indicates less than the critical level of activity which can be said to be above background.
A negative value is the calculated result of a reading which is below the instrument-specific background.

Table 6: Bliss and Laughlin Steel Characterization Level III Survey - 30 Points

			•				γ						
	· · · · · · · · · · · · · · · · · · ·			DIRECT						SFERABLE	DETA	GAMMA/100	SO CM
	Ī	ALPH/	4/100 S	Q CM	BETA	-GAMMA/1		ALPHA				SMPL	STD
	LOCATION/ITEM	SMI		STD		SMPL	STD	SMI		STD		DPM	DEV
NO:	i i	DPN	v	DEV		DPM	DEV	DP		DEV 6	<lc< td=""><td>-21</td><td>76</td></lc<>	-21	76
		<lc< td=""><td>-10</td><td>47</td><td></td><td>1101</td><td>617</td><td><lc< td=""><td>2</td><td></td><td><lc< td=""><td>-84</td><td>69</td></lc<></td></lc<></td></lc<>	-10	47		1101	617	<lc< td=""><td>2</td><td></td><td><lc< td=""><td>-84</td><td>69</td></lc<></td></lc<>	2		<lc< td=""><td>-84</td><td>69</td></lc<>	-84	69
1-3	A11; N8.9 W1.4	<lc< td=""><td>Q</td><td>51</td><td></td><td>887</td><td></td><td><lc< td=""><td>2</td><td>6</td><td>VLC.</td><td>-04</td><td></td></lc<></td></lc<>	Q	51		887		<lc< td=""><td>2</td><td>6</td><td>VLC.</td><td>-04</td><td></td></lc<>	2	6	VLC.	-04	
	A18: N6.7 W1.5	1	NA	NA	<lc< td=""><td>153</td><td>519</td><td></td><td></td><td></td><td>ļ</td><td></td><td></td></lc<>	153	519				ļ		
4	112 0 50 0	<lc< td=""><td>-29</td><td>39</td><td></td><td>642</td><td>572</td><td></td><td></td><td></td><td> </td><td></td><td></td></lc<>	-29	39		642	572				 		
·	E12; S2.2 E6.2	<lc< td=""><td>-19</td><td>43</td><td></td><td>581</td><td>565</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-19	43		581	565						
	E6; N1.2 W2.0	<lc< td=""><td>-39</td><td>34</td><td><lc< td=""><td>275</td><td>533</td><td>ļ</td><td></td><td></td><td> </td><td></td><td></td></lc<></td></lc<>	-39	34	<lc< td=""><td>275</td><td>533</td><td>ļ</td><td></td><td></td><td> </td><td></td><td></td></lc<>	275	533	ļ			 		
	E10, N1.0 E1.6	<lc< td=""><td>-19</td><td>43</td><td></td><td>459</td><td>553</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-19	43		459	553						
	3 120: S29.7 E20.3	<lc< td=""><td>-29</td><td>39</td><td><lc< td=""><td>336</td><td>539</td><td></td><td></td><td></td><td> </td><td></td><td></td></lc<></td></lc<>	-29	39	<lc< td=""><td>336</td><td>539</td><td></td><td></td><td></td><td> </td><td></td><td></td></lc<>	336	539				 		
	E16; N10.3 E0.0	<lc< td=""><td>-10</td><td>47</td><td><lc< td=""><td>306</td><td>536</td><td></td><td></td><td></td><td>╫</td><td></td><td></td></lc<></td></lc<>	-10	47	<lc< td=""><td>306</td><td>536</td><td></td><td></td><td></td><td>╫</td><td></td><td></td></lc<>	306	536				╫		
	G2; N1.6 E4.3	<lc< td=""><td>29</td><td>60</td><td><lc< td=""><td>214</td><td>526</td><td><u> </u></td><td></td><td></td><td>-</td><td></td><td></td></lc<></td></lc<>	29	60	<lc< td=""><td>214</td><td>526</td><td><u> </u></td><td></td><td></td><td>-</td><td></td><td></td></lc<>	214	526	<u> </u>			-		
11	120; S12.5 E20.3	<lc< td=""><td>-29</td><td>39</td><td><lc< td=""><td>-31</td><td>498</td><td> </td><td></td><td></td><td>╂~~~</td><td></td><td></td></lc<></td></lc<>	-29	39	<lc< td=""><td>-31</td><td>498</td><td> </td><td></td><td></td><td>╂~~~</td><td></td><td></td></lc<>	-31	498	 			╂~~~		
	H2: S1.3 E80.0	<lc< td=""><td>-19</td><td>43</td><td><lc< td=""><td>367</td><td>543</td><td> </td><td></td><td></td><td>╂──</td><td></td><td></td></lc<></td></lc<>	-19	43	<lc< td=""><td>367</td><td>543</td><td> </td><td></td><td></td><td>╂──</td><td></td><td></td></lc<>	367	543	 			╂──		
	E10; N21.4 E3.9	<lc< td=""><td>-10</td><td>47</td><td></td><td>734</td><td>581</td><td>-</td><td></td><td></td><td>╂</td><td></td><td></td></lc<>	-10	47		734	581	-			╂		
	1 111; N2.8 W1.5	<lc< td=""><td>-39</td><td>34</td><td><lc< td=""><td>306</td><td>536</td><td>ļ</td><td></td><td></td><td>╂</td><td></td><td></td></lc<></td></lc<>	-39	34	<lc< td=""><td>306</td><td>536</td><td>ļ</td><td></td><td></td><td>╂</td><td></td><td></td></lc<>	306	536	ļ			╂		
15	5 121; S7.5 E0.0	<lc< td=""><td>-19</td><td>43</td><td><lc< td=""><td>61</td><td>509</td><td> </td><td></td><td></td><td>╫──</td><td>,</td><td></td></lc<></td></lc<>	-19	43	<lc< td=""><td>61</td><td>509</td><td> </td><td></td><td></td><td>╫──</td><td>,</td><td></td></lc<>	61	509	 			╫──	,	
	5 J2; S4.6 E21.1	<lc< td=""><td>-39</td><td>34</td><td></td><td>550</td><td>562</td><td>ļ</td><td></td><td></td><td>#</td><td></td><td></td></lc<>	-39	34		550	562	ļ			#		
	7 114; N4.7 E4.0	<lc< td=""><td>-29</td><td>39</td><td><lc< td=""><td>367</td><td>543</td><td>ļ</td><td></td><td> </td><td>╂</td><td></td><td></td></lc<></td></lc<>	-29	39	<lc< td=""><td>367</td><td>543</td><td>ļ</td><td></td><td> </td><td>╂</td><td></td><td></td></lc<>	367	543	ļ		 	╂		
	B 116: N4.0 E8.4	<lc< td=""><td>-19</td><td>43</td><td><u> </u></td><td>428</td><td>549</td><td>-</td><td></td><td></td><td>╫──</td><td></td><td></td></lc<>	-19	43	<u> </u>	428	549	-			╫──		
	9 120; NO.7 WO.7	<lc< td=""><td>-48</td><td>28</td><td><lc< td=""><td>275</td><td>533</td><td> </td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-48	28	<lc< td=""><td>275</td><td>533</td><td> </td><td></td><td></td><td></td><td></td><td></td></lc<>	275	533	 					
	0 120: NO.7 E20.3	<lc< td=""><td>-48</td><td>28</td><td>ļ</td><td>581</td><td>565</td><td>-</td><td></td><td></td><td></td><td></td><td></td></lc<>	-48	28	ļ	581	565	-					
, 2	1 19; N10.1 W1.0	<lc< td=""><td>-29</td><td>39</td><td><lc< td=""><td>275</td><td>533</td><td> </td><td></td><td> </td><td></td><td></td><td></td></lc<></td></lc<>	-29	39	<lc< td=""><td>275</td><td>533</td><td> </td><td></td><td> </td><td></td><td></td><td></td></lc<>	275	533	 		 			
2	2 112; N9.7 E4.3	<lc< td=""><td>-10</td><td>47</td><td><lc< td=""><td>245</td><td>529</td><td>┨</td><td></td><td> </td><td>1</td><td></td><td></td></lc<></td></lc<>	-10	47	<lc< td=""><td>245</td><td>529</td><td>┨</td><td></td><td> </td><td>1</td><td></td><td></td></lc<>	245	529	┨		 	1		
2		<lc< td=""><td>-48</td><td>28</td><td><lc< td=""><td>275</td><td>533</td><td> </td><td></td><td>ļ</td><td>1</td><td></td><td></td></lc<></td></lc<>	-48	28	<lc< td=""><td>275</td><td>533</td><td> </td><td></td><td>ļ</td><td>1</td><td></td><td></td></lc<>	275	533	 		ļ	1		
	4 M6; N0.0 W7.5	<lc< td=""><td>-29</td><td>39</td><td><lc< td=""><td>275</td><td>1</td><td></td><td></td><td></td><td>+</td><td></td><td></td></lc<></td></lc<>	-29	39	<lc< td=""><td>275</td><td>1</td><td></td><td></td><td></td><td>+</td><td></td><td></td></lc<>	275	1				+		
2	5 M8; S0.9 W0.3	<lc< td=""><td>0</td><td>51</td><td><lc< td=""><td>367</td><td>543</td><td>-</td><td></td><td>+</td><td>+</td><td></td><td></td></lc<></td></lc<>	0	51	<lc< td=""><td>367</td><td>543</td><td>-</td><td></td><td>+</td><td>+</td><td></td><td></td></lc<>	367	543	-		+	+		
1 2	6 M12; N3.1 E3.4		67	71	↓	550		 		-	+		
2		<lc< td=""><td>-39</td><td>34</td><td><lc< td=""><td></td><td></td><td></td><td></td><td> </td><td>+</td><td></td><td>1</td></lc<></td></lc<>	-39	34	<lc< td=""><td></td><td></td><td></td><td></td><td> </td><td>+</td><td></td><td>1</td></lc<>					 	+		1
2		<lc< td=""><td>-48</td><td></td><td><lc< td=""><td></td><td></td><td></td><td>-1</td><td>1</td><td><lc< td=""><td>-105</td><td>66</td></lc<></td></lc<></td></lc<>	-48		<lc< td=""><td></td><td></td><td></td><td>-1</td><td>1</td><td><lc< td=""><td>-105</td><td>66</td></lc<></td></lc<>				-1	1	<lc< td=""><td>-105</td><td>66</td></lc<>	-105	66
	9 S6; N0.0 W11.4	<lc< td=""><td>-10</td><td></td><td></td><td>1070</td><td>565</td><td></td><td>-,</td><td> </td><td>+</td><td></td><td></td></lc<>	-10			1070	565		-,	 	+		
	0 S2; N4.0 E0.2	<lc< td=""><td>-19</td><td>43</td><td></td><td>581</td><td>565</td><td>Ш</td><td></td><td></td><td></td><td></td><td></td></lc<>	-19	43		581	565	Ш					

Comments:

NA= AREA TOO WET TO OBTAIN ALPHA MEASUREMENTS

THE ALPHA NUMERIC CHARACTERS REPRESENT THE REFERENCED COLUMN USED TO OBTAIN

THE COORDINATES

THE NUMBER REPRESENTS THE LOCATION AS SHOWN ON THE FIGURE.

Table 7: Bliss and Laughlin Steel Characterization Survey of Columns

a and a superior and			URECT				TRAN	ISFERABLE		400 00 014
	ALPHA		O CM	BETA-C	AMMA/1	00 SQ CM	ALPHA/100	SQ CM	BETA-GAMMA	/100 SQ CM
	1		STD		IPL	STD	SMPL	STD	SMPL	STD
LOCATION/ITEM	SMPI DPM		DEV		PM	DEV	DPM	DEV	DPM	DEV
COORDINATES	DPIVI		- DEV							
COLUMN E-18A		0	21	<lc< td=""><td>324</td><td>539</td><td></td><td></td><td></td><td></td></lc<>	324	539				
RONT @ 1M	<lc< td=""><td>38</td><td></td><td><lc< td=""><td>-195</td><td>476</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	38		<lc< td=""><td>-195</td><td>476</td><td></td><td></td><td></td><td></td></lc<>	-195	476				
BACK @ 1M		10		<lc< td=""><td>-130</td><td>484</td><td></td><td></td><td></td><td></td></lc<>	-130	484				
SIDE @ 1M	<lc< td=""><td>$\frac{10}{0}$</td><td></td><td><lc< td=""><td>-130</td><td>484</td><td></td><td></td><td></td><td>ļ</td></lc<></td></lc<>	$\frac{10}{0}$		<lc< td=""><td>-130</td><td>484</td><td></td><td></td><td></td><td>ļ</td></lc<>	-130	484				ļ
SIDE @ 1M	<lc< td=""><td></td><td></td><td>120</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			120						
COLUMN E-18B		19	34	<lc< td=""><td>97</td><td>512</td><td></td><td></td><td></td><td></td></lc<>	97	512				
FRONT @ 1M		0		<lc< td=""><td>-195</td><td>476</td><td></td><td></td><td></td><td></td></lc<>	-195	476				
BACK @ 1M	<lc< td=""><td>0</td><td>21</td><td><lc< td=""><td>-389</td><td>449</td><td></td><td></td><td></td><td>ļ<u>.</u></td></lc<></td></lc<>	0	21	<lc< td=""><td>-389</td><td>449</td><td></td><td></td><td></td><td>ļ<u>.</u></td></lc<>	-389	449				ļ <u>.</u>
SIDE @ 1M	<lc< td=""><td>19</td><td>34</td><td><lc< td=""><td>-195</td><td>476</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	19	34	<lc< td=""><td>-195</td><td>476</td><td></td><td></td><td></td><td></td></lc<>	-195	476				
SIDE @ 1M		19	J-4						1	
COLUMN E-18A	1 -	-40	8	<lc< td=""><td>-227</td><td>471</td><td></td><td></td><td></td><td></td></lc<>	-227	471				
FRONT @ 2M	<lc< td=""><td>-10 -10</td><td>8</td><td><lc< td=""><td>32</td><td>504</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-10 -10	8	<lc< td=""><td>32</td><td>504</td><td></td><td></td><td></td><td></td></lc<>	32	504				
BACK @ 2M	<lc< td=""><td></td><td>8</td><td><lc< td=""><td>-389</td><td>449</td><td></td><td></td><td></td><td>1</td></lc<></td></lc<>		8	<lc< td=""><td>-389</td><td>449</td><td></td><td></td><td></td><td>1</td></lc<>	-389	449				1
SIDE @ 2M	<lc< td=""><td>-10</td><td>21</td><td>T-LC</td><td>4085</td><td>871</td><td>8</td><td>10</td><td></td><td></td></lc<>	-10	21	T-LC	4085	871	8	10		
SIDE @ 2M	<lc< td=""><td>0</td><td></td><td> </td><td>3145</td><td>801</td><td>5</td><td>8</td><td>90</td><td>83</td></lc<>	0		 	3145	801	5	8	90	83
QC	<lc< td=""><td>0</td><td>21</td><td> </td><td>- 3173</td><td></td><td></td><td></td><td>\</td><td></td></lc<>	0	21	 	- 3173				\	
COLUMN E-18B			- 04	10	162	520				
FRONT @ 2M	<lc< td=""><td>0</td><td>21</td><td><lc< td=""><td>0</td><td>500</td><td> </td><td>· ·</td><td></td><td></td></lc<></td></lc<>	0	21	<lc< td=""><td>0</td><td>500</td><td> </td><td>· ·</td><td></td><td></td></lc<>	0	500		· ·		
BACK @ 2M	<lc< td=""><td>0</td><td>21</td><td></td><td>-259</td><td>467</td><td></td><td></td><td></td><td></td></lc<>	0	21		-259	467				
SIDE @ 2M	<lc< td=""><td>-10</td><td>8</td><td></td><td>-239 -130</td><td>484</td><td></td><td></td><td></td><td></td></lc<>	-10	8		-239 -130	484				
SIDE @ 2M		67	54	<lc< td=""><td>-130</td><td>10.1</td><td></td><td></td><td></td><td></td></lc<>	-130	10.1				
COLUMN E-20A				+	-130	484	<u> </u>			
FRONT @ 1M		19	34		162	520				
BACK @ 1M	<lc< td=""><td>-10</td><td>8</td><td></td><td>-97</td><td>488</td><td></td><td></td><td></td><td></td></lc<>	-10	8		-97	488				
SIDE @ 1M	<lc< td=""><td>-10</td><td></td><td><lc< td=""><td>-97</td><td>500</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-10		<lc< td=""><td>-97</td><td>500</td><td></td><td></td><td></td><td></td></lc<>	-97	500				
SIDE @ 1M		19	34	<lc< td=""><td>U</td><td>- 500</td><td></td><td></td><td></td><td></td></lc<>	U	- 500				
COLUMN E-20B			<u> </u>	 	120	484				
FRONT @ 1M		19		<lc< td=""><td>-130 -162</td><td>480</td><td></td><td>1</td><td></td><td></td></lc<>	-130 -162	480		1		
BACK @ 1M	<lc< td=""><td>-10</td><td></td><td></td><td></td><td>436</td><td>_</td><td></td><td></td><td></td></lc<>	-10				436	_			
SIDE @ 1M	<lc< td=""><td>-10</td><td></td><td></td><td>-486</td><td>480</td><td></td><td>_</td><td></td><td></td></lc<>	-10			-486	480		_		
SIDE @ 1M	<lc< td=""><td>-10</td><td>8</td><td><lc< td=""><td>-162</td><td>400</td><td></td><td>_</td><td></td><td></td></lc<></td></lc<>	-10	8	<lc< td=""><td>-162</td><td>400</td><td></td><td>_</td><td></td><td></td></lc<>	-162	400		_		
COLUMN E-20A						496	+	_		
FRONT @ 2M	<lc< td=""><td>0</td><td></td><td></td><td>-32</td><td><u> </u></td><td></td><td></td><td></td><td></td></lc<>	0			-32	<u> </u>				
BACK @ 2M	<lc< td=""><td>-10</td><td></td><td>3 <lc< td=""><td>97</td><td></td><td></td><td>8 1</td><td>0 11</td><td>1 85</td></lc<></td></lc<>	-10		3 <lc< td=""><td>97</td><td></td><td></td><td>8 1</td><td>0 11</td><td>1 85</td></lc<>	97			8 1	0 11	1 85
SIDE @ 2M	<lc< td=""><td>-10</td><td>)</td><td>3 <lc< td=""><td>-227</td><td></td><td></td><td></td><td>-</td><td></td></lc<></td></lc<>	-10)	3 <lc< td=""><td>-227</td><td></td><td></td><td></td><td>-</td><td></td></lc<>	-227				-	
SIDE @ 2M	<lc< td=""><td>C</td><td>) 2</td><td>1 <lc< td=""><td>-65</td><td>492</td><td>-</td><td></td><td></td><td></td></lc<></td></lc<>	C) 2	1 <lc< td=""><td>-65</td><td>492</td><td>-</td><td></td><td></td><td></td></lc<>	-65	492	-			
COLUMN E-20B						1	_			
FRONT @ 2M		19		4 <lc< td=""><td>-130</td><td></td><td></td><td>_</td><td></td><td></td></lc<>	-130			_		
BACK @ 2M	<lc< td=""><td>(</td><td>) 2</td><td></td><td>-454</td><td></td><td></td><td></td><td></td><td></td></lc<>	() 2		-454					
SIDE @ 2M	<lc< td=""><td>-10</td><td></td><td>8 <lc< td=""><td>-97</td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-10		8 <lc< td=""><td>-97</td><td></td><td></td><td></td><td></td><td></td></lc<>	-97					
SIDE @ 2M	<lc< td=""><td>(</td><td>) 2</td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td></lc<>	() 2					-		
QC .	<lc< td=""><td>10</td><td>0 2</td><td>8 <lc< td=""><td></td><td>50</td><td>J </td><td></td><td></td><td></td></lc<></td></lc<>	10	0 2	8 <lc< td=""><td></td><td>50</td><td>J </td><td></td><td></td><td></td></lc<>		50	J			

Comments: SMEARS COUNTED 3-13-95. FRONT = NORTH SIDE .
COLUMN A= SMALLER COLUMN. COLUMN B= LARGER COLUMN.

Attachment 1: Bliss & Laughlin Steel Characterization Radiological Data

Bliss and Laughlin Radiological Data

	- 1 - 11 4 d	Analyte	Result	Error	Units	MDL	BNI Flag
ample Location	Date Collected	AM-241	2	0	PCI/G	2 35.2	N) N)
3LS001	3/4/95 3/4/95	K-40	0.29	9.9	PCI/G	<i>3</i> 5.∠ 3.9	UJ
3LS001	3/4/95	RA-226	3.9	0	PCI/G PCI/G	9.8	ΩĴ
BLS001	3/4/95	RA-228	9.8	0	PCI/G	9.8	ÜĴ
BLS001	3/4/95	TH-228	9.8	0	PCI/G	7.5	ÜĴ
BLS001	3/4/95	TH-232	7.5	0 ~~ F	PCI/G	0,36	Ĵ
BLS001	3/4/95	U-234 •	- 71.1	22.5	PCI/G	0.34	J
BLS001	3/4/95	U-235	4.1	1.7 23.2	PCI/G	0.28	J
BLS001 BLS001	3/4/95	U-238	- 73.3			0.4	UJ
	3/5/95	AM-241	0.4	0	PCI/G PCI/G	0.4 5.7	n)
BLS002	3/5/95	K-40	3.9	1.8	PCI/G	0.6	
BLS002	3/5/95	RA-226	1.1	0.22	PCI/G	1.7	UJ
BLS002	3/5/95	RA-228	1.7	0	PCI/G	1.7	ÜJ
BLS002	3/5/95	TH-228	1.7	0	PCI/G	0.9	ŪJ
BLS002	3/5/95	TH-232	0.67	0.44	PCI/G	0.11	U
BLS002	3/5/95	U-234	5.1	1.4	PCI/G	0.12	Ĵ
BLS002	3/5/95	U-235	0.29	0.18	PCI/G	0.05	
BLS002 BLS002	3/5/95	U-238	4.8	1.3			UJ
	3/5/95	AM-241	0.3	0	PCI/G	0.3 1.9	J
BLS003	3/5/95	K-40	8.4	_ 1	PCI/G PCI/G	0.28	•
BLS003	3/5/95	RA-226	0.53	0.1	PCI/G PCI/G	- 0.7	UJ
BLS003	3/5/95	RA-228	0.7	0	PCI/G	0.7	ับป
BLS003	3/5/95	TH-228	0.7	0	PCI/G	0.56	ŪĴ
BLS003	3/5/95	TH-232	0.56	0	PCI/G	0.17	Ĵ
BLS003	3/5/95	U-234	30.8	9.3	PCI/G	0.09	Ĵ
BLS003	3/5/95	U-235	1.1	0.5	PCI/G	2.6	
BLS003	3/5/95	U-238	23.5	6.1	F 0.70		
BLS003		AM-241	0.76	. 0	PCI/G	0.76	UJ J
BLS004	3/5/95	K-40	12.4	2.2	PCI/G	2.2	ÜJ
BLS004	3/5/95	RA-226	0.27	0.1	PCI/G	0.35	· UJ
BLS004	3/5/95	RA-228	1.1	0	PCI/G	1.1	UJ 03
BLS004	3/5/95	TH-228	1.1	0	PCI/G	1.1 0.92	
BLS004	3/5/95	TH-232	0.92	0.	PCI/G		
BLS004	3/5/95	U-234	- 89.9	35.6	PCI/G	0.24 0.5	
BLS004	3/5/95	U-235	6.2	2.9	PCI/G	0.3	
BLS004	3/5/95 3/5/95	U-238	9 0.5	35.9	PCI/G		
BLS004			0.33	0	PCI/G	0.33	
BLS005	3/5/95	AM-241 K-40	12.1	1.5	PCI/G	2.8	
BLS005	3/5/95	RA-226	1.3	0.17	PCI/G	0.4	
BLS005	3/5/95	RA-228	1.2	. 0	PCI/G	1.2	
BLS005	3/5/95	TH-228	1.2	0	PCI/G	1.2	•
BLS005	3/5/95	TH-232	0.87	0	PCI/G	0.87	
BLS005	3/5/95	U-234	- 5	1.5	PCI/G	0.12	-
BLS005	3/5/95	U-235	0.31	0.2	PCI/G	0.12 0.13	
BLS005	3/5/95	U-238	6	1.8	PCI/G	0.1	
BLS005	3/5/95			0	PCI/G	0.49	
BLS007	3/5/95	AM-241	0.49 18.3	2.8	PCI/G	3.8	
BLS007	3/5/95	K-40		0	PCI/G	0.7	
BLS007	3/5/95	RA-226	0.78 1.6	ŏ	PCI/G	1.0	
BLS007	3/5/95	RA-228	1.6	ŏ	PCI/G	1.4	
BLS007	3/5/95	TH-228	1.0	ŏ	PCI/G	1.	
BLS007 BLS007	3/5/95	TH-232	13.6	3.3	PCI/Ģ	0.0	
BLS007	3/5/95	U-234		0.25	PCI/G	0.0	
BLS007 BLS007	3/5/95	U-235	0.66 15.3	3.7	PCI/G	0.0	3.
	3/5/95	U-238	7 ~ . 4	U. 1			

Bliss and Laughlin Radiological Data

a la Legation	Date Collected	Analyte	Result	Error	Units	MDL	BNI Flag
BLS008 BLS008 BLS008 BLS008 BLS008 BLS008 BLS008 BLS008 BLS008	3/5/95 3/5/95 3/5/95 3/5/95 3/5/95 3/5/95 3/5/95 3/5/95 3/5/95	AM-241 K-40 RA-226 RA-228 TH-228 TH-232 U-234 U-235 U-238	1.8 2.6 3.2 8.2 8.2 5.7 96.6 5.4 101.3	0 7.6 0 0 0 0 32.8 2.3 34.4	PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G	1.8 26.6 3.2 8.2 8.2 5.7 0.32 0.23 0.18	1 1 1 1 1 1 1 1 1 1 1
BLS008 BLS009 BLS009 BLS009 BLS009 BLS009 BLS009 BLS009 BLS009	3/4/95 3/4/95 3/4/95 3/4/95 3/4/95 3/4/95 3/4/95 3/4/95	AM-241 K-40 RA-226 RA-228 TH-228 TH-232 U-234 U-235 U-238	0.48 28 1.3 1.6 1.6 1.2 1.6 0.06	0 3.1 0.22 0 0 0.22 0.59 0.09 0.53	PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G	0.48 2.1 0.58 1.6 1.6 0.79 0.12 0.14 0.07	ר ה ה ה ח
BLS009 BLS011 BLS011 BLS011 BLS011 BLS011 BLS011 BLS011 BLS011	3/5/95 3/5/95 3/5/95 3/5/95 3/5/95 3/5/95 3/5/95 3/5/95 3/5/95	AM-241 K-40 RA-226 RA-228 TH-228 TH-232 U-234 U-235 U-238	0.56 21.8 1.8 1.9 1.9 1.4 1.9 0.07	0 2.6 0.3 0 0 0 0,54 0.07	PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G	0.56 2.6 0.68 1.9 1.9 1.4 0.07 0.08 0.04	רח רמ רמ רמ רח
BLS011 BLS014 BLS014 BLS014 BLS014 BLS014 BLS014 BLS014 BLS014	2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95	AM-241 K-40 RA-226 RA-228 TH-228 TH-232 U-234 U-235 U-238	0.49 21.1 1 2.3 2.3 1.6 13 1.4	0 3.4 0 0 0 0 5.5 0.83 6.5	PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G	0.49 4.5 1 2.3 2.3 1.6 0.39 0.3 0.34	7 7 7 7 7 7
BLS014 BLS015 BLS015 BLS015 BLS015 BLS015 BLS015 BLS015	2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95	AM-241 K-40 RA-226 RA-228 TH-228 TH-232 U-234 U-235 U-238	0.64 17.8 1.2 2.7 2.7 2 12.4 0.69 11.8	0 3.7 0 0 0 0 5.3 0.53 5	PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G	0.64 7.2 1.2 2.7 2.7 2 0.27 0.39 0.16	7 7 7 7 7 7 7
BLS015 BLS016 BLS016 BLS016 BLS016 BLS016 BLS016 BLS016 BLS016 BLS016	2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95	AM-241 K-40 RA-226 RA-228 TH-228 TH-232 U-234 U-235 U-238	0.3 0.85 0.73 1.8 1.8 1.3 0.47	0 1.7 0 0 0 0 4.4 0.41 4.9	PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G	0.3 5.8 0.73 1.8 1.8 1.3 0.26 0.32	3 UJ 3 UJ 3 UJ 5 UJ 5 J

Bliss and Laughlin Radiological Data

Sample Location	Date Collected	Analyte	Result	Error	Units	MDL	BNI Flag	
BLS017 BLS017 BLS017 BLS017 BLS017 BLS017 BLS017 BLS017 BLS017	2/26/95 2/26/95 2/26/95 2/26/95 2/26/95 2/26/95 2/26/95 2/26/95	AM-241 K-40 RA-226 RA-228 TH-228 TH-232 U-234 U-235 U-238	37.2 21.9 23 39.2 39.2 35.1 24290 1026 23570	0 36.1 0 0 0 0 6664 443.6 6471	PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G	37.2 123 23 39.2 39.2 35.1 64.7 136.3 64.4	1 01 01 01 01	
BLS017 BLS018 BLS018 BLS018 BLS018 BLS018 BLS018 BLS018 BLS018	2/26/95 2/26/95 2/26/95 2/26/95 2/26/95 2/26/95 2/26/95 2/26/95 2/26/95	AM-241 K-40 RA-226 RA-228 TH-228 TH-232 U-234 U-235 U-238	2.4 12.2 3.8 1.8 0.75 3.8 1220 41.8	0 2.5 0.39 0 1.7 1.6 490.8 84.2 488.7	PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G	2.4 5.8 1.2 1.8 1.8 1.1 91.9 113.3 91.5	7 7 7 7	

Data Qualifier Flags

ī Esti	nate, qualitatively correct but quantitatively suspe	ect
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Reject, data are not suitable for any purpose. R

Undetected-estimated. UJ

Undetected. The blank's result is equal to the detection limit, or above U the detection limit and the results of the sample are less than 5 times the blank's result.

Attachment 2: Bliss & Laughlin Steel Characterization Chemical Data

Bliss and Laughlin Chemical Data

	Date Collected	Analyte	Result	Units	BNI Flag	Lab Flag	DL	Matrix
Sample Location		1,1-Dichloroethene	0.05	mg/l		U	0.05	W
3LS013	3/9/95	Chlorobenzene	0.05	mg/l		U	0.05	W
3LS013	3/9/95	Vinyl Chloride	0.1	mg/l		U	0.1	W
BLS013	3/9/95	•	0.05	mg/l		U	0.05	W
BLS013	3/9/95	Chloroform	0.05	mg/l		U	0.05	W
BLS013	3/9/95	1,2-Dichloroethane	0.1	mg/l		U	0.1	W
BLS013	3/9/95	2-Butanone	0.05	mg/l		U	0.05	W
BLS013	3/9/95	Carbon Tetrachloride	0.05	mg/l		U	0.05	W
BLS013	3/9/95	Trichloroethene	0.05	mg/l		U	0.05	W
BLS013	3/9/95	Benzene	0.05	mg/l		U	0.05	W
BLS013	3/9/95	Tetrachloroethene	2.5	ug/I	UJ	U	2.5	W
BLS013	3/10/95	Silver, TCLP Leachate	0.1	ug/l		U	0.1	W
BLS013	3/10/95	Mercury, TCLP Leachate	0.5	ug/l		U	0.5	W
BLS013	3/10/95	alpha-Chiordane	0.5	ug/l		U	0.5	W
BLS013	3/10/95	Heptachlor	44.4	ug/l		U	44.4	W
BLS013	3/10/95	Selenium, TCLP Leachate	20.5	ug/l	UJ	U	20.5	W
BLS013	3/10/95	Lead, TCLP Leachate		_	0.5	U	0.5	W
BLS013	3/10/95	gamma-Chlordane	0.5	ug/l		=	2.9	W
BLS013	3/10/95	Chromium, TCLP Leachate	17.7	ug/l		U	3.5	W
BLS013	3/10/95	Cadmium, TCLP Leachate	3.5	ug/l		U	0.5	W
BLS013	3/10/95	gamma-BHC (Lindane)	0.5	ug/l		Ü	25.5	W
BLS013	3/10/95	Arsenic, TCLP Leachate	25.5	ug/l		Ü	0.1	W
BLS013	3/10/95	1,4-Dichlorobenzene	0.1	mg/l		Ü	5	W
BLS013	3/10/95	2,4,5-T	5	ug/l		U	5	W
	3/10/95	2,4,5-TP (Silvex)	5	ug/l		= .	2.8	w
BLS013	3/10/95	Barium, TCLP Leachate	866	ug/l	J	U U	0.1	W
BLS013	3/10/95	Nitrobenzene	0.1	mg/l		U	0.5	W
BLS013	3/10/95	Pentachlorophenol	0.5	mg/l			0.1	W
BLS013	3/10/95	Hexachiorobenzene	0.1	mg/l		U	0.1	W
BLS013	3/10/95	2,4-Dinitrotoluene	0.1	mg/l		U	0.5	w
BLS013	3/10/95	2,4,5-Trichlorophenol	0.5	mg/l		U	0.5	w
BLS013	3/10/95	Heptachlor Epoxide	0.5	ug/l		U		W
BLS013	3/10/95	Hexachlorobutadiene	0.1	mg/l		U	0.1	W
BLS013		Endrin	1	ug/l		U	1	
BLS013	3/10/95	Hexachioroethane	0.1	mg/l		U	0.1	W
BLS013	3/10/95	3- and/or 4-Methylphenol	0.1	mg/l		U	0.1	. W
BLS013	3/10/95	2-Methylphenol	0.1	mg/		· U	0.1	· W
BLS013	3/10/95		0.1	mg/	l UJ	U	0.1	W
BLS013	3/10/95	Pyridine	10	ug/l		U	10	W
BLS013	3/10/95	2,4-D	10	ug/l		U	10	W
BLS013	3/10/95	Toxaphene	5			U _.	5	W
BLS013	3/10/95 3/10/95	Methoxychlor 2,4,6-Trichlorophenol	0.1	mg/		Ú	0.1	W

Attachment 3:
DOE 5400.5, Figure IV-1
Surface Contamination Guidelines

Figure IV-1 Surface Contamination Guidelines

	Allowable To	tal Residual Su (dpm/100 c	urface Contamination
Radionuclides2/	Average3/.4/	Maximum ² /·5/	Removable4/.6/
Transuranics, I-125, I-129, Ra-226, Ac-227, Ra-228, Th-228, Th-230, Pa-231.	RESERVED	RESERVED	RESERVED
Th-Natural, Sr-90, I-126, I-131, I-133, Ra-223, Ra-224, U-232, Th-232.	1,000	3,000	200
U-Natural, U-235, U-238, and associated decay product, alpha emitters.	5,000	15,000	1,000
Beta-gamma emitters (radionuclides with decay modes other than alpha emission or spontaneous fission) except Sr-90 and others noted above. ⁷	5,000	15,000	1,000

As used in this table, dpm (disintegrations per minute) means the rate of emission by radioactive material as determined by correcting the counts per minute measured by an appropriate detector for background, efficiency, and geometric factors associated with the instrumentation.

Where surface contamination by both alpha- and beta-gamma-emitting radionuclides exists, the limits established for alpha- and beta-gamma-emitting radionuclides should apply independently.

Measurements of average contamination should not be averaged over an area of more than 1 $\rm m^2$. For objects of less surface area, the average should be derived for each such object.

The average and maximum dose rates associated with surface contamination resulting from beta-gamma emitters should not exceed 0.2 mrad/h and 1.0 mrad/h, respectively, at 1 cm.

^{1/2} The maximum contamination level applies to an area of not more than 100 cm².

Attachment 4: Bliss & Laughlin Steel Characterization 5-point Survey Data Special Finishing Area,

Survey of Elevated Locations in the Special finishing Area Identified by Floor Monitor Scans,

5-point Survey of Area in Grid E16

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Ţ			DIRECT					ALDU		SQ CM	BE	TA-GAMMA/1	00 SQ	СМ
	ALPHA	100 5			AMMA/10					STD	1 55	SMPL	STD	
OCATION/ITEM	SMPL	- [STD		1PL	STE	*	SM		DEV		DPM	DEV	
COORDINATES	DPM	. [DEV	DI	PM	DE/		DF	(V)	DEV	1			
V-0.5 E-0.5		29	37		492		484				<lc< td=""><td>-4</td><td></td><td>77</td></lc<>	-4		77
N-0.5 E-1.5		29	37		751		510		<u>-1</u>		<lc< td=""><td></td><td></td><td>76</td></lc<>			76
N-0.5 E0.5	l	29	37		674	<u> </u>	503		2					72
N-0.5 E1.5	<lc< td=""><td>-7</td><td>7</td><td></td><td>907</td><td>L</td><td>525</td><td><lc_< td=""><td><u>-1</u></td><td></td><td>\ <lc< td=""><td>-50</td><td> </td><td></td></lc<></td></lc_<></td></lc<>	-7	7		907	L	525	<lc_< td=""><td><u>-1</u></td><td></td><td>\ <lc< td=""><td>-50</td><td> </td><td></td></lc<></td></lc_<>	<u>-1</u>		\ <lc< td=""><td>-50</td><td> </td><td></td></lc<>	-50	 	
N-0.5 E10.5	1	39	41	<lc< td=""><td>0</td><td></td><td>431</td><td></td><td></td><td></td><td>╂</td><td></td><td></td><td></td></lc<>	0		431				╂			
	 	20	32	<lc< td=""><td>155</td><td></td><td>449</td><td></td><td></td><td>ļ</td><td>-</td><td></td><td> </td><td></td></lc<>	155		449			ļ	-		 	
N-0.5 E11.5	<lc< td=""><td>2</td><td>19</td><td></td><td>466</td><td>3</td><td>482</td><td></td><td></td><td></td><td>┨—</td><td></td><td></td><td></td></lc<>	2	19		466	3	482				┨—			
N-0.5 E12.5	<lc< td=""><td>11</td><td></td><td><lc< td=""><td>233</td><td>3</td><td>457</td><td></td><td></td><td></td><td>1-</td><td></td><td></td><td></td></lc<></td></lc<>	11		<lc< td=""><td>233</td><td>3</td><td>457</td><td></td><td></td><td></td><td>1-</td><td></td><td></td><td></td></lc<>	233	3	457				1-			
N-0.5 E13.5	\	20	32		389)	474							
N-0.5 E14.5	╫	48		<lc< td=""><td>285</td><td>5</td><td>463</td><td></td><td></td><td></td><td></td><td></td><td>1.</td><td>7</td></lc<>	285	5	463						1.	7
N-0.5 E15.5	#	20	32		777		513	<lc< td=""><td>-1</td><td></td><td>) <l< td=""><td>c 8</td><td>4</td><td></td></l<></td></lc<>	-1) <l< td=""><td>c 8</td><td>4</td><td></td></l<>	c 8	4	
N-0.5 E16.5	1 -	11		<lc< td=""><td>78</td><td>_</td><td>440</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td>7</td></lc<>	78	_	440				1			 7
N-0.5 E17.5	<lc< td=""><td>29</td><td>37</td><td>120</td><td>674</td><td></td><td>503</td><td><lc< td=""><td></td><td></td><td>0 <l< td=""><td>c -59</td><td>' </td><td>7</td></l<></td></lc<></td></lc<>	29	37	120	674		503	<lc< td=""><td></td><td></td><td>0 <l< td=""><td>c -59</td><td>' </td><td>7</td></l<></td></lc<>			0 <l< td=""><td>c -59</td><td>' </td><td>7</td></l<>	c -59	' 	7
N-0.5 E18.5				<lc< td=""><td>337</td><td></td><td>468</td><td></td><td></td><td></td><td></td><td></td><td>↓</td><td></td></lc<>	337		468						↓	
N-0.5 E19.5		20			415		476						<u> </u>	
N-0.5 E2.5		39	41	<lc< td=""><td>52</td><td></td><td>437</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	52		437							
N-0.5 E20.5	<lc< td=""><td>-7</td><td></td><td></td><td>36</td><td></td><td>471</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-7			36		471							
N-0.5 E21.5	<lc< td=""><td>11</td><td></td><td><lc< td=""><td>44</td><td></td><td>479</td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	11		<lc< td=""><td>44</td><td></td><td>479</td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	44		479	-						
N-0.5 E3.5		29	37		36		471							
N-0.5 E4.5		39		<lc< td=""><td>75</td><td></td><td></td><td><lc< td=""><td></td><td>2</td><td>6 <l< td=""><td>.c -5</td><td>)</td><td>7</td></l<></td></lc<></td></lc<>	75			<lc< td=""><td></td><td>2</td><td>6 <l< td=""><td>.c -5</td><td>)</td><td>7</td></l<></td></lc<>		2	6 <l< td=""><td>.c -5</td><td>)</td><td>7</td></l<>	.c -5)	7
N-0.5 E5.5	<lc< td=""><td>11</td><td>27</td><td></td><td></td><td></td><td>443</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td></lc<>	11	27				443				1			
N-0.5 E6.5	<lc< td=""><td>11</td><td></td><td><lc< td=""><td>10</td><td></td><td></td><td><lc< td=""><td></td><td>2</td><td>6 <l< td=""><td>c -5</td><td>4</td><td>Ī</td></l<></td></lc<></td></lc<></td></lc<>	11		<lc< td=""><td>10</td><td></td><td></td><td><lc< td=""><td></td><td>2</td><td>6 <l< td=""><td>c -5</td><td>4</td><td>Ī</td></l<></td></lc<></td></lc<>	10			<lc< td=""><td></td><td>2</td><td>6 <l< td=""><td>c -5</td><td>4</td><td>Ī</td></l<></td></lc<>		2	6 <l< td=""><td>c -5</td><td>4</td><td>Ī</td></l<>	c -5	4	Ī
N-0.5 E7.5	<lc< td=""><td>2</td><td>19</td><td></td><td>95</td><td></td><td></td><td></td><td></td><td>-</td><td>_</td><td></td><td></td><td></td></lc<>	2	19		95					-	_			
N-0.5 E8.5	<lc< td=""><td>2</td><td></td><td><lc< td=""><td>18</td><td></td><td>451</td><td>_</td><td></td><td></td><td>-</td><td></td><td></td><td></td></lc<></td></lc<>	2		<lc< td=""><td>18</td><td></td><td>451</td><td>_</td><td></td><td></td><td>-</td><td></td><td></td><td></td></lc<>	18		451	_			-			
N-0.5 E9.5	<lc< td=""><td>-7</td><td></td><td></td><td>36</td><td></td><td>471</td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc<>	-7			36		471						1	
N-1.0 E-1.0	<lc< td=""><td>11</td><td></td><td></td><td>51</td><td></td><td>487</td><td></td><td></td><td>5</td><td>8 <1</td><td>°c 1</td><td>7 .</td><td></td></lc<>	11			51		487			5	8 <1	°c 1	7 .	
N-1.0 E-2.0	<lc< td=""><td>11</td><td>27</td><td>'II</td><td>70</td><td></td><td>505</td><td></td><td></td><td>5</td><td></td><td></td><td>`</td><td></td></lc<>	11	27	'II	70		505			5			`	
N-1.0 E0.0	<lc< td=""><td>2</td><td>19</td><td></td><td>41</td><td></td><td>476</td><td></td><td></td><td>_</td><td></td><td></td><td>_</td><td></td></lc<>	2	19		41		476			_			_	
N-1.0 E1.0		20		2 <lc< td=""><td></td><td>2</td><td>437</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		2	437							
N-1.0 E10.0	<lc< td=""><td>2</td><td></td><td></td><td>51</td><td></td><td>487</td><td>_</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	2			51		487	_						
N-1.0 E10.0		29		7 <lc< td=""><td>28</td><td>35</td><td>463</td><td></td><td></td><td></td><td>_</td><td>Lc -2</td><td></td><td></td></lc<>	28	35	463				_	Lc -2		
N-1.0 E11.0		20			70	00		<lc< td=""><td></td><td>2</td><td>6 <</td><td>LC -2</td><td>7</td><td></td></lc<>		2	6 <	LC -2	7	
	- <lc< td=""><td>11</td><td></td><td></td><td>4</td><td>15</td><td>476</td><td>3</td><td></td><td></td><td>_#_</td><td></td><td></td><td></td></lc<>	11			4	15	476	3			_#_			
N-1.0 E13.0				9 < Lc	20	07	454	4						
N-1.0 E14.0	<lc< td=""><td>20</td><td>- </td><td>2 <lc< td=""><td>10</td><td>04</td><td>443</td><td>3</td><td></td><td></td><td> </td><td></td><td></td><td></td></lc<></td></lc<>	20	-	2 <lc< td=""><td>10</td><td>04</td><td>443</td><td>3</td><td></td><td></td><td> </td><td></td><td></td><td></td></lc<>	10	04	443	3						
N-1.0 E15.0	- - -	- 2		7 <lc< td=""><td>33</td><td>37</td><td>468</td><td>8</td><td></td><td></td><td> _</td><td></td><td></td><td></td></lc<>	33	37	468	8			_			
N-1.0 E16.0	<lc< td=""><td></td><td>· • · · · · · · · · · · · · · · · · · ·</td><td>9</td><td></td><td>40</td><td>47</td><td>9</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		· • · · · · · · · · · · · · · · · · · ·	9		40	47	9						
N-1.0 E17.0	<lc< td=""><td>20</td><td></td><td>2 < Lc</td><td></td><td>04</td><td>41</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	20		2 < Lc		04	41							
N-1.0 E18.0	_			7 <lc< td=""><td></td><td>63</td><td>47</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		63	47							
N-1.0 E19.0	<lc< td=""><td>1</td><td></td><td>7</td><td></td><td>40</td><td>47</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	1		7		40	47							
N-1.0 E2.0	<lc< td=""><td></td><td></td><td></td><td></td><td>89</td><td>47</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>					89	47							
N-1.0 E20.0	<lc< td=""><td>1</td><td></td><td>7</td><td></td><td>89</td><td>47</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	1		7		89	47							
N-1.0 E21.0	<lc< td=""><td></td><td></td><td>9</td><td></td><td>81</td><td>45</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			9		81	45							
N-1.0 E22.0		2		7 <lc< td=""><td></td><td></td><td>43</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			43							
N-1.0 E3.0	<lc< td=""><td></td><td></td><td>7 <lc< td=""><td></td><td>26</td><td>48</td><td></td><td></td><td>_</td><td></td><td></td><td></td><td></td></lc<></td></lc<>			7 <lc< td=""><td></td><td>26</td><td>48</td><td></td><td></td><td>_</td><td></td><td></td><td></td><td></td></lc<>		26	48			_				
N-1.0 E4.0	<lc< td=""><td></td><td></td><td>9</td><td></td><td>66</td><td>48</td><td></td><td></td><td></td><td>- </td><td></td><td></td><td></td></lc<>			9		66	48				-			
N-1.0 E5.0	<lc< td=""><td></td><td></td><td>7 <lc< td=""><td></td><td>52</td><td></td><td></td><td></td><td></td><td></td><td>·</td><td>1</td><td></td></lc<></td></lc<>			7 <lc< td=""><td></td><td>52</td><td></td><td></td><td></td><td></td><td></td><td>·</td><td>1</td><td></td></lc<>		52						·	1	
N-1.0 E6.0	<lc< td=""><td></td><td>2 1</td><td>9</td><td></td><td>18</td><td>48</td><td></td><td></td><td></td><td></td><td></td><td>\neg</td><td></td></lc<>		2 1	9		18	48						\neg	
N-1.0 E7.0	<lc< td=""><td></td><td>.7</td><td>7</td><td></td><td>15</td><td>47</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		.7	7		15	47							
N-1.0 E8.0	<lc< td=""><td></td><td>.7</td><td>7</td><td></td><td>89</td><td>47</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		.7	7		89	47							
N-1.0 E0.0	- 			15 <lc< td=""><td></td><td>-52</td><td>42</td><td>25</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		-52	42	25						
N-1.0 E9.0		NA	NA		NA		VA							
N-1.5 E-0.5		NA NA	NA	-11	NA	1	NA							
N-1.5 E-1.5		NA NA	NA NA		NA	TI.	NA						-+-	
N-1.5 E0.5			NA NA		NA		NA						\dashv	
N-1.5 E1.5		NA_					NA							
N 1 5 E 10 5		NA	NA al level of		NA			no obo	ie hac	karound				

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

,		DIDECT				TF	RANSFER	ABLE			
		DIRECT	BETA-GAM	MA/100 S	O CM	ALPHA/100		BETA	A-GAMMA/1		М
	ALPHA/100		SMPL			SMPL	STD	*	J	STD	
LOCATION/ITEM	SMPL	STD	DPM	DE		DPM	DEV		DPM	DEV	\dashv
COORDINATES	DPM	DEV	NA NA	NA NA							
N-1.5 E11.5	NA	NA	NA NA	NA NA							
N-1.5 E12.5	NA	NA	NA NA	- NA							
N-1.5 E13.5	NA	NA	11								
N-1.5 E14.5	NA	NA	NA NA					1			
N-1.5 E15.5	NA	NA	NA NA								
N-1.5 E16.5	NA	NA	NA NA					1			
N-1.5 E17.5	NA	NA	NA NA					1			
N-1.5 E18.5	NA	NA	NA NA					+			
N-1.5 E19.5	NA	NA	NA NA			······································		1			
N-1.5 E2.5	NA	NA	NA NA					1			
N-1.5 E20.5	NA	NA	N/					+			
N-1.5 E21.5	NA	NA	N/								
N-1.5 E3.5	NA	NA	N/								
N-1.5 E4.5	NA NA	NA	N/					-			
N-1.5 E5.5	NA NA	NA	N/					+		 	
N-1.5 E5.5	NA NA	NA	N/								
N-1.5 E6.5	NA NA	NA	N/	A NA	4					-	
N-1.5 E7.5	NA NA	NA NA	N/	A N	۸					 	
N-1.5 E8.5	NA NA	NA NA	N.	A N	4			_			
N-1.5 E9.5	NA NA	NA NA	N.	A N	٩					 	
N-2.0 E-1.0	NA NA	NA NA	N.		4			_			
N-2.0 E-2.0		NA NA	N		Ą						
N-2.0 E0.0	NA NA	NA NA	N								
N-2.0 E1.0	NA_		N							ļ	
N-2.0 E10.0	NA NA	NA									
N-2.0 E11.0	NA NA	NA		A N							
N-2.0 E12.0	NA	NA	11	A N							
N-2.0 E13.0	NA NA	NA		A N							
N-2.0 E14.0	NA	NA_									
N-2.0 E15.0	NA	NA	11								
N-2.0 E16.0	NA NA	NA			A						
N-2.0 E17.0	NA	NA				<u> </u>					
N-2.0 E18.0	NA	NA	11		IA .		_				
N-2.0 E19.0	NA	NA	. 11	<u> </u>	IA	<u> </u>		_			
N-2.0 E2.0	NA	NA			IA						
N-2.0 E20.0	NA	NA	11		IA	ļ					
N-2.0 E21.0	NA	NA	1		IA						
	NA	NA	1		1A					-	
N-2.0 E22.0	NA NA	NA			NA	ļ					
N-2.0 E3:0	NA NA	NA			۱A	<u> </u>		 		+	
N-2.0 E4.0	NA NA	NA NA		I AV	٧A	<u> </u>					
N-2.0 E5.0	NA NA	NA NA			VA.						
N-2.0 E6.0		NA NA			NA A			_			
N-2.0 E7.0	NA NA	NA NA			NA						
N-2.0 E8.0		NA NA	11		NA					- ·	
N-2.0 E9.0	NA		37	415	476	3					
N0.0 E-1.0		29	27	570	492						
N0.0 E-2.0	<lc_< td=""><td>11</td><td>20</td><td>544</td><td>457</td><td></td><td></td><td></td><td></td><td>-</td><td></td></lc_<>	11	20	544	457					-	
N0.0 E0.0	<lc< td=""><td>-4</td><td></td><td>803</td><td></td><td>4 <lc< td=""><td>2 .</td><td>6 <l< td=""><td>c</td><td>13</td><td></td></l<></td></lc<></td></lc<>	-4		803		4 <lc< td=""><td>2 .</td><td>6 <l< td=""><td>c</td><td>13</td><td></td></l<></td></lc<>	2 .	6 <l< td=""><td>c</td><td>13</td><td></td></l<>	c	13	
N0.0 E1.0		42	45	155	413						
N0.0 E10.0	<lc< td=""><td>6</td><td>27 <lc< td=""><td>259</td><td>42</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	6	27 <lc< td=""><td>259</td><td>42</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	259	42						
N0.0 E11.0	<lc< td=""><td>-4</td><td>20 <lc< td=""><td></td><td>42</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-4	20 <lc< td=""><td></td><td>42</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		42						
N0.0 E12.0	<lc< td=""><td>6</td><td>27 <lc< td=""><td>259</td><td>42</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	6	27 <lc< td=""><td>259</td><td>42</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	259	42						
N0.0 E13.0	<lc< td=""><td>15</td><td>33</td><td>492</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	15	33	492							
N0.0 E14.0	<lc< td=""><td>-4</td><td>20 <lc< td=""><td>155</td><td>41</td><td>-</td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-4	20 <lc< td=""><td>155</td><td>41</td><td>-</td><td></td><td></td><td></td><td></td><td></td></lc<>	155	41	-					
NO.0 E15.0	<lc< td=""><td>-13</td><td>10 < Lc</td><td>104</td><td>40</td><td>to il</td><td></td><td></td><td></td><td></td><td></td></lc<>	-13	10 < Lc	104	40	to il					

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

_							\neg		TRA	NSFER	AB	LE		
			DIRECT	5 F T A	-GAMMA/10	00 80 0	M	LPHA/			В	ETA-GAMN	/A/100	SQ CM
	ALPHA			BEIA		STD	141 /	SMPL		STD	T	SMPL	_	ΓD
OCATION/ITEM	SMPI	- 1	STD		SMPL	DEV	1	DPM		DEV		DPM	D	ΞV
COORDINATES	DPM	<u> </u>	DEV		DPM 492		51	D(101			T			
10.0 E16.0		33	41		285		28				1			
10.0 E17.0	<lc< td=""><td>15</td><td></td><td><lc< td=""><td>311</td><td></td><td>31</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td></lc<></td></lc<>	15		<lc< td=""><td>311</td><td></td><td>31</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td></lc<>	311		31				1			
10.0 E18.0		24	37	<lc< td=""><td></td><td><u> </u></td><td>54</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td></lc<>		<u> </u>	54				1			
10.0 E19.0	<lc< td=""><td>15</td><td>33</td><td></td><td>518</td><td>1</td><td>34</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td></lc<>	15	33		518	1	34				1			
10.0 E2.0	<lc< td=""><td>15</td><td>33</td><td><u> </u></td><td>337 155</td><td></td><td>13</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td></lc<>	15	33	<u> </u>	337 155		13				1			
NO.0 E20.0	<lc< td=""><td>6</td><td></td><td><lc< td=""><td>259</td><td>1</td><td>25</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td></lc<></td></lc<>	6		<lc< td=""><td>259</td><td>1</td><td>25</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td></lc<>	259	1	25				1			
NO.0 E21.0	<lc< td=""><td>-4</td><td></td><td><lc_< td=""><td></td><td></td><td>25</td><td></td><td></td><td></td><td>T</td><td></td><td></td><td></td></lc_<></td></lc<>	-4		<lc_< td=""><td></td><td></td><td>25</td><td></td><td></td><td></td><td>T</td><td></td><td></td><td></td></lc_<>			25				T			
NO.0 E22.0	<lc< td=""><td>6</td><td>27</td><td><lc< td=""><td>259</td><td></td><td>46</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td></lc<></td></lc<>	6	27	<lc< td=""><td>259</td><td></td><td>46</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td></lc<>	259		46				1			
N0.0 E3.0		61	52		440		54				1			
N0.0 E4.0	<lc< td=""><td>6</td><td>1</td><td>ļ</td><td>518</td><td></td><td>49</td><td></td><td></td><td>······</td><td>+</td><td></td><td></td><td></td></lc<>	6	1	ļ	518		49			······	+			
NO.0 E5.0	<lc< td=""><td>15</td><td></td><td> </td><td>466</td><td></td><td></td><td></td><td></td><td></td><td>+</td><td></td><td></td><td></td></lc<>	15		 	466						+			
N0.0 E6.0		24		ļ	492		151 184 <	Lc	-1		0 <	Lc	46	80
N0.0 E7.0		33			803		151	·LU						
N0.0 E8.0	<lc< td=""><td>-13</td><td></td><td></td><td>492</td><td></td><td>146</td><td></td><td></td><td></td><td>+</td><td></td><td></td><td></td></lc<>	-13			492		146				+			
N0.0 E9.0	<lc< td=""><td>6</td><td></td><td></td><td>440</td><td></td><td>176</td><td></td><td></td><td></td><td>+</td><td></td><td></td><td></td></lc<>	6			440		176				+			
N0.5 E-0.5		29			415		474				-			
N0.5 E-1.5	<lc< td=""><td>-7</td><td></td><td></td><td>389</td><td></td><td></td><td></td><td></td><td></td><td>+</td><td></td><td></td><td></td></lc<>	-7			389						+			
N0.5 E0.5	<lc< td=""><td>-4</td><td></td><td></td><td>44</td><td></td><td>446</td><td></td><td></td><td>-</td><td>+</td><td></td><td></td><td></td></lc<>	-4			44		446			-	+			
N0.5 E1.5		33		<lc< td=""><td></td><td></td><td>431</td><td></td><td></td><td></td><td>╅</td><td></td><td></td><td></td></lc<>			431				╅			
N0.5 E10.5	<lc< td=""><td>15</td><td></td><td><lc< td=""><td>20</td><td></td><td>419</td><td></td><td></td><td>-</td><td>+</td><td></td><td></td><td></td></lc<></td></lc<>	15		<lc< td=""><td>20</td><td></td><td>419</td><td></td><td></td><td>-</td><td>+</td><td></td><td></td><td></td></lc<>	20		419			-	+			
N0.5 E11.5	<lc< td=""><td>15</td><td></td><td></td><td>38</td><td></td><td>440</td><td></td><td></td><td> </td><td></td><td></td><td></td><td></td></lc<>	15			38		440			 				
N0.5 E12.5		42		<lc< td=""><td></td><td></td><td>416</td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td></lc<>			416				-			
N0.5 E13.5	<lc< td=""><td>-4</td><td></td><td>) < Lc</td><td>2</td><td></td><td>397</td><td></td><td></td><td></td><td>+</td><td></td><td></td><td></td></lc<>	-4) < Lc	2		397				+			
N0.5 E14.5		24			59	<u> </u>	463			-	\dashv			
N0.5 E15.5	<lc< td=""><td>15</td><td></td><td>3 < Lc</td><td></td><td></td><td>409</td><td></td><td></td><td> </td><td></td><td></td><td></td><td></td></lc<>	15		3 < Lc			409			 				
N0.5 E16.5	<lc< td=""><td>(</td><td></td><td></td><td>67</td><td></td><td>471</td><td></td><td></td><td> </td><td>-†</td><td></td><td></td><td></td></lc<>	(67		471			 	-†			
N0.5 E17.5		42			51		454			┼──	-			
N0.5 E18.5		33		1 < L	10	<u> </u>	406				-			
N0.5 E19.5	· <lc td="" ·<=""><td>1:</td><td></td><td></td><td>57</td><td></td><td>460</td><td></td><td></td><td>+</td><td>\dashv</td><td></td><td></td><td></td></lc>	1:			57		460			+	\dashv			
N0.5 E2.5	<lc< td=""><td>1:</td><td>5 3</td><td>3</td><td>72</td><td></td><td>476</td><td></td><td></td><td> </td><td>\dashv</td><td></td><td></td><td></td></lc<>	1:	5 3	3	72		476			 	\dashv			
N0.5 E20.5	<lc< td=""><td>1</td><td></td><td>3 <l0< td=""><td></td><td></td><td>419</td><td></td><td></td><td>┧───</td><td>-#</td><td></td><td></td><td></td></l0<></td></lc<>	1		3 <l0< td=""><td></td><td></td><td>419</td><td></td><td></td><td>┧───</td><td>-#</td><td></td><td></td><td></td></l0<>			419			┧───	-#			
N0.5 E21.5	<lc< td=""><td>1</td><td>5 3</td><td>3</td><td>38</td><td></td><td>440</td><td></td><td></td><td>+</td><td>- </td><td></td><td></td><td></td></lc<>	1	5 3	3	38		440			+	-			
N0.5 E3.5	<lc< td=""><td>-</td><td>4 2</td><td>0 </td><td>49</td><td></td><td>451</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-	4 2	0	49		451							
N0.5 E4.5		3	3 4			70	460							
N0.5 E5.5	<lc< td=""><td></td><td></td><td>7</td><td></td><td>14</td><td>457</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			7		14	457							
N0.5 E6.5	1	3	3 4	1 <l< td=""><td>c 2</td><td>59</td><td>425</td><td></td><td></td><td>2</td><td>ᇹ</td><td><lc< td=""><td>-46</td><td>7</td></lc<></td></l<>	c 2	59	425			2	ᇹ	<lc< td=""><td>-46</td><td>7</td></lc<>	-46	7
N0.5 E7.5	<lc< td=""><td>1</td><td>5 3</td><td>3</td><td>142</td><td></td><td></td><td><lc< td=""><td></td><td>4</td><td></td><td><u> </u></td><td></td><td></td></lc<></td></lc<>	1	5 3	3	142			<lc< td=""><td></td><td>4</td><td></td><td><u> </u></td><td></td><td></td></lc<>		4		<u> </u>		
N0.5 E8.5		6	51 5	2		44	457				-	<lc< td=""><td>0</td><td></td></lc<>	0	
N0.5 E9.5	<lc< td=""><td></td><td></td><td>0</td><td></td><td>07</td><td>495</td><td></td><td></td><td>5</td><td>- 9</td><td></td><td></td><td></td></lc<>			0		07	495			5	- 9			
N1.0 E-1.0	<lc< td=""><td></td><td>2 1</td><td>9 <l< td=""><td></td><td>33</td><td>457</td><td>41 -</td><td></td><td>4</td><td>0</td><td></td><td>71</td><td>1</td></l<></td></lc<>		2 1	9 <l< td=""><td></td><td>33</td><td>457</td><td>41 -</td><td></td><td>4</td><td>0</td><td></td><td>71</td><td>1</td></l<>		33	457	41 -		4	0		71	1
N1.0 E-2.0	<lc< td=""><td></td><td>1 2</td><td>7</td><td></td><td>74</td><td></td><td><lc< td=""><td></td><td>1</td><td></td><td></td><td></td><td></td></lc<></td></lc<>		1 2	7		74		<lc< td=""><td></td><td>1</td><td></td><td></td><td></td><td></td></lc<>		1				
N1.0 E0.0	<lc< td=""><td></td><td></td><td>0 <l< td=""><td></td><td>81</td><td>416</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<></td></lc<>			0 <l< td=""><td></td><td>81</td><td>416</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<>		81	416							
N1.0 E1.0	-#- 	- 2	· 1	37		49	805			+				
N1.0 E10.0			33 4	11 <l< td=""><td></td><td>04</td><td>406</td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td></l<>		04	406			-				
N1.0 E10.0				37 <l< td=""><td></td><td>11</td><td>431</td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td><td></td></l<>		11	431					<u> </u>		
N1.0 E12.0			42	15		18	454							
N1.0 E12.0	<lc< td=""><td></td><td>15</td><td>33 <l< td=""><td></td><td>85</td><td>428</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<></td></lc<>		15	33 <l< td=""><td></td><td>85</td><td>428</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<>		85	428							
N1.0 E14.0	<lc< td=""><td></td><td></td><td>27</td><td>ϵ</td><td>74</td><td>471</td><td></td><td></td><td></td><td></td><td></td><td></td><td> </td></lc<>			27	ϵ	74	471							
	-11-5			41		92	451							
N1.0 E15.0	<lc< td=""><td></td><td></td><td>33 <1</td><td>_c 1</td><td>30</td><td>409</td><td></td><td></td><td></td><td></td><td></td><td></td><td> </td></lc<>			33 <1	_c 1	30	409							
N1.0 E16.0	<lc< td=""><td></td><td></td><td>10 <</td><td></td><td>04</td><td>406</td><td>_</td><td></td><td></td><td></td><td><u> </u></td><td></td><td></td></lc<>			10 <		04	406	_				<u> </u>		
N1.0 E17.0	1-20			37		96	463			_		CLC	-21	
N1.0 E18.0	<lc< td=""><td></td><td></td><td>20 <</td><td>_c</td><td>155</td><td></td><td><lc< td=""><td></td><td>2</td><td></td><td><lc< td=""><td>-<u></u></td><td></td></lc<></td></lc<></td></lc<>			20 <	_c	155		<lc< td=""><td></td><td>2</td><td></td><td><lc< td=""><td>-<u></u></td><td></td></lc<></td></lc<>		2		<lc< td=""><td>-<u></u></td><td></td></lc<>	- <u></u>	
N1.0 E19.0 N1.0 E2.0	<lc< td=""><td></td><td></td><td>20</td><td>1.</td><td>114</td><td>515</td><td><lc< td=""><td></td><td>2</td><td>Ö</td><td><lc< td=""><td></td><td><u> </u></td></lc<></td></lc<></td></lc<>			20	1.	114	515	<lc< td=""><td></td><td>2</td><td>Ö</td><td><lc< td=""><td></td><td><u> </u></td></lc<></td></lc<>		2	Ö	<lc< td=""><td></td><td><u> </u></td></lc<>		<u> </u>

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

			DIDECT					TR	ANSFER	ABLE		
			DIRECT	5574	GAMMA/10	0 SO CM	ALPHA			BETA-G	AMMA/10	00 SQ CM
							SMP		STD	SM		STD
OCATION/ITEM	SM		STD		=	STD	DPM		DEV	DP	1	DEV
COORDINATES	DP	M	DEV		1 111	DEV	DEN	<u> </u>	DLY			
N1.0 E20.0	<lc< td=""><td>-4</td><td></td><td><lc< td=""><td>26</td><td>397</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-4		<lc< td=""><td>26</td><td>397</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	26	397						
11.0 E21.0	<lc< td=""><td>15</td><td>33</td><td></td><td>492</td><td>451</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	15	33		492	451						
N1.0 E22		42		<lc< td=""><td>181</td><td>416</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	181	416						
11.0 E3.0	<lc< td=""><td>15</td><td>33</td><td></td><td>518</td><td>454</td><td></td><td></td><td></td><td></td><td></td><td>····································</td></lc<>	15	33		518	454						····································
V1.0 E4.0	<lc< td=""><td>-4</td><td></td><td><lc< td=""><td>233</td><td>422</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-4		<lc< td=""><td>233</td><td>422</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	233	422						
N1.0 E5.0	<lc< td=""><td>15</td><td>33</td><td></td><td>544</td><td>457</td><td></td><td>2</td><td>6</td><td><lc< td=""><td>-46</td><td>73</td></lc<></td></lc<>	15	33		544	457		2	6	<lc< td=""><td>-46</td><td>73</td></lc<>	-46	73
V1.0 E6.0	<lc< td=""><td>-4</td><td>20</td><td></td><td>777</td><td>482</td><td><lc< td=""><td></td><td></td><td>720</td><td></td><td></td></lc<></td></lc<>	-4	20		777	482	<lc< td=""><td></td><td></td><td>720</td><td></td><td></td></lc<>			720		
N1.0 E7.0		24	37		674	471						
V1.0 E8.0	<lc< td=""><td>6</td><td>27</td><td><lc< td=""><td>104</td><td>406</td><td></td><td></td><td></td><td> </td><td>-</td><td></td></lc<></td></lc<>	6	27	<lc< td=""><td>104</td><td>406</td><td></td><td></td><td></td><td> </td><td>-</td><td></td></lc<>	104	406				 	-	
N1.0 E9.0	<lc< td=""><td>15</td><td>33</td><td><lc< td=""><td>233</td><td>422</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	15	33	<lc< td=""><td>233</td><td>422</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	233	422						
N1.5 E-0.5	<lc< td=""><td>-7</td><td>7</td><td></td><td>492</td><td>484</td><td>+</td><td></td><td>ļ</td><td> </td><td></td><td></td></lc<>	-7	7		492	484	+		ļ	 		
N1.5 E-1.5	<lc< td=""><td>2</td><td>19</td><td><lc< td=""><td>78</td><td>440</td><td></td><td></td><td>ļ</td><td></td><td></td><td></td></lc<></td></lc<>	2	19	<lc< td=""><td>78</td><td>440</td><td></td><td></td><td>ļ</td><td></td><td></td><td></td></lc<>	78	440			ļ			
N1.5 E0.5	<lc< td=""><td>-9</td><td>35</td><td><lc< td=""><td>134</td><td>442</td><td></td><td></td><td>ļ</td><td>ļ</td><td></td><td></td></lc<></td></lc<>	-9	35	<lc< td=""><td>134</td><td>442</td><td></td><td></td><td>ļ</td><td>ļ</td><td></td><td></td></lc<>	134	442			ļ	ļ		
N1.5 E1.5	<lc< td=""><td>18</td><td>47</td><td><lc< td=""><td>-134</td><td>410</td><td></td><td></td><td> </td><td>10</td><td>-59</td><td>69</td></lc<></td></lc<>	18	47	<lc< td=""><td>-134</td><td>410</td><td></td><td></td><td> </td><td>10</td><td>-59</td><td>69</td></lc<>	-134	410			 	10	-59	69
N1.5 E10.5	<lc< td=""><td>28</td><td>50</td><td></td><td>857</td><td></td><td><lc< td=""><td>-1</td><td><u> </u></td><td><lc< td=""><td>-58</td><td><u></u></td></lc<></td></lc<></td></lc<>	28	50		857		<lc< td=""><td>-1</td><td><u> </u></td><td><lc< td=""><td>-58</td><td><u></u></td></lc<></td></lc<>	-1	<u> </u>	<lc< td=""><td>-58</td><td><u></u></td></lc<>	-58	<u></u>
N1.5 E11.5	<lc< td=""><td>9</td><td>43</td><td></td><td>482</td><td>481</td><td>4</td><td></td><td> </td><td><u> </u></td><td>4</td><td>70</td></lc<>	9	43		482	481	4		 	<u> </u>	4	70
N1.5 E12.5	<lc< td=""><td>-18</td><td>30</td><td></td><td>1017</td><td>1</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>- 4</td><td></td></lc<></td></lc<></td></lc<>	-18	30		1017	1	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>- 4</td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>- 4</td><td></td></lc<>	- 4	
N1.5 E13.5	<lc< td=""><td>0</td><td>40</td><td><lc< td=""><td>321</td><td>463</td><td></td><td></td><td></td><td>1 6</td><td>-17</td><td>7</td></lc<></td></lc<>	0	40	<lc< td=""><td>321</td><td>463</td><td></td><td></td><td></td><td>1 6</td><td>-17</td><td>7</td></lc<>	321	463				1 6	-17	7
N1.5 E14.5	-Lc	18	47		857		<lc< td=""><td>2</td><td></td><td><lc< td=""><td>-17 -29</td><td>7</td></lc<></td></lc<>	2		<lc< td=""><td>-17 -29</td><td>7</td></lc<>	-17 -29	7
N1.5 E15.5	<lc< td=""><td>-18</td><td></td><td></td><td>883</td><td>522</td><td><lc< td=""><td>-1</td><td><u> </u></td><td> <lc< td=""><td>-25</td><td></td></lc<></td></lc<></td></lc<>	-18			883	522	<lc< td=""><td>-1</td><td><u> </u></td><td> <lc< td=""><td>-25</td><td></td></lc<></td></lc<>	-1	<u> </u>	<lc< td=""><td>-25</td><td></td></lc<>	-25	
N1.5 E16.5		VA.	NA		NA	NA				ļ		
N1.5 E17.5	_11	VA.	NA		NA	NA				<u> </u>		
N1.5 E18.5	<lc< td=""><td>-18</td><td>30</td><td></td><td>696</td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td><td></td></lc<>	-18	30		696					<u> </u>		
N1.5 E19.5	<lc< td=""><td>0</td><td></td><td></td><td>375</td><td>469</td><td></td><td></td><td></td><td><u> </u></td><td></td><td></td></lc<>	0			375	469				<u> </u>		
N1.5 E19.5	<lc< td=""><td>-18</td><td></td><td></td><td>375</td><td>469</td><td>9</td><td></td><td></td><td>1</td><td></td><td>7</td></lc<>	-18			375	469	9			1		7
	-Lc	0			1365	568	<lc< td=""><td></td><td>1 (</td><td>) <lc< td=""><td>29</td><td>· · · · · · ·</td></lc<></td></lc<>		1 () <lc< td=""><td>29</td><td>· · · · · · ·</td></lc<>	29	· · · · · · ·
N1.5 E20.5	<lc< td=""><td></td><td></td><td><lc< td=""><td>294</td><td>460</td><td></td><td></td><td></td><td>1</td><td></td><td> </td></lc<></td></lc<>			<lc< td=""><td>294</td><td>460</td><td></td><td></td><td></td><td>1</td><td></td><td> </td></lc<>	294	460				1		
N1.5 E21.5	<lc< td=""><td>9</td><td>1</td><td><lc< td=""><td>214</td><td>45</td><td>1</td><td></td><td></td><td>_</td><td></td><td>7</td></lc<></td></lc<>	9	1	<lc< td=""><td>214</td><td>45</td><td>1</td><td></td><td></td><td>_</td><td></td><td>7</td></lc<>	214	45	1			_		7
N1.5 E3.5	<lc< td=""><td>-18</td><td></td><td></td><td>830</td><td>51</td><td>7 <lc< td=""><td></td><td>1 (</td><td>) <lc< td=""><td>8</td><td>/</td></lc<></td></lc<></td></lc<>	-18			830	51	7 <lc< td=""><td></td><td>1 (</td><td>) <lc< td=""><td>8</td><td>/</td></lc<></td></lc<>		1 () <lc< td=""><td>8</td><td>/</td></lc<>	8	/
N1.5 E4.5	11-11	37			642	49	3					
N1.5 E5.5	- - - -	-18		-	910		5 <lc< td=""><td>-</td><td>1</td><td>) <lc< td=""><td>38</td><td>7</td></lc<></td></lc<>	-	1) <lc< td=""><td>38</td><td>7</td></lc<>	38	7
N1.5 E6.5	<lc< td=""><td>-10</td><td></td><td>/Lc</td><td>294</td><td>46</td><td>5</td><td></td><td></td><td></td><td><u>,</u></td><td></td></lc<>	-10		/Lc	294	46	5				<u>,</u>	
N1.5 E7.5			1		589		2					ļ
N1.5 E8.5	<lc< td=""><td>-9</td><td></td><td></td><td>45</td><td></td><td>8</td><td></td><td></td><td></td><td></td><td></td></lc<>	-9			45		8					
N1.5 E9.5	<lc< td=""><td></td><td></td><td>/ / / Lc</td><td>33</td><td></td><td>8</td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>			/ / / Lc	33		8					<u> </u>
N10.0 E-1.0	<lc< td=""><td>20</td><td></td><td>2 <lc< td=""><td>25</td><td></td><td>0</td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	20		2 <lc< td=""><td>25</td><td></td><td>0</td><td></td><td></td><td></td><td></td><td></td></lc<>	25		0					
N10.0 E-2.0			NA S	11-0	NA	NA						
N10.0 E1.0		NA 10		, 	104		1 <lc< td=""><td></td><td></td><td>0 <lc< td=""><td>-4</td><td>1</td></lc<></td></lc<>			0 <lc< td=""><td>-4</td><td>1</td></lc<>	-4	1
N10.0 E10.0	<lc< td=""><td>19</td><td></td><td></td><td>91</td><td></td><td>9 <lc< td=""><td></td><td>1</td><td>0 <lc< td=""><td>(</td><td></td></lc<></td></lc<></td></lc<>	19			91		9 <lc< td=""><td></td><td>1</td><td>0 <lc< td=""><td>(</td><td></td></lc<></td></lc<>		1	0 <lc< td=""><td>(</td><td></td></lc<>	(
N10.0 E11.0	<lc< td=""><td>10</td><td></td><td></td><td>52</td><td><u> </u></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	10			52	<u> </u>						
N10.0 E12.0	<lc< td=""><td>-19</td><td></td><td></td><td>73</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-19			73							
N10.0 E13.0	<lc< td=""><td>-4</td><td></td><td></td><td>70</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-4			70							
N10.0 E14.0	<lc< td=""><td>-4</td><td></td><td>4 < Lc</td><td>18</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-4		4 < Lc	18							
N10.0 E15.0	<lc< td=""><td>-3</td><td></td><td>0</td><td>45</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-3		0	45							
N10.0 E16.0	- C	2			NA 43	NA NA	1					
N10.0 E17.0	_#	NA	NA NA		NA NA	NA NA						
N10.0 E18.0		NA_	NA		NA NA	NA NA						
N10.0 E19.0		NA	NA			NA NA	-					<u> </u>
N10.0 E2.0		NA	NA		NA NA	NA NA						
N10.0 E20.0		NA	NA		NA NA	NA NA	-					
N10.0 E21.0		NA	NA	_#-	NA 21		26					
N10.0 E22.0	<lc< td=""><td>-1</td><td></td><td>7 <lc< td=""><td></td><td></td><td>26</td><td></td><td>_</td><td></td><td></td><td></td></lc<></td></lc<>	-1		7 <lc< td=""><td></td><td></td><td>26</td><td></td><td>_</td><td></td><td></td><td></td></lc<>			26		_			
N10.0 E3.0	<lc< td=""><td></td><td></td><td>1 <lc< td=""><td></td><td></td><td>78</td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>			1 <lc< td=""><td></td><td></td><td>78</td><td></td><td></td><td></td><td></td><td></td></lc<>			78					
N10.0 E4.0	<lc< td=""><td></td><td></td><td>9</td><td>70</td><td></td><td></td><td></td><td></td><td>1</td><td></td><td></td></lc<>			9	70					1		
N10.0 E5.0	<lc< td=""><td>- 2</td><td>29 3</td><td>9</td><td>42</td><td>28 5</td><td>49</td><td></td><td></td><td></td><td></td><td></td></lc<>	- 2	29 3	9	42	28 5	49					

Lc indicates less than the critical level of activity which can be said to be above background.
A negative value is the calculated result of a reading which is below the instrument-specific background.

	•										4.51				
ſ		Γ	DIRECT				\Box			ANSFER	ARL	E TA-GAM	NA A /1 (00.50	CM
	ALPHA/1			3ETA	-GAMMA/10	0 SQ	CM	ALPH/			RE			STD	
LOCATIONITEM	SMPL		STD		SMPL	STD	ı	SMF		STD		SMPL DPM	i i	DEV	İ
LOCATION/ITEM COORDINATES	DPM		DEV		DPM	DEV		DP	М	DEV	╂	DPM		ULV	
N10.0 E6.0	<lc< td=""><td>ol</td><td>51</td><td><lc< td=""><td>-122</td><td></td><td>487</td><td></td><td></td><td></td><td>╂</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	ol	51	<lc< td=""><td>-122</td><td></td><td>487</td><td></td><td></td><td></td><td>╂</td><td></td><td></td><td></td><td></td></lc<>	-122		487				╂				
N10.0 E0.0 N10.0 E7.0		-39	34	<lc< td=""><td>397</td><td></td><td>546</td><td></td><td></td><td></td><td>╂</td><td></td><td></td><td></td><td></td></lc<>	397		546				╂				
	<lc< td=""><td>10</td><td>54</td><td><lc< td=""><td>61</td><td></td><td>509</td><td></td><td></td><td></td><td>1-</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	10	54	<lc< td=""><td>61</td><td></td><td>509</td><td></td><td></td><td></td><td>1-</td><td></td><td></td><td></td><td></td></lc<>	61		509				1-				
N10.0 E8.0		-48		<lc< td=""><td>306</td><td></td><td>536</td><td></td><td></td><td></td><td>1</td><td></td><td>-67</td><td></td><td>71</td></lc<>	306		536				1		-67		71
N10.0 E9.0	<lc< td=""><td>11</td><td>27</td><td></td><td>751</td><td></td><td>510</td><td><lc_< td=""><td>2</td><td></td><td><<u>L</u>0</td><td>·</td><td>0/</td><td></td><td></td></lc_<></td></lc<>	11	27		751		510	<lc_< td=""><td>2</td><td></td><td><<u>L</u>0</td><td>·</td><td>0/</td><td></td><td></td></lc_<>	2		< <u>L</u> 0	·	0/		
N10.5 E-0.5	<lc< td=""><td>11</td><td></td><td><lc< td=""><td>259</td><td>Ī</td><td>460</td><td></td><td></td><td></td><td>╂-</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	11		<lc< td=""><td>259</td><td>Ī</td><td>460</td><td></td><td></td><td></td><td>╂-</td><td></td><td></td><td></td><td></td></lc<>	259	Ī	460				╂-				
N10.5 E-1.5	<lc< td=""><td>-9</td><td></td><td><lc< td=""><td>294</td><td></td><td>460</td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-9		<lc< td=""><td>294</td><td></td><td>460</td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td></lc<>	294		460				-				
N10.5 E0.5	NA		NA		NA	NA				ļ	1.		25		78
N10.5 E1.5	<lc< td=""><td>18</td><td>47</td><td></td><td>776</td><td></td><td>511</td><td><lc< td=""><td><u>-1</u></td><td></td><td>) <l< td=""><td><u>C</u></td><td></td><td></td><td></td></l<></td></lc<></td></lc<>	18	47		776		511	<lc< td=""><td><u>-1</u></td><td></td><td>) <l< td=""><td><u>C</u></td><td></td><td></td><td></td></l<></td></lc<>	<u>-1</u>) <l< td=""><td><u>C</u></td><td></td><td></td><td></td></l<>	<u>C</u>			
N10.5 E10.5	1	46	57		723		506			ļ					
N10.5 E11.5	<lc< td=""><td>-0</td><td>40</td><td></td><td>482</td><td></td><td>481</td><td></td><td></td><td>ļ</td><td>1-</td><td></td><td></td><td></td><td></td></lc<>	-0	40		482		481			ļ	1-				
N10.5 E12.5	<lc< td=""><td>9</td><td></td><td><lc< td=""><td>321</td><td></td><td>463</td><td></td><td></td><td></td><td></td><td></td><td></td><td> </td><td></td></lc<></td></lc<>	9		<lc< td=""><td>321</td><td></td><td>463</td><td></td><td></td><td></td><td></td><td></td><td></td><td> </td><td></td></lc<>	321		463							 	
N10.5 E13.5	<lc< td=""><td>-28</td><td></td><td><lc< td=""><td>161</td><td></td><td>445</td><td></td><td></td><td><u> </u></td><td></td><td></td><td></td><td> </td><td></td></lc<></td></lc<>	-28		<lc< td=""><td>161</td><td></td><td>445</td><td></td><td></td><td><u> </u></td><td></td><td></td><td></td><td> </td><td></td></lc<>	161		445			<u> </u>				 	
N10.5 E14.5	<lc< td=""><td>28</td><td>50</td><td></td><td>375</td><td>5</td><td>469</td><td></td><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td></lc<>	28	50		375	5	469							-	
N10.5 E15.5	<lc< td=""><td>28</td><td>50</td><td></td><td>803</td><td>3</td><td>514</td><td></td><td></td><td></td><td>-</td><td></td><td>-13</td><td> </td><td>74</td></lc<>	28	50		803	3	514				-		-13	 	74
N10.5 E16.5	<lc< td=""><td>0</td><td></td><td><lc< td=""><td>-80</td><td></td><td></td><td><lc_< td=""><td>-1</td><td></td><td></td><td></td><td>-13 8</td><td></td><td>76</td></lc_<></td></lc<></td></lc<>	0		<lc< td=""><td>-80</td><td></td><td></td><td><lc_< td=""><td>-1</td><td></td><td></td><td></td><td>-13 8</td><td></td><td>76</td></lc_<></td></lc<>	-80			<lc_< td=""><td>-1</td><td></td><td></td><td></td><td>-13 8</td><td></td><td>76</td></lc_<>	-1				-13 8		76
N10.5 E17.5	11-20	37	54		616	3	495	<lc< td=""><td><u>-1</u></td><td></td><td>0 <l< td=""><td>.U</td><td></td><td> </td><td></td></l<></td></lc<>	<u>-1</u>		0 <l< td=""><td>.U</td><td></td><td> </td><td></td></l<>	.U		 	
N10.5 E18.5	NA NA	<u> </u>	NA		NA	NA					#-			 	
N10.5 E19.5	NA NA		NA		NA	NA								 	
N10.5 E2.5	NA NA		NA		NA	NA								┼	
N10.5 E20.5	NA NA		NA	1	NA	NA				<u> </u>				┼──	
N10.5 E21.5	NA NA		NA	1	NA	NA								-	
N10.5 E3.5	NA NA		NA	1	NA	NA		ł			_#_			╂	
N10.5 E4.5	<lc< td=""><td>9</td><td></td><td>#</td><td>53</td><td>5</td><td>487</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	9		#	53	5	487								
N10.5 E5.5		28		<lc< td=""><td>16</td><td>1</td><td>445</td><td></td><td></td><td></td><td>_</td><td></td><td></td><td></td><td></td></lc<>	16	1	445				_				
N10.5 E6.5	<lc <lc< td=""><td>C</td><td></td><td><lc< td=""><td></td><td>8</td><td>382</td><td>2</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<></lc 	C		<lc< td=""><td></td><td>8</td><td>382</td><td>2</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		8	382	2							
N10.5 E7.5	/ <lc< td=""><td></td><td></td><td><l0< td=""><td></td><td>0</td><td>436</td><td>6</td><td></td><td></td><td>_ _</td><td></td><td></td><td>-</td><td></td></l0<></td></lc<>			<l0< td=""><td></td><td>0</td><td>436</td><td>6</td><td></td><td></td><td>_ _</td><td></td><td></td><td>-</td><td></td></l0<>		0	436	6			_ _			-	
N10.5 E8.5	<lc< td=""><td></td><td></td><td> <lc< td=""><td></td><td>4</td><td>433</td><td>3</td><td></td><td></td><td></td><td></td><td></td><td> </td><td></td></lc<></td></lc<>			<lc< td=""><td></td><td>4</td><td>433</td><td>3</td><td></td><td></td><td></td><td></td><td></td><td> </td><td></td></lc<>		4	433	3						 	
N10.5 E9.5	<lc< td=""><td>-7</td><td></td><td></td><td>41</td><td>5</td><td>476</td><td>3</td><td></td><td></td><td>_ -</td><td></td><td></td><td></td><td></td></lc<>	-7			41	5	476	3			_ -				
N11.0 E-1.0	1/20	20		2 < L	-10	14	419)						+	
N11.0 E-2.0	<lc< td=""><td></td><td>27</td><td></td><td>41</td><td>5</td><td>440</td><td>3</td><td></td><td></td><td>- -</td><td></td><td></td><td>-</td><td></td></lc<>		27		41	5	440	3			- -			-	
N11.0 E0.0	- II-LC	24			5	2	400				_				
N11.0 E1.0	<lc< td=""><td>-13</td><td></td><td></td><td></td><td>31</td><td>416</td><td>3</td><td></td><td></td><td></td><td></td><td>3</td><td></td><td>8:</td></lc<>	-13				31	416	3					3		8:
N11.0 E10.0	<lc< td=""><td>1:</td><td></td><td></td><td>82</td><td>29</td><td>48</td><td>7</td><td></td><td>5</td><td>8 <</td><td>LC</td><td></td><td>^</td><td><u> </u></td></lc<>	1:			82	29	48	7		5	8 <	LC		^	<u> </u>
N11.0 E11.0	1120	2		7	72	25	47				_				
N11.0 E12.0	_	2		7 <l< td=""><td>c 28</td><td>35</td><td>42</td><td>8</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<>	c 28	35	42	8							
N11.0 E13.0		2		7 <l< td=""><td></td><td>11</td><td>43</td><td>1</td><td></td><td></td><td>_#-</td><td></td><td></td><td></td><td></td></l<>		11	43	1			_#-				
N11.0 E14.0		2		711	5!	96	46	3							
N11.0 E15.0		3		1	4	15	44	3							
N11.0 E16.0		4		5		51	47	9							
N11.0 E17.0				9		25	47	6						-	7
N11.0 E18.0	- - - 			öl	10		51	0 <lc< td=""><td></td><td>-1</td><td>0 <</td><td><lc< td=""><td>2</td><td>25</td><td></td></lc<></td></lc<>		-1	0 <	<lc< td=""><td>2</td><td>25</td><td></td></lc<>	2	25	
N11.0 E19.0	<lc< td=""><td></td><td></td><td>0 < L</td><td></td><td>52</td><td>38</td><td>7</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			0 < L		52	38	7							
N11.0 E2.0	<lc< td=""><td></td><td></td><td>0 <l< td=""><td></td><td>30</td><td>40</td><td>9</td><td></td><td></td><td>$- \downarrow$</td><td></td><td></td><td></td><td></td></l<></td></lc<>			0 <l< td=""><td></td><td>30</td><td>40</td><td>9</td><td></td><td></td><td>$- \downarrow$</td><td></td><td></td><td></td><td></td></l<>		30	40	9			$- \downarrow$				
N11.0 E20.0	<lc< td=""><td></td><td></td><td>7 <l< td=""><td></td><td>04</td><td>40</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<></td></lc<>			7 <l< td=""><td></td><td>04</td><td>40</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<>		04	40								
N11.0 E21.0	<lc< td=""><td>_</td><td></td><td>0 <l< td=""><td></td><td>78</td><td>40</td><td>3</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<></td></lc<>	_		0 <l< td=""><td></td><td>78</td><td>40</td><td>3</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<>		78	40	3							
N11.0 E22.0	<lc< td=""><td></td><td></td><td>7 <l< td=""><td></td><td>04</td><td>40</td><td>6</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<></td></lc<>			7 <l< td=""><td></td><td>04</td><td>40</td><td>6</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<>		04	40	6							
N11.0 E3.0	<lc< td=""><td></td><td></td><td>0 <l< td=""><td></td><td>04</td><td>40</td><td>06</td><td></td><td><u> </u></td><td>#</td><td></td><td></td><td></td><td></td></l<></td></lc<>			0 <l< td=""><td></td><td>04</td><td>40</td><td>06</td><td></td><td><u> </u></td><td>#</td><td></td><td></td><td></td><td></td></l<>		04	40	06		<u> </u>	#				
N11.0 E4.0	<lc< td=""><td></td><td></td><td>20 < L</td><td></td><td>26</td><td></td><td>7</td><td></td><td></td><td></td><td></td><td></td><td></td><td><u></u></td></lc<>			20 < L		26		7							<u></u>
N11.0 E5.0	<lc< td=""><td></td><td></td><td>2011</td><td>7</td><td>25</td><td></td><td>76</td><td></td><td></td><td></td><td></td><td></td><td>-+-</td><td></td></lc<>			2011	7	25		76						-+-	
N11.0 E6.0	<lc< td=""><td></td><td></td><td>10</td><td></td><td>18</td><td></td><td>54</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			10		18		54							
N11.0 E7.0	<lc< td=""><td></td><td></td><td>27</td><td></td><td>192</td><td></td><td>51</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			27		192		51							
N11.0 E8.0	<lc< td=""><td></td><td></td><td>27</td><td></td><td>192</td><td></td><td>51</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			27		192		51							
N11.0 E9.0	<lc< td=""><td></td><td></td><td></td><td></td><td>337</td><td></td><td>38</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>					337		38							
N11.5 E-0.5	<lc< td=""><td></td><td>2</td><td>19 <</td><td>ty which can</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		2	19 <	ty which can										

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

									TD	ANSFER	AB	ī F			
ſ			DIRECT					ALPHA/			R	ETA-GAN	IMA/1	00 SQ	СМ
	ALPH/				-GAMMA/10		M	SMPL		STD	-	SMPL	.,,,,	STD	
LOCATION/ITEM	SMF	PL :	STD		···· -	STD				DEV		DPM		DEV	
COORDINATES	DPI	м !!	DEV			DEV		DPM		DEV	1-				
N11.5 E-1.5		20		<lc< td=""><td>-52</td><td></td><td>25</td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td></lc<>	-52		25				-				
N11.5 E0.5	<lc< td=""><td>28</td><td>50</td><td><lc< td=""><td>348</td><td></td><td>66</td><td></td><td></td><td></td><td><</td><td></td><td>-38</td><td> </td><td>71</td></lc<></td></lc<>	28	50	<lc< td=""><td>348</td><td></td><td>66</td><td></td><td></td><td></td><td><</td><td></td><td>-38</td><td> </td><td>71</td></lc<>	348		66				<		-38	 	71
N11.5 E1.5	<lc< td=""><td>-28</td><td>24</td><td></td><td>883</td><td></td><td>22 <</td><td>LC</td><td>1</td><td></td><td>1</td><td></td><td>-50</td><td></td><td></td></lc<>	-28	24		883		22 <	LC	1		1		-50		
	<lc< td=""><td>-28</td><td>24</td><td><lc< td=""><td>54</td><td></td><td>33</td><td></td><td></td><td></td><td>١.,</td><td></td><td>24</td><td> </td><td>77</td></lc<></td></lc<>	-28	24	<lc< td=""><td>54</td><td></td><td>33</td><td></td><td></td><td></td><td>١.,</td><td></td><td>24</td><td> </td><td>77</td></lc<>	54		33				١.,		24	 	77
N11.5 E10.5	<lc< td=""><td>18</td><td>47</td><td></td><td>964</td><td>5</td><td>30 <</td><td>Lc</td><td>-1</td><td></td><td> < </td><td>_C</td><td>21</td><td> </td><td></td></lc<>	18	47		964	5	30 <	Lc	-1		<	_C	21	 	
N11.5 E11.5		9	43		509	4	84				┺				
N11.5 E12.5	<lc< td=""><td>-9</td><td></td><td><lc< td=""><td>27</td><td>4</td><td>29</td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<></td></lc<>	-9		<lc< td=""><td>27</td><td>4</td><td>29</td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<>	27	4	29							<u> </u>	
N11.5 E13.5	<lc< td=""><td></td><td>35</td><td>120</td><td>509</td><td></td><td>84</td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<>		35	120	509		84							<u> </u>	
N11.5 E14.5	<lc< td=""><td>-9</td><td></td><td><lc< td=""><td>321</td><td></td><td>63</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-9		<lc< td=""><td>321</td><td></td><td>63</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	321		63								
N11.5 E15.5	<lc< td=""><td>0</td><td></td><td></td><td>294</td><td></td><td>60</td><td></td><td></td><td></td><td>T</td><td></td><td></td><td></td><td></td></lc<>	0			294		60				T				
N11.5 E16.5	<lc< td=""><td>-9</td><td></td><td><lc< td=""><td>910</td><td></td><td>25</td><td><l c<="" td=""><td>-1</td><td>(</td><td>) <</td><td>Lc</td><td>-29</td><td></td><td>72</td></l></td></lc<></td></lc<>	-9		<lc< td=""><td>910</td><td></td><td>25</td><td><l c<="" td=""><td>-1</td><td>(</td><td>) <</td><td>Lc</td><td>-29</td><td></td><td>72</td></l></td></lc<>	910		25	<l c<="" td=""><td>-1</td><td>(</td><td>) <</td><td>Lc</td><td>-29</td><td></td><td>72</td></l>	-1	() <	Lc	-29		72
N11.5 E17.5	<lc_< td=""><td>0</td><td>40</td><td></td><td>509</td><td></td><td>184</td><td></td><td><u>`</u></td><td></td><td>1</td><td></td><td></td><td>I</td><td></td></lc_<>	0	40		509		184		<u>`</u>		1			I	
N11.5 E18.5	<lc< td=""><td>-18</td><td>30</td><td>ļ</td><td></td><td>NA</td><td>-0-7</td><td></td><td></td><td> </td><td>1</td><td></td><td></td><td></td><td></td></lc<>	-18	30	ļ		NA	-0-7			 	1				
N11.5 E19.5	N	Α	NA	I	NA C11		154				+				
N11.5 E2.5	<lc< td=""><td>9</td><td></td><td><lc< td=""><td>241</td><td></td><td>+54 </td><td></td><td></td><td> </td><td>+</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	9		<lc< td=""><td>241</td><td></td><td>+54 </td><td></td><td></td><td> </td><td>+</td><td></td><td></td><td></td><td></td></lc<>	241		+54			 	+				
N11.5 E20.5	l N	IA	NA	 	NA NA	NA_	∦			 	#			T	
N11.5 E21.5	l N	IA	NA	I	NA	NA_	400			 	+			1	
N11.5 E3.5	<lc< td=""><td>0</td><td></td><td></td><td>294</td><td></td><td>460</td><td></td><td></td><td> </td><td>╫</td><td></td><td></td><td>†</td><td></td></lc<>	0			294		460			 	╫			†	
N11.5 E4.5	<lc< td=""><td>-18</td><td>30</td><td></td><td>375</td><td></td><td>469</td><td></td><td></td><td> </td><td>╫</td><td></td><td></td><td>1</td><td></td></lc<>	-18	30		375		469			 	╫			1	
N11.5 E5.5	<lc< td=""><td>18</td><td></td><td></td><td>428</td><td></td><td>475</td><td></td><td></td><td><u> </u></td><td></td><td></td><td></td><td>-</td><td></td></lc<>	18			428		475			<u> </u>				-	
N11.5 E5.5	<lc< td=""><td>0</td><td>·</td><td></td><td>402</td><td>2</td><td>472</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	0	·		402	2	472								
N11.5 E6.5	<lc< td=""><td>9</td><td></td><td><lc< td=""><td>80</td><td>)</td><td>436</td><td></td><td></td><td></td><td>╬</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	9		<lc< td=""><td>80</td><td>)</td><td>436</td><td></td><td></td><td></td><td>╬</td><td></td><td></td><td></td><td></td></lc<>	80)	436				╬				
N11.5 E7.5	_	0		<lc< td=""><td>321</td><td></td><td>463</td><td></td><td></td><td></td><td>4</td><td></td><td></td><td></td><td></td></lc<>	321		463				4				
N11.5 E9.5	<lc< td=""><td>29</td><td></td><td><lc< td=""><td></td><td>5</td><td>463</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	29		<lc< td=""><td></td><td>5</td><td>463</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		5	463								
N12.0 E-1.0				≺Lc			460			T					
N12.0 E-2.0	4	39			3639		824	<lc< td=""><td></td><td>2</td><td>6</td><td><lc< td=""><td>-3</td><td>3</td><td>7</td></lc<></td></lc<>		2	6	<lc< td=""><td>-3</td><td>3</td><td>7</td></lc<>	-3	3	7
N12.0 E1.0	<lc< td=""><td>-10</td><td></td><td></td><td></td><td></td><td>546</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-10					546								
N12.0 E10.0	<lc< td=""><td><u> </u></td><td></td><td></td><td>1254</td><td></td><td>631</td><td><1 c</td><td>-</td><td>1</td><td>0</td><td><lc< td=""><td>-3</td><td>8</td><td>7</td></lc<></td></lc<>	<u> </u>			1254		631	<1 c	-	1	0	<lc< td=""><td>-3</td><td>8</td><td>7</td></lc<>	-3	8	7
N12.0 E11.0	<lc< td=""><td>-10</td><td></td><td></td><td>58</td><td></td><td>565</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-10			58		565								
N12.0 E12.0	<lc< td=""><td>-10</td><td></td><td></td><td></td><td></td><td>599</td><td>610</td><td></td><td>1</td><td>0</td><td><lc< td=""><td>-3</td><td>8</td><td>7</td></lc<></td></lc<>	-10					599	610		1	0	<lc< td=""><td>-3</td><td>8</td><td>7</td></lc<>	-3	8	7
N12.0 E13.0	<lc< td=""><td>-19</td><td></td><td></td><td>91</td><td></td><td>553</td><td>_LC</td><td></td><td>+</td><td></td><td></td><td></td><td></td><td></td></lc<>	-19			91		553	_LC		+					
N12.0 E14.0	<lc< td=""><td>-39</td><td></td><td></td><td>45</td><td></td><td></td><td>-10</td><td></td><td>1</td><td>0</td><td><lc< td=""><td>-2</td><td>5</td><td>7</td></lc<></td></lc<>	-39			45			-10		1	0	<lc< td=""><td>-2</td><td>5</td><td>7</td></lc<>	-2	5	7
N12.0 E15.0	<lc< td=""><td>-29</td><td></td><td></td><td>82</td><td></td><td>590</td><td>\<u>L</u>U</td><td></td><td>' </td><td>-</td><td></td><td></td><td></td><td></td></lc<>	-29			82		590	\ <u>L</u> U		' 	-				
N12.0 E16.0	<lc< td=""><td>-1(</td><td>) 4</td><td>7 </td><td>58</td><td></td><td>565</td><td></td><td></td><td></td><td></td><td><lc< td=""><td>-5</td><td>0</td><td>7</td></lc<></td></lc<>	-1() 4	7	58		565					<lc< td=""><td>-5</td><td>0</td><td>7</td></lc<>	-5	0	7
N12.0 E17.0	<lc< td=""><td>-10</td><td>) 4</td><td>7</td><td>128</td><td>4</td><td></td><td><lc< td=""><td></td><td>1</td><td>ᅫ</td><td><u> </u></td><td></td><td>`</td><td></td></lc<></td></lc<>	-10) 4	7	128	4		<lc< td=""><td></td><td>1</td><td>ᅫ</td><td><u> </u></td><td></td><td>`</td><td></td></lc<>		1	ᅫ	<u> </u>		`	
N12.0 E18.0	<lc< td=""><td>-39</td><td>9 3</td><td>4</td><td>67</td><td>3</td><td>575</td><td></td><td></td><td></td><td>-#</td><td></td><td></td><td>_</td><td></td></lc<>	-39	9 3	4	67	3	575				-#			_	
		NA	NA	7	NA	NA					_			34	8
N12.0 E19.0	<lc< td=""><td>-10</td><td></td><td>7</td><td>171</td><td>2</td><td>673</td><td><lc< td=""><td>-</td><td>1</td><td>0</td><td></td><td></td><td>*</td><td></td></lc<></td></lc<>	-10		7	171	2	673	<lc< td=""><td>-</td><td>1</td><td>0</td><td></td><td></td><td>*</td><td></td></lc<>	-	1	0			*	
N12.0 E2.0		NA - I	NA	+	NA	NA					_				
N12.0 E20.0			NA NA	-	NA	NA					_				
N12.0 E21.0		NA _		1	45	9	553								
N12.0 E22.0	<lc< td=""><td>-5</td><td></td><td>3</td><td>104</td><td></td><td>611</td><td></td><td></td><td>5</td><td>8</td><td><lc< td=""><td></td><td>21</td><td>7</td></lc<></td></lc<>	-5		3	104		611			5	8	<lc< td=""><td></td><td>21</td><td>7</td></lc<>		21	7
N12.0 E3.0	<lc< td=""><td>-1</td><td></td><td></td><td>70</td><td></td><td></td><td><lc< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td></td><td>13</td><td></td></lc<></td></lc<></td></lc<>	-1			70			<lc< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td></td><td>13</td><td></td></lc<></td></lc<>		-1	0	<lc< td=""><td></td><td>13</td><td></td></lc<>		13	
N12.0 E4.0	<lc< td=""><td>-1</td><td></td><td>3 </td><td>91</td><td></td><td>599</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-1		3	91		599								
N12.0 E5.0	<lc< td=""><td>-2</td><td></td><td>9</td><td>119</td><td></td><td></td><td><lc< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td></td><td>33</td><td></td></lc<></td></lc<></td></lc<>	-2		9	119			<lc< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td></td><td>33</td><td></td></lc<></td></lc<>		-1	0	<lc< td=""><td></td><td>33</td><td></td></lc<>		33	
N12.0 E6.0	<lc< td=""><td>-2</td><td></td><td>9</td><td>6</td><td></td><td>569</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>· · · · · · · · · · · · · · · · · · ·</td></lc<>	-2		9	6		569								· · · · · · · · · · · · · · · · · · ·
N12.0 E7.0	<lc< td=""><td>-1</td><td></td><td>3</td><td></td><td></td><td>543</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-1		3			543								
N12.0 E8.0	<lc< td=""><td></td><td></td><td>7 <l< td=""><td></td><td></td><td>581</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<></td></lc<>			7 <l< td=""><td></td><td></td><td>581</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<>			581								
N12.0 E9.0	<lc< td=""><td>1</td><td></td><td>4</td><td></td><td>34</td><td></td><td>_</td><td></td><td>_</td><td>\dashv</td><td></td><td></td><td></td><td></td></lc<>	1		4		34		_		_	\dashv				
N12.5 E0.5		6		2		35	487			-1 -		<lc< td=""><td></td><td>50</td><td></td></lc<>		50	
N12.5 E1.5	<lc< td=""><td></td><td></td><td>35</td><td></td><td>76</td><td></td><td><lc< td=""><td></td><td>-' </td><td><u> </u></td><td></td><td></td><td>1</td><td></td></lc<></td></lc<>			35		76		<lc< td=""><td></td><td>-' </td><td><u> </u></td><td></td><td></td><td>1</td><td></td></lc<>		-' 	<u> </u>			1	
N12.5 E1.5	-11			11 <l< td=""><td></td><td>78</td><td>440</td><td></td><td></td><td></td><td></td><td></td><td></td><td>_</td><td></td></l<>		78	440							_	
N12.5 E 10.5				15	5	96	495								
N12.5 E11.5	$-\parallel$			55 <l< td=""><td>С</td><td>52</td><td>437</td><td>_</td><td></td><td></td><td></td><td> </td><td></td><td></td><td></td></l<>	С	52	437	_				 			
N12.5 E12.5				37 <l< td=""><td></td><td>81</td><td>451</td><td>1</td><td><u></u></td><td> </td><td></td><td> </td><td></td><td></td><td></td></l<>		81	451	1	<u></u>			 			
N12.5 E13.5 N12.5 E14.5				45 <l< td=""><td></td><td>0</td><td>431</td><td>1</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<>		0	431	1							
	i i	- 4		32 <		11	465	_ II				11		- 1	

Lc indicates less than the critical level of activity which can be said to be above background.
A negative value is the calculated result of a reading which is below the instrument-specific background.

									70	ANSFER	ΔR	F			
			DIRECT				١.	ALPHA/			TR	ETA-GAN	MA/1	00 SQ	CM
	ALPHA/	100	SQ CM	BETA	-GAMMA/10		\ /			STD	+=	SMPL		STD	\neg
LOCATION/ITEM	SMPL		STD		SMPL	STD	ı	SMPL		DEV	1	DPM		DEV	ļ
COORDINATES	DPM	ļ	DEV		DPM	DEV	+	DPM		DEV	1				
N12.5 E16.5		29	37		570	492					1	^	-17		76
N12.5 E17.5	<lc< td=""><td>2</td><td>19</td><td></td><td>725</td><td>508</td><td>_</td><td>LC</td><td>_2</td><td></td><td>1</td><td></td><td></td><td></td><td></td></lc<>	2	19		725	508	_	LC	_2		1				
N12.5 E17.5	<lc< td=""><td>2</td><td>19</td><td><lc< td=""><td>-26</td><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	2	19	<lc< td=""><td>-26</td><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td></lc<>	-26						-				
N12.5 E 10.5	<lc< td=""><td>-7</td><td>7</td><td></td><td>52</td><td>437</td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td></lc<>	-7	7		52	437					-				
N12.5 E19.5	<lc< td=""><td>-7</td><td>7</td><td><lc< td=""><td>363</td><td>47</td><td>1</td><td></td><td></td><td></td><td></td><td></td><td></td><td> </td><td></td></lc<></td></lc<>	-7	7	<lc< td=""><td>363</td><td>47</td><td>1</td><td></td><td></td><td></td><td></td><td></td><td></td><td> </td><td></td></lc<>	363	47	1							 	
N12.5 E2.5	1	20	32	<lc< td=""><td>285</td><td>463</td><td>3</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	285	463	3								
N12.5 E20.5	10	2		<lc< td=""><td>207</td><td></td><td>4]</td><td></td><td></td><td></td><td>—</td><td></td><td></td><td></td><td></td></lc<>	207		4]				—				
N12.5 E21.5	<lc< td=""><td>29</td><td></td><td><u> </u></td><td>389</td><td>47.</td><td>4</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td><td></td></lc<>	29		<u> </u>	389	47.	4				1				
N12.5 E3.5	1	2		<lc< td=""><td>285</td><td></td><td>3</td><td></td><td></td><td><u> </u></td><td>1</td><td></td><td></td><td> </td><td></td></lc<>	285		3			<u> </u>	1			 	
N12.5 E4.5	<lc_< td=""><td>39</td><td></td><td></td><td>570</td><td></td><td>2</td><td></td><td></td><td></td><td></td><td></td><td></td><td> </td><td></td></lc_<>	39			570		2							 	
N12.5 E5.5				<lc< td=""><td>26</td><td></td><td>4</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td><td></td></lc<>	26		4				1				
N12.5 E6.5		29		<lc< td=""><td>104</td><td></td><td>3</td><td></td><td></td><td></td><td>1_</td><td></td><td></td><td></td><td></td></lc<>	104		3				1_				
N12.5 E7.5	<lc< td=""><td>11</td><td></td><td><lc< td=""><td>-52</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td> </td><td></td></lc<></td></lc<>	11		<lc< td=""><td>-52</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td> </td><td></td></lc<>	-52									 	
N12.5 E8.5	↓	20			155									 	
N12.5 E9.5	4	20		_	39										
N13.0 E1.0	<lc< td=""><td>-39</td><td></td><td>+</td><td>1559</td><td></td><td></td><td><lc< td=""><td>- 2</td><td></td><td>6 <</td><td>Lc ·</td><td>-33</td><td></td><td>71</td></lc<></td></lc<>	-39		+	1559			<lc< td=""><td>- 2</td><td></td><td>6 <</td><td>Lc ·</td><td>-33</td><td></td><td>71</td></lc<>	- 2		6 <	Lc ·	-33		71
N13.0 E10.0	<lc< td=""><td>-19</td><td></td><td></td><td>122</td><td></td><td></td><td><lc< td=""><td>-1</td><td></td><td>0 <</td><td>Lc</td><td></td><td>1</td><td>76</td></lc<></td></lc<>	-19			122			<lc< td=""><td>-1</td><td></td><td>0 <</td><td>Lc</td><td></td><td>1</td><td>76</td></lc<>	-1		0 <	Lc		1	76
N13.0 E11.0	<lc< td=""><td>0</td><td></td><td></td><td>45</td><td></td><td></td><td></td><td></td><td>1</td><td>\top</td><td></td><td></td><td></td><td></td></lc<>	0			45					1	\top				
N13.0 E12.0	<lc< td=""><td>-39</td><td></td><td></td><td></td><td></td><td>_</td><td><lc< td=""><td>_1</td><td></td><td>0 <</td><td>Lc</td><td>-42</td><td>2</td><td>71</td></lc<></td></lc<>	-39					_	<lc< td=""><td>_1</td><td></td><td>0 <</td><td>Lc</td><td>-42</td><td>2</td><td>71</td></lc<>	_1		0 <	Lc	-42	2	71
N13.0 E13.0	<lc< td=""><td>29</td><td></td><td></td><td>100</td><td></td><td></td><td><lc< td=""><td></td><td></td><td>0 <</td><td></td><td></td><td>4</td><td>75</td></lc<></td></lc<>	29			100			<lc< td=""><td></td><td></td><td>0 <</td><td></td><td></td><td>4</td><td>75</td></lc<>			0 <			4	75
N13.0 E14.0	<lc< td=""><td>10</td><td></td><td></td><td>82</td><td></td><td></td><td></td><td></td><td>2</td><td>6</td><td></td><td>-59</td><td>9</td><td>69</td></lc<>	10			82					2	6		-59	9	69
N13.0 E15.0	<lc< td=""><td>-10</td><td></td><td></td><td>94</td><td></td><td></td><td><lc< td=""><td></td><td></td><td>Ť</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-10			94			<lc< td=""><td></td><td></td><td>Ť</td><td></td><td></td><td></td><td></td></lc<>			Ť				
N13.0 E16.0	<lc< td=""><td>(</td><td></td><td></td><td>58</td><td></td><td>35</td><td></td><td></td><td>+</td><td>-1</td><td></td><td></td><td></td><td></td></lc<>	(58		35			+	-1				
N13.0 E17.0	<lc< td=""><td>-19</td><td></td><td></td><td>58</td><td></td><td>35</td><td></td><td></td><td></td><td>$-\parallel$</td><td></td><td></td><td></td><td></td></lc<>	-19			58		35				$-\parallel$				
N13.0 E18.0	<lc< td=""><td>-29</td><td>9 39</td><td></td><td>67</td><td></td><td>75</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-29	9 39		67		75								
N13.0 E19.0	<lc< td=""><td>-48</td><td>8 2</td><td>3 <lc< td=""><td></td><td></td><td>19</td><td></td><td></td><td></td><td></td><td> </td><td></td><td></td><td></td></lc<></td></lc<>	-48	8 2	3 <lc< td=""><td></td><td></td><td>19</td><td></td><td></td><td></td><td></td><td> </td><td></td><td></td><td></td></lc<>			19					 			
N13.0 E2.0	<lc< td=""><td>-19</td><td></td><td>3</td><td>64</td><td></td><td>72</td><td></td><td></td><td></td><td></td><td></td><td></td><td>_</td><td></td></lc<>	-19		3	64		72							_	
N13.0 E20.0	<lc< td=""><td>-19</td><td></td><td>3</td><td>73</td><td></td><td>81</td><td></td><td></td><td>_</td><td></td><td></td><td></td><td>+</td><td></td></lc<>	-19		3	73		81			_				+	
N13.0 E20.0	- CLC	-1			55		62							+	
N13.0 E21.0	<lc< td=""><td>-1</td><td></td><td></td><td>73</td><td>4 5</td><td>81</td><td></td><td></td><td></td><td></td><td></td><td></td><td>_</td><td></td></lc<>	-1			73	4 5	81							_	
N13.0 E22.0	<lc< td=""><td>-3</td><td></td><td>4 < L</td><td>-42</td><td></td><td>48</td><td></td><td></td><td></td><td>-#</td><td></td><td></td><td></td><td></td></lc<>	-3		4 < L	-42		48				-#				
N13.0 E3.0	<lc< td=""><td>-3</td><td></td><td>4 <l< td=""><td></td><td>51 5</td><td>09</td><td></td><td></td><td></td><td>-#</td><td></td><td></td><td></td><td></td></l<></td></lc<>	-3		4 <l< td=""><td></td><td>51 5</td><td>09</td><td></td><td></td><td></td><td>-#</td><td></td><td></td><td></td><td></td></l<>		51 5	09				-#				
N13.0 E4.0				4 < L		6 5	39				_#				
N13.0 E5.0	<lc< td=""><td><u></u> -1</td><td></td><td>3 < L</td><td></td><td></td><td>39</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	<u></u> -1		3 < L			39								
N13.0 E6.0	<lc< td=""><td></td><td></td><td></td><td></td><td></td><td>46</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>						46								
N13.0 E7.0	<lc< td=""><td></td><td><u> </u></td><td>4</td><td></td><td></td><td>53</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		<u> </u>	4			53								
N13.0 E8.0	<lc< td=""><td></td><td></td><td></td><td></td><td></td><td>56</td><td></td><td></td><td></td><td></td><td></td><td></td><td>_</td><td></td></lc<>						56							_	
N13.0 E9.0	<lc< td=""><td></td><td></td><td>7</td><td></td><td></td><td>22</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			7			22								
N14.0 E0.0				7 <l< td=""><td></td><td></td><td>37</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<>			37								
N14.0 E1.0				5			74								
N14.0 E10.0		2		7			160								
N14.0 E11.0	<lc< td=""><td></td><td></td><td>7</td><td></td><td></td><td>149</td><td></td><td></td><td>_</td><td>\neg</td><td></td><td></td><td></td><td></td></lc<>			7			149			_	\neg				
N14.0 E12.0	<lc< td=""><td></td><td></td><td>13</td><td></td><td></td><td>434</td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td></lc<>			13			434			-					
N14.0 E13.0				37						5	8	<lc< td=""><td></td><td>13</td><td>7</td></lc<>		13	7
N14.0 E14.0	<lc< td=""><td>•</td><td></td><td>33</td><td></td><td></td><td>500</td><td></td><td></td><td>- Ĭ </td><td>-</td><td></td><td></td><td></td><td></td></lc<>	•		33			500			- Ĭ 	-				
N14.0 E15.0	<lc< td=""><td></td><td>15</td><td>33 <</td><td></td><td></td><td>425</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		15	33 <			425								
N14.0 E16.0	<lc< td=""><td></td><td>13</td><td>10</td><td></td><td></td><td>449</td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td></lc<>		13	10			449					-			
N14.0 E17.0	<lc< td=""><td></td><td>6</td><td>27 <</td><td></td><td></td><td>428</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		6	27 <			428								
N14.0 E17.0	- LC		6	27 <			419								
N14.0 E 10.0	<lc< td=""><td></td><td></td><td>33 <</td><td>_c</td><td></td><td>393</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			33 <	_c		393								
N14.0 E19.0	<lc< td=""><td></td><td></td><td>27</td><td>6</td><td></td><td>46</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			27	6		46								
N14.0 E2.0				27 <	Lc 2		42							_	
N14.0 E20.0	<lc< td=""><td></td><td></td><td>10 <</td><td></td><td></td><td>419</td><td>9</td><td></td><td></td><td></td><td><u> </u></td><td></td><td></td><td></td></lc<>			10 <			419	9				<u> </u>			
N14.0 E21.0	<lc< td=""><td></td><td></td><td>37 <</td><td></td><td></td><td>43</td><td>1</td><td></td><td></td><td></td><td> </td><td></td><td></td><td></td></lc<>			37 <			43	1				 			
N14.0 E22.0				33 <			42	5				ļ			
N14.0 E3.0	<lc< td=""><td></td><td></td><td></td><td></td><td>518</td><td>45</td><td></td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td></lc<>					518	45					1			
N1440 E40	<lc< td=""><td></td><td>-41</td><td>20</td><td>ity which car</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		-41	20	ity which car										

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

									TD	ANSFER	ARIE			 -1
[DIRECT					ALPHA			RET	A-GAMMA	/100 S	Q CM
	ALPH.	A/100 S	SQ CM		GAMMA/10		CM			STD	اسال	SMPL	ISTE	
OCATION/ITEM	SM		STD			STD	1	SMF		DEV		DPM	DEV	l l
COORDINATES	DP	М [DEV			DEV	454	DPN	<u>VI</u>	DEV		<u> </u>		
N14.0 E5.0	<lc< td=""><td>-13</td><td>10</td><td></td><td>518</td><td></td><td>454</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-13	10		518		454							
N14.0 E6.0	<lc< td=""><td>6</td><td></td><td><lc< td=""><td>78</td><td></td><td>403</td><td></td><td></td><td></td><td> </td><td></td><td></td><td>_ ,</td></lc<></td></lc<>	6		<lc< td=""><td>78</td><td></td><td>403</td><td></td><td></td><td></td><td> </td><td></td><td></td><td>_ ,</td></lc<>	78		403				 			_ ,
N14.0 E7.0	<lc< td=""><td>-13</td><td>10</td><td></td><td>570</td><td></td><td>460</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-13	10		570		460							
N14.0 E8.0	<lc< td=""><td>-13</td><td>10</td><td><lc< td=""><td>130</td><td></td><td>409</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-13	10	<lc< td=""><td>130</td><td></td><td>409</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	130		409							
N14.0 E9.0	<lc< td=""><td>-4</td><td>20</td><td><lc< td=""><td>-26</td><td></td><td>390</td><td></td><td></td><td></td><td>!</td><td></td><td>+-</td><td></td></lc<></td></lc<>	-4	20	<lc< td=""><td>-26</td><td></td><td>390</td><td></td><td></td><td></td><td>!</td><td></td><td>+-</td><td></td></lc<>	-26		390				!		+-	
N15.0 E1.0	<lc< td=""><td>-48</td><td>28</td><td></td><td>520</td><td></td><td>559</td><td></td><td></td><td></td><td><lc< td=""><td></td><td>38</td><td>71</td></lc<></td></lc<>	-48	28		520		559				<lc< td=""><td></td><td>38</td><td>71</td></lc<>		38	71
N15.0 E10.0	<lc< td=""><td>29</td><td>60</td><td></td><td>764</td><td></td><td>584</td><td></td><td>-1</td><td></td><td><lc< td=""><td></td><td>21</td><td>73</td></lc<></td></lc<>	29	60		764		584		-1		<lc< td=""><td></td><td>21</td><td>73</td></lc<>		21	73
N15.0 E11.0	<lc< td=""><td>-39</td><td>34</td><td></td><td>887</td><td></td><td></td><td><<u>Lc</u></td><td><u>-1</u></td><td>0</td><td></td><td></td><td>50</td><td>70</td></lc<>	-39	34		887			< <u>Lc</u>	<u>-1</u>	0			50	70
N15.0 E12.0	<lc< td=""><td>-19</td><td>43</td><td></td><td>917</td><td></td><td>599</td><td><lc< td=""><td>-1</td><td><u> </u></td><td>1</td><td></td><td>"</td><td></td></lc<></td></lc<>	-19	43		917		599	<lc< td=""><td>-1</td><td><u> </u></td><td>1</td><td></td><td>"</td><td></td></lc<>	-1	<u> </u>	1		"	
N15.0 E13.0	<lc< td=""><td>-19</td><td>43</td><td><lc< td=""><td>397</td><td></td><td>546</td><td></td><td></td><td></td><td> </td><td></td><td></td><td></td></lc<></td></lc<>	-19	43	<lc< td=""><td>397</td><td></td><td>546</td><td></td><td></td><td></td><td> </td><td></td><td></td><td></td></lc<>	397		546				 			
N15.0 E14.0		Α	NA			NA					-		_	
N15.0 E15.0	<lc< td=""><td>-48</td><td>28</td><td></td><td>306</td><td></td><td>536</td><td></td><td></td><td></td><td>#-</td><td></td><td></td><td></td></lc<>	-48	28		306		536				#-			
N15.0 E16.0	<lc< td=""><td>-19</td><td>43</td><td><lc< td=""><td>275</td><td></td><td>533</td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td></lc<></td></lc<>	-19	43	<lc< td=""><td>275</td><td></td><td>533</td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td></lc<>	275		533				-			
N15.0 E17.0	<lc< td=""><td>-10</td><td>47</td><td></td><td>550</td><td></td><td>562</td><td></td><td></td><td><u> </u></td><td></td><td></td><td>_</td><td></td></lc<>	-10	47		550		562			<u> </u>			_	
N15.0 E18.0	<lc< td=""><td>-10</td><td>47</td><td><lc< td=""><td>275</td><td></td><td>533</td><td></td><td></td><td><u> </u></td><td>-</td><td></td><td></td><td></td></lc<></td></lc<>	-10	47	<lc< td=""><td>275</td><td></td><td>533</td><td></td><td></td><td><u> </u></td><td>-</td><td></td><td></td><td></td></lc<>	275		533			<u> </u>	-			
N15.0 E18.0		JA	NA		NA	NA				ļ	-			
N15.0 E2.0	<lc .<="" td=""><td>0</td><td></td><td></td><td>642</td><td></td><td>572</td><td></td><td></td><td><u> </u></td><td>╂</td><td></td><td></td><td></td></lc>	0			642		572			<u> </u>	╂			
N15.0 E2.0 N15.0 E20.0		VA.	NA		NA	NA				<u> </u>	1			
N15.0 E20.0		VA.	NA		NA	NA					↓			
		-10		11	550		562				٠.		47	73
N15.0 E22.0	<lc< td=""><td>-19</td><td></td><td>_</td><td>1468</td><td></td><td>651</td><td><lc< td=""><td>2</td><td></td><td><lc< td=""><td></td><td>17</td><td>75</td></lc<></td></lc<></td></lc<>	-19		_	1468		651	<lc< td=""><td>2</td><td></td><td><lc< td=""><td></td><td>17</td><td>75</td></lc<></td></lc<>	2		<lc< td=""><td></td><td>17</td><td>75</td></lc<>		17	75
N15.0 E3.0	<lc< td=""><td>-10</td><td></td><td>-</td><td>948</td><td></td><td>602</td><td><lc< td=""><td>-1</td><td></td><td>) <lc< td=""><td></td><td>-4</td><td></td></lc<></td></lc<></td></lc<>	-10		-	948		602	<lc< td=""><td>-1</td><td></td><td>) <lc< td=""><td></td><td>-4</td><td></td></lc<></td></lc<>	-1) <lc< td=""><td></td><td>-4</td><td></td></lc<>		-4	
N15.0 E4.0	<lc< td=""><td>-10</td><td><u> </u></td><td></td><td>183</td><td></td><td>522</td><td></td><td></td><td></td><td>↓</td><td><u></u></td><td></td><td></td></lc<>	-10	<u> </u>		183		522				↓	<u></u>		
N15.0 E5.0	<lc< td=""><td>29</td><td>1</td><td><lc< td=""><td>397</td><td></td><td>546</td><td></td><td></td><td></td><td></td><td></td><td>-</td><td>7.</td></lc<></td></lc<>	29	1	<lc< td=""><td>397</td><td></td><td>546</td><td></td><td></td><td></td><td></td><td></td><td>-</td><td>7.</td></lc<>	397		546						-	7.
N15.0 E6.0	<lc< td=""><td>-19</td><td></td><td></td><td>1009</td><td>)</td><td>608</td><td></td><td></td><td>5</td><td>B <lc< td=""><td></td><td>33</td><td></td></lc<></td></lc<>	-19			1009)	608			5	B <lc< td=""><td></td><td>33</td><td></td></lc<>		33	
N15.0 E7.0	<lc< td=""><td>-10</td><td></td><td></td><td>703</td><td></td><td>578</td><td></td><td></td><td></td><td></td><td></td><td></td><td>0/</td></lc<>	-10			703		578							0/
N15.0 E8.0	<lc< td=""><td>19</td><td></td><td></td><td>917</td><td>7</td><td>599</td><td><lc< td=""><td></td><td>2</td><td>6 < Lc</td><td><u>`</u></td><td>42</td><td>80</td></lc<></td></lc<>	19			917	7	599	<lc< td=""><td></td><td>2</td><td>6 < Lc</td><td><u>`</u></td><td>42</td><td>80</td></lc<>		2	6 < Lc	<u>`</u>	42	80
N15.0 E9.0		NA 13	NA .	╫	NA	NA					1			74
N16.0 E1.0	<lc< td=""><td>C</td><td></td><td></td><td>1162</td><td>2</td><td>623</td><td><lc< td=""><td></td><td></td><td>6 < L</td><td></td><td>-8</td><td>7</td></lc<></td></lc<>	C			1162	2	623	<lc< td=""><td></td><td></td><td>6 < L</td><td></td><td>-8</td><td>7</td></lc<>			6 < L		-8	7
N16.0 E10.0	- ``	67			1009	9	608				8 < L		4	7
N16.0 E11.0	<lc< td=""><td>10</td><td></td><td></td><td>1070</td><td></td><td>614</td><td><lc< td=""><td>-</td><td><u>: </u></td><td>0 <l0< td=""><td></td><td>21</td><td></td></l0<></td></lc<></td></lc<>	10			1070		614	<lc< td=""><td>-</td><td><u>: </u></td><td>0 <l0< td=""><td></td><td>21</td><td></td></l0<></td></lc<>	-	<u>: </u>	0 <l0< td=""><td></td><td>21</td><td></td></l0<>		21	
N16.0 E12.0	<lc< td=""><td>10</td><td></td><td></td><td>887</td><td></td><td>596</td><td><lc< td=""><td>_</td><td>1</td><td>0 <l0< td=""><td><u> </u></td><td>0</td><td>7</td></l0<></td></lc<></td></lc<>	10			887		596	<lc< td=""><td>_</td><td>1</td><td>0 <l0< td=""><td><u> </u></td><td>0</td><td>7</td></l0<></td></lc<>	_	1	0 <l0< td=""><td><u> </u></td><td>0</td><td>7</td></l0<>	<u> </u>	0	7
N16.0 E13.0			NA NA	' 	NA	NA								
N16.0 E14.0		NA NA	NA NA		NA	NA								
N16.0 E15.0				- 1	67:		575	5						
N16.0 E16.0	<lc< td=""><td>-19</td><td></td><td>4 <lc< td=""><td>36</td><td>_+</td><td>543</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-19		4 <lc< td=""><td>36</td><td>_+</td><td>543</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	36	_+	543							
N16.0 E17.0	<lc< td=""><td>10</td><td></td><td>4 < LC</td><td>9:</td><td></td><td>512</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	10		4 < LC	9:		512							
N16.0 E18.0	<lc< td=""><td>-39</td><td></td><td>3 <lc< td=""><td>36</td><td></td><td>543</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-39		3 <lc< td=""><td>36</td><td></td><td>543</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	36		543							
N16.0 E19.0	<lc< td=""><td>-19</td><td></td><td>4</td><td>70</td><td></td><td>578</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-19		4	70		578							
N16.0 E2.0	<lc< td=""><td>-39</td><td></td><td>7 <lc< td=""><td>24</td><td></td><td>529</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-39		7 <lc< td=""><td>24</td><td></td><td>529</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	24		529							
N16.0 E20.0	<lc< td=""><td>-10</td><td></td><td>4</td><td>52</td><td>_</td><td>559</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-10		4	52	_	559							
N16.0 E21.0	<lc< td=""><td>11</td><td></td><td>3 <lc< td=""><td></td><td></td><td>546</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	11		3 <lc< td=""><td></td><td></td><td>546</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			546							
N16.0 E22.0	<lc< td=""><td>-1</td><td></td><td>7 <lc< td=""><td></td><td></td><td>530</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-1		7 <lc< td=""><td></td><td></td><td>530</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			530							
N16.0 E3.0	<lc< td=""><td>1</td><td></td><td></td><td>42</td><td></td><td>54</td><td></td><td></td><td></td><td></td><td></td><td></td><td>į.</td></lc<>	1			42		54							į.
N16.0 E4.0	<lc< td=""><td>-1</td><td></td><td>7</td><td>48</td><td></td><td>55</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-1		7	48		55							
N16.0 E5.0	<lc< td=""><td>-1</td><td></td><td>7</td><td>42</td><td></td><td>54</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-1		7	42		54							
N16.0 E6.0	<lc< td=""><td></td><td></td><td>1</td><td></td><td></td><td>53</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			1			53							
N16.0 E7.0	<lc< td=""><td>-1</td><td></td><td>3 <lc< td=""><td>48</td><td></td><td>55</td><td></td><td></td><td>•</td><td></td><td></td><td></td><td><u> </u></td></lc<></td></lc<>	-1		3 <lc< td=""><td>48</td><td></td><td>55</td><td></td><td></td><td>•</td><td></td><td></td><td></td><td><u> </u></td></lc<>	48		55			•				<u> </u>
N16.0 E8.0	<lc< td=""><td>-3</td><td></td><td>4</td><td>122</td><td></td><td></td><td>9 <lc< td=""><td></td><td>-1</td><td>0 <l< td=""><td>.c</td><td>-17</td><td></td></l<></td></lc<></td></lc<>	-3		4	122			9 <lc< td=""><td></td><td>-1</td><td>0 <l< td=""><td>.c</td><td>-17</td><td></td></l<></td></lc<>		-1	0 <l< td=""><td>.c</td><td>-17</td><td></td></l<>	.c	-17	
N16.0 E9.0	<lc< td=""><td>-1</td><td></td><td>7</td><td></td><td></td><td>47</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-1		7			47							
N2.0 E-1.0		4		5 < Lc		33		8 <lc< td=""><td></td><td>-1</td><td>0 <1</td><td>С</td><td>-42</td><td></td></lc<>		-1	0 <1	С	-42	
N2.0 E-2.0	<lc< td=""><td></td><td></td><td>9</td><td></td><td>22</td><td>49</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			9		22	49							
N2.0 E0.0				37 <lc< td=""><td></td><td>59</td><td>42</td><td></td><td></td><td>_</td><td></td><td></td><td></td><td></td></lc<>		59	42			_				
N2.0 E1.0	<lc< td=""><td></td><td></td><td>20</td><td></td><td>33</td><td>43</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			20		33	43							
N2.0 E10.0	<lc< td=""><td></td><td>6</td><td>27</td><td></td><td>39</td><td></td><td>. U</td><td></td><td>ground.</td><td></td><td></td><td></td><td></td></lc<>		6	27		39		. U		ground.				

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

									Т	ΔΝ	SFER	ABI	E			
[DIRECT			0.00	CM	AL DE	1A/100			BI	TA-GAM	MA/10	00 SQ	СМ
	ALPHA	100 8	SQ CM		GAMMA/10		CM		APL	Tsī		<u> </u>	SMPL		STD	
LOCATION/ITEM	SMPL	- 1	STD		SMPL	STD	1		PM	DE			DPM		DEV	
COORDINATES	DPM	-	DEV		DPM	DEV			- ·	_		<l< td=""><td></td><td>-38</td><td></td><td>74</td></l<>		-38		74
V2.0 E11.0		52	49		1218			<lc< td=""><td></td><td>' </td><td></td><td>-</td><td></td><td></td><td></td><td></td></lc<>		' 		-				
N2.0 E12.0		24	37		622		465					<	<u></u>	-13		76
12.0 E 12.0	<lc< td=""><td>6</td><td>27</td><td></td><td>1347</td><td></td><td>537</td><td><lc_< td=""><td></td><td>Ч-</td><td></td><td>-</td><td></td><td></td><td></td><td></td></lc_<></td></lc<>	6	27		1347		537	<lc_< td=""><td></td><td>Ч-</td><td></td><td>-</td><td></td><td></td><td></td><td></td></lc_<>		Ч-		-				
N2.0 E13.0 N2.0 E14.0	<lc< td=""><td>6</td><td>27</td><td></td><td>596</td><td></td><td>463</td><td></td><td></td><td></td><td></td><td>1-</td><td></td><td></td><td></td><td></td></lc<>	6	27		596		463					1-				
	1 120	61	52		389		440					╀				
V2.0 E15.0	NA NA		NA		NA	NA	1			┿		₩-				
V2.0 E16.0	NA NA		NA		NA	NA						-		-38		74
N2.0 E17.0	13/2	24	37		1114		515	<lc< td=""><td></td><td>1</td><td></td><td><u> </u></td><td><u>.c</u></td><td>-50</td><td></td><td></td></lc<>		1		<u> </u>	<u>.c</u>	-50		
V2.0 E18.0	1	-4	20		725		476					1-				
N2.0 E19.0	<lc< td=""><td>24</td><td></td><td><lc< td=""><td>181</td><td></td><td>416</td><td></td><td></td><td>\perp</td><td></td><td>1</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	24		<lc< td=""><td>181</td><td></td><td>416</td><td></td><td></td><td>\perp</td><td></td><td>1</td><td></td><td></td><td></td><td></td></lc<>	181		416			\perp		1				
N2.0 E2.0		-4	20		466		449					1				
N2.0 E20.0	<lc< td=""><td></td><td></td><td></td><td>570</td><td></td><td>460</td><td></td><td></td><td></td><td></td><td>_</td><td></td><td></td><td></td><td></td></lc<>				570		460					_				
N2.0 E21.0	<lc< td=""><td>-13</td><td></td><td><lc< td=""><td>78</td><td></td><td>403</td><td></td><td></td><td></td><td></td><td>_</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-13		<lc< td=""><td>78</td><td></td><td>403</td><td></td><td></td><td></td><td></td><td>_</td><td></td><td></td><td></td><td></td></lc<>	78		403					_				
N2.0 E22.0	<lc< td=""><td>-4</td><td></td><td><lc< td=""><td>. 18</td><td></td><td>416</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<></td></lc<>	-4		<lc< td=""><td>. 18</td><td></td><td>416</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<>	. 18		416								<u> </u>	
N2.0 E3.0	<lc< td=""><td>-4</td><td></td><td></td><td>674</td><td>_</td><td>471</td><td></td><td></td><td>T</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-4			674	_	471			T						
N2.0 E4.0	<lc< td=""><td>15</td><td></td><td></td><td>41:</td><td></td><td>443</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	15			41:		443									
N2.0 E5.0	<lc< td=""><td>4</td><td></td><td></td><td>38</td><td></td><td>440</td><td></td><td></td><td></td><td></td><td>\blacksquare</td><td></td><td></td><td><u> </u></td><td></td></lc<>	4			38		440					\blacksquare			<u> </u>	
N2.0 E6.0		33					449					T				
N2.0 E7.0		24			46		437			\dashv						
N2.0 E8.0	<lc< td=""><td>-13</td><td></td><td></td><td>36</td><td>_</td><td>397</td><td>╂</td><td></td><td>_</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-13			36	_	397	╂		_						
N2.0 E9.0	<lc< td=""><td>-13</td><td></td><td>) <lc< td=""><td>2</td><td>_</td><td></td><td><lc< td=""><td></td><td>-1</td><td></td><td>0 <</td><td>Lc</td><td>-42</td><td></td><td>73</td></lc<></td></lc<></td></lc<>	-13) <lc< td=""><td>2</td><td>_</td><td></td><td><lc< td=""><td></td><td>-1</td><td></td><td>0 <</td><td>Lc</td><td>-42</td><td></td><td>73</td></lc<></td></lc<>	2	_		<lc< td=""><td></td><td>-1</td><td></td><td>0 <</td><td>Lc</td><td>-42</td><td></td><td>73</td></lc<>		-1		0 <	Lc	-42		73
N2.5 E-0.5	<lc< td=""><td>-7</td><td></td><td><u> </u></td><td>67</td><td></td><td></td><td>1</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td><td></td></lc<>	-7		<u> </u>	67			1				1				
N2.5 E-1.5	<lc< td=""><td>11</td><td></td><td></td><td>23</td><td></td><td>457</td><td>-</td><td></td><td>2</td><td></td><td>6 4</td><td>Lc</td><td>-17</td><td>7</td><td>73</td></lc<>	11			23		457	-		2		6 4	Lc	-17	7	73
N2.5 E0.5	<lc< td=""><td>-18</td><td>3 3</td><td>o </td><td>75</td><td></td><td></td><td><lc< td=""><td></td><td>-4</td><td></td><td>-</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-18	3 3	o	75			<lc< td=""><td></td><td>-4</td><td></td><td>-</td><td></td><td></td><td></td><td></td></lc<>		-4		-				
N2.5 E1.5	<lc< td=""><td>- (</td><td>9 4</td><td>3</td><td>48</td><td></td><td>481</td><td></td><td></td><td></td><td></td><td>0 <</td><td>-1 c</td><td>-63</td><td>3</td><td>6</td></lc<>	- (9 4	3	48		481					0 <	-1 c	-63	3	6
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N2.5 E10.5	<lc< td=""><td>-</td><td></td><td>5</td><td>88</td><td>3</td><td>522</td><td></td><td></td><td>2</td><td></td><td>0 4</td><td></td><td></td><td>4</td><td>7</td></lc<>	-		5	88	3	522			2		0 4			4	7
N2.5 E11.5	<lc< td=""><td></td><td></td><td>5</td><td>88</td><td>3</td><td></td><td>· CLC</td><td></td><td>-11</td><td></td><td>-#-</td><td><lc< td=""><td>1</td><td>7</td><td>7</td></lc<></td></lc<>			5	88	3		· CLC		-11		-#-	<lc< td=""><td>1</td><td>7</td><td>7</td></lc<>	1	7	7
N2.5 E12.5	<lc< td=""><td></td><td></td><td>5</td><td>310</td><td>)5</td><td>708</td><td><lc< td=""><td></td><td>-11</td><td></td><td></td><td></td><td></td><td></td><td>7</td></lc<></td></lc<>			5	310)5	708	<lc< td=""><td></td><td>-11</td><td></td><td></td><td></td><td></td><td></td><td>7</td></lc<>		-11						7
N2.5 E13.5	- <lc< td=""><td></td><td></td><td>5</td><td>275</td><td>57</td><td>682</td><td></td><td>:</td><td>-1</td><td></td><td></td><td><lc< td=""><td>-1</td><td></td><td>7</td></lc<></td></lc<>			5	275	57	682		:	-1			<lc< td=""><td>-1</td><td></td><td>7</td></lc<>	-1		7
N2.5 E14.5				oll	141	19	572	2 < L c	;	-1		<u> </u>	<lc< td=""><td>- 1.</td><td></td><td></td></lc<>	- 1.		
N2.5 E15.5	<lc_< td=""><td></td><td>NA S</td><td>ੱ∥</td><td>NA</td><td>N/</td><td>4</td><td></td><td></td><td></td><td></td><td>_#</td><td></td><td></td><td></td><td></td></lc_<>		NA S	ੱ∥	NA	N/	4					_#				
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N2.5 E18.5	<lc< td=""><td></td><td></td><td>3 <l< td=""><td></td><td>21</td><td>463</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<></td></lc<>			3 <l< td=""><td></td><td>21</td><td>463</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<>		21	463									
N2.5 E19.5	<lc< td=""><td></td><td><u> </u></td><td></td><td><u> </u></td><td></td><td>41</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		<u> </u>		<u> </u>		41									
N2.5 E2.5	<l¢< td=""><td></td><td></td><td>7 <l0< td=""><td></td><td>21</td><td>46</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l0<></td></l¢<>			7 <l0< td=""><td></td><td>21</td><td>46</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l0<>		21	46									
N2.5 E20.5	<lc< td=""><td></td><td></td><td>35 <l< td=""><td></td><td>21</td><td>46</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<></td></lc<>			35 <l< td=""><td></td><td>21</td><td>46</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<>		21	46									
N2.5 E21.5	<lc< td=""><td></td><td></td><td>13 <l0< td=""><td></td><td></td><td></td><td>8 <l< td=""><td></td><td>2</td><td></td><td>6</td><td><lc< td=""><td>-3</td><td>3</td><td>7</td></lc<></td></l<></td></l0<></td></lc<>			13 <l0< td=""><td></td><td></td><td></td><td>8 <l< td=""><td></td><td>2</td><td></td><td>6</td><td><lc< td=""><td>-3</td><td>3</td><td>7</td></lc<></td></l<></td></l0<>				8 <l< td=""><td></td><td>2</td><td></td><td>6</td><td><lc< td=""><td>-3</td><td>3</td><td>7</td></lc<></td></l<>		2		6	<lc< td=""><td>-3</td><td>3</td><td>7</td></lc<>	-3	3	7
N2.5 E3.5	<lc< td=""><td></td><td></td><td>10</td><td>11</td><td></td><td></td><td>4 < L</td><td></td><td>2</td><td></td><td>6</td><td><lc< td=""><td>-3</td><td>3</td><td>7</td></lc<></td></lc<>			10	11			4 < L		2		6	<lc< td=""><td>-3</td><td>3</td><td>7</td></lc<>	-3	3	7
N2.5 E4.5	<lc< td=""><td>-</td><td></td><td>30</td><td></td><td>53</td><td></td><td></td><td><u> </u></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-		30		53			<u> </u>							
N2.5 E5.5	<lc< td=""><td></td><td></td><td>35</td><td></td><td>62</td><td>48</td><td></td><td></td><td></td><td></td><td>_</td><td></td><td></td><td></td><td></td></lc<>			35		62	48					_				
N2.5 E6.5	<lc< td=""><td></td><td>0</td><td>40</td><td></td><td>55</td><td>47</td><td></td><td></td><td>-1</td><td></td><td>0</td><td><lc< td=""><td>-2</td><td>29</td><td></td></lc<></td></lc<>		0	40		55	47			-1		0	<lc< td=""><td>-2</td><td>29</td><td></td></lc<>	-2	29	
N2.5 E7.5	<lc< td=""><td>_</td><td>18</td><td>30</td><td></td><td>03</td><td></td><td>4 < L</td><td><u>c</u></td><td></td><td>}</td><td></td><td></td><td></td><td></td><td></td></lc<>	_	18	30		03		4 < L	<u>c</u>		}					
NZ.5 E7.5	<lc< td=""><td></td><td></td><td>43</td><td></td><td>82</td><td>48</td><td></td><td></td><td></td><td> </td><td></td><td></td><td></td><td></td><td></td></lc<>			43		82	48				 					
N2.5 E8.5	<lc< td=""><td></td><td>28</td><td>24</td><td></td><td>303</td><td>51</td><td></td><td></td><td></td><td>┼</td><td>-1</td><td></td><td></td><td></td><td></td></lc<>		28	24		303	51				┼	-1				
N2.5 E9.5	<lc< td=""><td></td><td></td><td>27</td><td></td><td>18</td><td>48</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>_</td><td></td></lc<>			27		18	48								_	
N3.0 E-1.0			20	32 <l< td=""><td>.c</td><td>55</td><td></td><td>19</td><td></td><td></td><td> </td><td></td><td></td><td></td><td></td><td></td></l<>	.c	55		19			 					
N3.0 E-2.0	- 		6	27 <l< td=""><td></td><td>104</td><td></td><td>)6</td><td></td><td></td><td> </td><td></td><td></td><td></td><td></td><td></td></l<>		104)6			 					
N3.0 E0.0	<lc< td=""><td></td><td>24</td><td>37</td><td></td><td>140</td><td></td><td>16</td><td></td><td></td><td><u> </u></td><td></td><td></td><td></td><td>21</td><td></td></lc<>		24	37		140		16			<u> </u>				21	
N3.0 E1.0	#			20		959	5(00 <l< td=""><td>_C</td><td>1</td><td></td><td></td><td><lc< td=""><td></td><td></td><td></td></lc<></td></l<>	_C	1			<lc< td=""><td></td><td></td><td></td></lc<>			
N3.0 E10.0	<lc< td=""><td></td><td>-4</td><td>37</td><td></td><td>176</td><td></td><td>)> ec</td><td></td><td></td><td></td><td></td><td><lc< td=""><td></td><td>-8</td><td></td></lc<></td></lc<>		-4	37		176)> ec					<lc< td=""><td></td><td>-8</td><td></td></lc<>		-8	
N3.0 E11.0			24			829		87 <		- 7	2	6	<lc< td=""><td></td><td>13</td><td></td></lc<>		13	
N3.0 E12.0	<lc< td=""><td></td><td>15</td><td>33</td><td></td><td></td><td></td><td>03</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		15	33				03								
N3.0 E13.0	<lc< td=""><td></td><td>-4</td><td></td><td></td><td>399</td><td></td><td>42 <</td><td>_C</td><td></td><td>2</td><td></td><td><lc< td=""><td></td><td>25</td><td></td></lc<></td></lc<>		-4			399		42 <	_C		2		<lc< td=""><td></td><td>25</td><td></td></lc<>		25	
N3.0 E14.0			33	41				46 <				0	<lc< td=""><td></td><td>-8 </td><td></td></lc<>		-8	
N3.0 E15.0			24	37	tv which car	042										

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

,			DIRECT					TR	ANSFER	AB	LE			\Box
	41.511			DETA G	Δ N A N A Δ / 1 C	00 SQ CM	ALPH	IA/100	SQ CM	E	BETA-GAM			M
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OCATION/ITEM	SMF	_	DEV		PM	DEV	D	PM .	DEV		DPM		DEV	
COORDINATES	DP		37	, D.	6063	871	<lc< td=""><td>2</td><td></td><td>1</td><td></td><td>-54</td><td></td><td>72</td></lc<>	2		1		-54		72
13.0 E16.0		24 6	27		4405	770		8	10	<	Lc	0		78
13.0 E17.0	<lc< td=""><td>15</td><td>33</td><td></td><td>648</td><td>468</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	15	33		648	468								
13.0 E18.0	<lc< td=""><td></td><td>20</td><td></td><td>725</td><td>476</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		20		725	476								
13.0 E19.0	<lc< td=""><td>-4</td><td>33</td><td>ļ</td><td>622</td><td>465</td><td>1</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-4	33	ļ	622	465	1							
13.0 E2.0	<lc< td=""><td>15</td><td></td><td>rl 0</td><td>155</td><td>413</td><td></td><td></td><td></td><td>T</td><td></td><td></td><td></td><td></td></lc<>	15		rl 0	155	413				T				
13.0 E20.0	<lc< td=""><td>6</td><td></td><td><lc <lc< td=""><td>207</td><td>419</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td><td></td></lc<></lc </td></lc<>	6		<lc <lc< td=""><td>207</td><td>419</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td><td></td></lc<></lc 	207	419				1				
N3.0 E21.0	<lc< td=""><td>6</td><td>27</td><td>CLC .</td><td>337</td><td>434</td><td></td><td></td><td>†</td><td>T</td><td></td><td></td><td></td><td></td></lc<>	6	27	CLC .	337	434			†	T				
N3.0 E22.0	<u> </u>	125			803				1					
V3.0 E3.0	Ⅱ	70	55		622			5		3 <	Lc	-4		77
V3.0 E4.0	<lc< td=""><td>15</td><td></td><td>ļ</td><td>674</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td><td></td><td></td></lc<>	15		ļ	674				1					
V3.0 E5.0	<lc< td=""><td>-4</td><td></td><td></td><td>725</td><td></td><td></td><td></td><td>T</td><td>1</td><td></td><td></td><td></td><td></td></lc<>	-4			725				T	1				
V3.0 E6.0	<lc< td=""><td>15</td><td></td><td></td><td>751</td><td></td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td><td></td></lc<>	15			751					1				
N3.0 E7.0		33		 					1	1				
N3.0 E8.0	<lc< td=""><td>6</td><td></td><td>Ⅱ</td><td>466</td><td></td><td></td><td></td><td> </td><td>1</td><td><u></u></td><td></td><td></td><td></td></lc<>	6		Ⅱ	466				 	1	<u></u>			
V3.0 E9.0	<lc< td=""><td>15</td><td></td><td></td><td>518</td><td></td><td></td><td></td><td>-</td><td>+</td><td></td><td></td><td></td><td></td></lc<>	15			518				-	+				
N3.5 E-0.5	<lc< td=""><td>11</td><td></td><td><lc< td=""><td>-207</td><td></td><td></td><td></td><td>-</td><td>1</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	11		<lc< td=""><td>-207</td><td></td><td></td><td></td><td>-</td><td>1</td><td></td><td></td><td></td><td></td></lc<>	-207				-	1				
N3.5 E-1.5		20		<lc< td=""><td>285</td><td></td><td></td><td></td><td> </td><td>+</td><td></td><td></td><td></td><td></td></lc<>	285				 	+				
N3.5 E0.5	<lc< td=""><td>-9</td><td></td><td></td><td>375</td><td><u> </u></td><td></td><td></td><td>-</td><td>+</td><td></td><td></td><td></td><td></td></lc<>	-9			375	<u> </u>			-	+				
N3.5 E1.5	<lc< td=""><td>-6</td><td></td><td></td><td>375</td><td></td><td></td><td></td><td>┪</td><td>0 <</td><td><lc< td=""><td>-25</td><td></td><td>72</td></lc<></td></lc<>	-6			375				┪	0 <	<lc< td=""><td>-25</td><td></td><td>72</td></lc<>	-25		72
N3.5 E10.5	<lc< td=""><td></td><td></td><td></td><td>1526</td><td></td><td>2 < L C</td><td></td><td><u>' </u></td><td>┧</td><td></td><td></td><td></td><td></td></lc<>				1526		2 < L C		<u>' </u>	┧				
N3.5 E11.5	<lc< td=""><td>-9</td><td></td><td><lc< td=""><td>348</td><td></td><td></td><td></td><td></td><td>+</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-9		<lc< td=""><td>348</td><td></td><td></td><td></td><td></td><td>+</td><td></td><td></td><td></td><td></td></lc<>	348					+				
N3.5 E12.5	<lc< td=""><td>9</td><td></td><td></td><td>37</td><td></td><td></td><td></td><td>1</td><td>۸.</td><td><lc< td=""><td>8</td><td><u> </u></td><td>7(</td></lc<></td></lc<>	9			37				1	۸.	<lc< td=""><td>8</td><td><u> </u></td><td>7(</td></lc<>	8	<u> </u>	7(
N3.5 E13.5	<lc< td=""><td></td><td></td><td></td><td>232</td><td></td><td>9 <lc< td=""><td></td><td>' </td><td></td><td><lc< td=""><td>-50</td><td></td><td>7</td></lc<></td></lc<></td></lc<>				232		9 <lc< td=""><td></td><td>' </td><td></td><td><lc< td=""><td>-50</td><td></td><td>7</td></lc<></td></lc<>		' 		<lc< td=""><td>-50</td><td></td><td>7</td></lc<>	-50		7
N3.5 E14.5	<lc< td=""><td>28</td><td></td><td></td><td>736</td><td></td><td>9 <lc< td=""><td></td><td></td><td>-</td><td>~</td><td></td><td></td><td></td></lc<></td></lc<>	28			736		9 <lc< td=""><td></td><td></td><td>-</td><td>~</td><td></td><td></td><td></td></lc<>			-	~			
N3.5 E15.5	<lc< td=""><td>-28</td><td></td><td></td><td>53</td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td>1</td><td></td></lc<>	-28			53					-			1	
N3.5 E17.5	<lc< td=""><td>18</td><td></td><td></td><td>125</td><td></td><td></td><td></td><td></td><td>\dashv</td><td></td><td></td><td><u> </u></td><td></td></lc<>	18			125					\dashv			<u> </u>	
N3.5 E18.5	<lc< td=""><td>-28</td><td>3 24</td><td><lc< td=""><td>26</td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-28	3 24	<lc< td=""><td>26</td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td></lc<>	26					-				
N3.5 E19.5	<lc< td=""><td>-!</td><td>9 3</td><td><lc< td=""><td>29</td><td></td><td></td><td></td><td></td><td>-#</td><td><u></u></td><td></td><td><u> </u></td><td></td></lc<></td></lc<>	-!	9 3	<lc< td=""><td>29</td><td></td><td></td><td></td><td></td><td>-#</td><td><u></u></td><td></td><td><u> </u></td><td></td></lc<>	29					-#	<u></u>		<u> </u>	
N3.5 E2.5	1	6	4 6	2	69					-			 	
N3.5 E20.5	<lc< td=""><td>-2</td><td>8 2</td><td>4</td><td>50</td><td></td><td></td><td></td><td></td><td>╝</td><td></td><td></td><td> </td><td></td></lc<>	-2	8 2	4	50					╝			 	
N3.5 E21.5	<lc< td=""><td></td><td>0 4</td><td></td><td>48</td><td></td><td></td><td></td><td></td><td>6</td><td><lc< td=""><td>-21</td><td> </td><td>7</td></lc<></td></lc<>		0 4		48					6	<lc< td=""><td>-21</td><td> </td><td>7</td></lc<>	-21	 	7
N3.5 E3.5	<lc< td=""><td></td><td>9 4</td><td>3</td><td>107</td><td></td><td>0 <lc< td=""><td></td><td>2</td><td>9</td><td><u> </u></td><td></td><td> </td><td></td></lc<></td></lc<>		9 4	3	107		0 <lc< td=""><td></td><td>2</td><td>9</td><td><u> </u></td><td></td><td> </td><td></td></lc<>		2	9	<u> </u>		 	
N3.5 E4.5	<lc< td=""><td></td><td>0 4</td><td></td><td>166</td><td></td><td></td><td></td><td></td><td></td><td>-1 -</td><td>-42</td><td>, </td><td>7</td></lc<>		0 4		166						-1 -	-42	, 	7
N3.5 E5.5	<lc< td=""><td>1</td><td>8 4</td><td>7</td><td>37</td><td></td><td></td><td></td><td>8</td><td>10</td><td><lc< td=""><td>-42</td><td>1</td><td></td></lc<></td></lc<>	1	8 4	7	37				8	10	<lc< td=""><td>-42</td><td>1</td><td></td></lc<>	-42	1	
N3.5 E6.5	<lc< td=""><td>-1</td><td>8 3</td><td>0</td><td>61</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td></lc<>	-1	8 3	0	61								-	
N3.5 E7.5	<lc< td=""><td></td><td>9 3</td><td>5</td><td>53</td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td>+</td><td></td></lc<>		9 3	5	53					-			+	
N3.5 E8.5	- 			5	61		5			_		46	. 	
N3.5 E8.5 N3.5 E9.5				5	93		7 <lc< td=""><td></td><td>2</td><td>Ы</td><td><lc< td=""><td>40</td><td></td><td></td></lc<></td></lc<>		2	Ы	<lc< td=""><td>40</td><td></td><td></td></lc<>	40		
N4.0 E-1.0	<lc< td=""><td><u> </u></td><td></td><td>9 < Lc</td><td></td><td></td><td>54</td><td></td><td></td><td></td><td></td><td></td><td>+</td><td></td></lc<>	<u> </u>		9 < Lc			54						+	
N4.0 E-1.0 N4.0 E-2.0	<lc< td=""><td></td><td></td><td>7</td><td>51</td><td> 1</td><td>37</td><td></td><td></td><td> </td><td></td><td></td><td>-</td><td></td></lc<>			7	51	1	37						-	
	<lc< td=""><td></td><td></td><td>ol</td><td></td><td></td><td>13</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			ol			13							
N4.0 E0.0	- 11 - 1-0			5			51					2.	1	
N4.0 E1.0				7	103		08 <lc< td=""><td></td><td>-1</td><td></td><td><lc< td=""><td>-2°</td><td></td><td></td></lc<></td></lc<>		-1		<lc< td=""><td>-2°</td><td></td><td></td></lc<>	-2°		
N4.0 E10.0	<lc< td=""><td></td><td></td><td>3</td><td>10:</td><td></td><td>08 < Lo</td><td><u> </u></td><td>-1</td><td>U</td><td><lc< td=""><td>-3.</td><td>-</td><td></td></lc<></td></lc<>			3	10:		08 < Lo	<u> </u>	-1	U	<lc< td=""><td>-3.</td><td>-</td><td></td></lc<>	-3.	-	
N4.0 E11.0	<lc< td=""><td></td><td></td><td>3</td><td>6</td><td></td><td>86</td><td></td><td></td><td> </td><td></td><td>3</td><td>2</td><td></td></lc<>			3	6		86					3	2	
N4.0 E12.0	1-5			17	. 9		00 <la< td=""><td></td><td>2</td><td>6</td><td><lc< td=""><td>٥.</td><td>~</td><td></td></lc<></td></la<>		2	6	<lc< td=""><td>٥.</td><td>~</td><td></td></lc<>	٥.	~	
N4.0 E13.0	<lc< td=""><td></td><td></td><td>7</td><td>6</td><td></td><td>71</td><td></td><td></td><td></td><td>al c</td><td></td><td>2</td><td></td></lc<>			7	6		71				al c		2	
N4.0 E14.0	<lc< td=""><td></td><td></td><td>33</td><td>25</td><td></td><td>40 <l0< td=""><td></td><td>-1</td><td></td><td><lc< td=""><td>-3</td><td></td><td></td></lc<></td></l0<></td></lc<>			33	25		40 <l0< td=""><td></td><td>-1</td><td></td><td><lc< td=""><td>-3</td><td></td><td></td></lc<></td></l0<>		-1		<lc< td=""><td>-3</td><td></td><td></td></lc<>	-3		
N4.0 E15.0				27		77 4	82 <l< td=""><td>3</td><td>-1</td><td>0</td><td><lc< td=""><td>-3</td><td>의</td><td></td></lc<></td></l<>	3	-1	0	<lc< td=""><td>-3</td><td>의</td><td></td></lc<>	-3	의	
N4.0 E16.0	<lc< td=""><td></td><td></td><td>20</td><td></td><td></td><td>74</td><td></td><td></td><td></td><td><u> </u></td><td></td><td></td><td></td></lc<>			20			74				<u> </u>			
N4.0 E17.0	<lc< td=""><td></td><td></td><td>27</td><td></td><td></td><td>57</td><td></td><td></td><td></td><td>ļ</td><td></td><td></td><td></td></lc<>			27			57				ļ			
N4.0 E18.0	<lc< td=""><td></td><td></td><td>20</td><td></td><td></td><td>10 <l< td=""><td>С</td><td>-1</td><td></td><td><lc< td=""><td>-6</td><td></td><td></td></lc<></td></l<></td></lc<>			20			10 <l< td=""><td>С</td><td>-1</td><td></td><td><lc< td=""><td>-6</td><td></td><td></td></lc<></td></l<>	С	-1		<lc< td=""><td>-6</td><td></td><td></td></lc<>	-6		
N4.0 E19.0	<lc< td=""><td></td><td></td><td>27</td><td></td><td></td><td>98 <l< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td>-1</td><td>/ </td><td></td></lc<></td></l<></td></lc<>			27			98 <l< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td>-1</td><td>/ </td><td></td></lc<></td></l<>		-1	0	<lc< td=""><td>-1</td><td>/ </td><td></td></lc<>	-1	/	
N4.0 E2.0	<lc< td=""><td></td><td></td><td>27</td><td></td><td></td><td>54</td><td></td><td></td><td></td><td>1</td><td></td><td>l</td><td></td></lc<>			27			54				1		l	

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

									NOTE	2 4 12	1 5			
[1	DIRECT						ANSFER	TB	ETA-GAN	AMA/10	n so (СМ
	ALPHA/	100 \$	SQ CM	BETA-	3AMMA/10				SQ CM	+-	SMPL		STD	
OCATION/ITEM	SMPL		STD	S	MPL	STD	SM		STD		DPM		DEV	į
COORDINATES	DPM		DEV	[DPM	DEV	DI	M	DEV	╂	D1 1V1			
N4.0 E21.0	<lc< td=""><td>-4</td><td>20</td><td></td><td>570</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-4	20		570									
14.0 E22.0	<lc< td=""><td>15</td><td>33</td><td></td><td>440</td><td></td><td></td><td></td><td></td><td>╂</td><td></td><td></td><td></td><td></td></lc<>	15	33		440					╂				
N4.0 E3.0		24	37		415		<u> </u>			<u> </u>		4		78
N4.0 E4.0	<lc< td=""><td>-4</td><td>20</td><td></td><td>337</td><td></td><td><lc< td=""><td>-1</td><td></td><td>7</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-4	20		337		<lc< td=""><td>-1</td><td></td><td>7</td><td></td><td></td><td></td><td></td></lc<>	-1		7				
N4.0 E5.0		42	45	<lc< td=""><td>311</td><td>431</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	311	431								
N4.0 E6.0	-	52	49		751				ļ	+-				
N4.0 E7.0		24	37	<lc< td=""><td>285</td><td></td><td></td><td></td><td><u> </u></td><td>╫</td><td></td><td></td><td></td><td></td></lc<>	285				<u> </u>	╫				
N4.0 E8.0	<lc< td=""><td>6</td><td>27</td><td></td><td>492</td><td></td><td> </td><td></td><td> </td><td>-1-</td><td></td><td></td><td></td><td></td></lc<>	6	27		492		 		 	-1-				
N4.0 E9.0	<lc< td=""><td>15</td><td>33</td><td></td><td>363</td><td></td><td>!</td><td></td><td><u> </u></td><td>0 <</td><td>Lc</td><td>-42</td><td></td><td>73</td></lc<>	15	33		363		!		<u> </u>	0 <	Lc	-42		73
N4.5 E-0.5	<lc< td=""><td>-7</td><td>7</td><td></td><td>959</td><td></td><td><lc< td=""><td>-1</td><td> </td><td><u> </u></td><td>LU</td><td>-7-</td><td></td><td></td></lc<></td></lc<>	-7	7		959		<lc< td=""><td>-1</td><td> </td><td><u> </u></td><td>LU</td><td>-7-</td><td></td><td></td></lc<>	-1	 	<u> </u>	LU	-7-		
N4.5 E-0.5		20	32		466		*		 					
	<lc< td=""><td>0</td><td>40</td><td></td><td>535</td><td></td><td></td><td></td><td> </td><td>#-</td><td></td><td></td><td></td><td></td></lc<>	 0	40		535				 	#-				
N4.5 E0.5	<lc< td=""><td>-28</td><td>24</td><td></td><td>402</td><td></td><td></td><td></td><td>ļ</td><td>_ -</td><td>1 -</td><td>21</td><td></td><td>77</td></lc<>	-28	24		402				ļ	_ -	1 -	21		77
N4.5 E1.5	#	46			883		-	2		6 <		<u>-8</u>		74
N4.5 E10.5	╢	55	1		/ 136			-1		0 <	LC	-0		
N4.5 E11.5	 	46		<lc< td=""><td></td><td>426</td><td></td><td></td><td></td><td>_ _</td><td>.1 .</td><td></td><td></td><td>76</td></lc<>		426				_ _	.1 .			76
N4.5 E12.5	<lc< td=""><td>9</td><td></td><td> <u> </u></td><td>572</td><td>878</td><td><lc< td=""><td>-1</td><td></td><td>0 <</td><td></td><td>4</td><td>ļ</td><td>74</td></lc<></td></lc<>	9		<u> </u>	572	878	<lc< td=""><td>-1</td><td></td><td>0 <</td><td></td><td>4</td><td>ļ</td><td>74</td></lc<>	-1		0 <		4	ļ	74
N4.5 E13.5	1175	55			259	7 670				0		-8		74
N4.5 E14.5	1/2	-9			374	8 753	<lc< td=""><td>- 2</td><td></td><td>6 <</td><td></td><td>-8</td><td><u> </u></td><td>75</td></lc<>	- 2		6 <		-8	<u> </u>	75
N4.5 E15.5	<lc< td=""><td>9</td><td></td><td></td><td>216</td><td>8 636</td><td><lc< td=""><td></td><td></td><td>6</td><td></td><td>-4</td><td></td><td>70</td></lc<></td></lc<>	9			216	8 636	<lc< td=""><td></td><td></td><td>6</td><td></td><td>-4</td><td></td><td>70</td></lc<>			6		-4		70
N4.5 E16.5	<lc< td=""><td>28</td><td></td><td></td><td>104</td><td></td><td>3 <lc< td=""><td>^</td><td>1</td><td>0 <</td><td><lc< td=""><td>-46</td><td></td><td></td></lc<></td></lc<></td></lc<>	28			104		3 <lc< td=""><td>^</td><td>1</td><td>0 <</td><td><lc< td=""><td>-46</td><td></td><td></td></lc<></td></lc<>	^	1	0 <	<lc< td=""><td>-46</td><td></td><td></td></lc<>	-46		
N4.5 E17.5	<lc< td=""><td>28</td><td></td><td></td><td>45</td><td>5 47</td><td>3</td><td></td><td></td><td>_</td><td></td><td></td><td>ļ</td><td></td></lc<>	28			45	5 47	3			_			ļ	
N4.5 E18.5	<lc< td=""><td></td><td></td><td><lc< td=""><td>34</td><td></td><td>3</td><td></td><td></td><td></td><td></td><td></td><td>ļ</td><td></td></lc<></td></lc<>			<lc< td=""><td>34</td><td></td><td>3</td><td></td><td></td><td></td><td></td><td></td><td>ļ</td><td></td></lc<>	34		3						ļ	
N4.5 E19.5	<lc< td=""><td>28</td><td></td><td><lc< td=""><td>21</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	28		<lc< td=""><td>21</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	21									
N4.5 E2.5	<lc_< td=""><td></td><td></td><td></td><td>40</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc_<>				40								<u> </u>	
N4.5 E20.5	<lc< td=""><td>- 40</td><td></td><td></td><td>18</td><td></td><td>в</td><td></td><td></td><td></td><td></td><td></td><td> </td><td></td></lc<>	- 40			18		в						 	
N4.5 E21.5	∥ <lc< td=""><td>-18</td><td></td><td></td><td>66</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>ļ</td><td></td></lc<>	-18			66								ļ	
N4.5 E3.5	4	37			58									
N4.5 E4.5	<lc< td=""><td>28</td><td></td><td></td><td>77</td><td></td><td></td><td></td><td>8</td><td>10</td><td><lc< td=""><td>-38</td><td>-</td><td>7</td></lc<></td></lc<>	28			77				8	10	<lc< td=""><td>-38</td><td>-</td><td>7</td></lc<>	-38	-	7
N4.5 E5.5	<lc< td=""><td></td><td></td><td></td><td>34</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>				34									
N4.5 E6.5	<lc< td=""><td></td><td></td><td></td><td>2</td><td></td><td></td><td>·</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>				2			·						
N4.5 E7.5	<lc< td=""><td>- !</td><td></td><td></td><td>115</td><td></td><td>8 <lc< td=""><td></td><td>2</td><td>6</td><td><lc< td=""><td>-21</td><td></td><td>7</td></lc<></td></lc<></td></lc<>	- !			115		8 <lc< td=""><td></td><td>2</td><td>6</td><td><lc< td=""><td>-21</td><td></td><td>7</td></lc<></td></lc<>		2	6	<lc< td=""><td>-21</td><td></td><td>7</td></lc<>	-21		7
N4.5 E8.5		40			123				8	10	<lc< td=""><td>46</td><td>3</td><td>8</td></lc<>	46	3	8
N4.5 E9.5		4				55 44								
N5.0 E-1.0		2				35 46								
N5.0 E-2.0	<lc< td=""><td></td><td><u> </u></td><td>7 <lc< td=""><td></td><td></td><td></td><td></td><td></td><td>1</td><td>-</td><td></td><td></td><td></td></lc<></td></lc<>		<u> </u>	7 <lc< td=""><td></td><td></td><td></td><td></td><td></td><td>1</td><td>-</td><td></td><td></td><td></td></lc<>						1	-			
N5.0 E0.0	<lc< td=""><td></td><td></td><td>3</td><td></td><td></td><td>8</td><td></td><td>_</td><td>1</td><td></td><td></td><td></td><td></td></lc<>			3			8		_	1				
N5.0 E1.0				1 <lc< td=""><td></td><td></td><td>7</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			7							
N5.0 E10.0	<lc< td=""><td></td><td></td><td>7</td><td></td><td></td><td>88</td><td></td><td>_</td><td></td><td></td><td></td><td></td><td></td></lc<>			7			88		_					
N5.0 E11.0	<lc< td=""><td></td><td></td><td></td><td></td><td></td><td>71</td><td></td><td>_</td><td></td><td></td><td></td><td></td><td></td></lc<>						71		_					
N5.0 E12.0				2			6 <lc< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td>-6</td><td>3</td><td></td></lc<></td></lc<>		-1	0	<lc< td=""><td>-6</td><td>3</td><td></td></lc<>	-6	3	
N5.0 E13.0	<lc< td=""><td></td><td></td><td>3</td><td></td><td></td><td>76</td><td></td><td>-</td><td>\neg</td><td></td><td></td><td></td><td></td></lc<>			3			76		-	\neg				
N5.0 E14.0				2			74			_			\perp	
N5.0 E15.0	<lc< td=""><td></td><td></td><td></td><td></td><td></td><td>79</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>						79							
N5.0 E16.0	<lc< td=""><td></td><td></td><td>0</td><td></td><td></td><td>57</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			0			57							
N5.0 E17.0	<lc< td=""><td></td><td></td><td>이</td><td></td><td></td><td>28 <lo< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td>-6</td><td>7</td><td></td></lc<></td></lo<></td></lc<>			이			28 <lo< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td>-6</td><td>7</td><td></td></lc<></td></lo<>		-1	0	<lc< td=""><td>-6</td><td>7</td><td></td></lc<>	-6	7	
N5.0 E18.0		3		1 < Lc					5		<lc< td=""><td>5</td><td>0</td><td></td></lc<>	5	0	
N5.0 E19.0	<lc< td=""><td></td><td></td><td>20</td><td></td><td></td><td>15</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			20			15							
N5.0 E2.0		- 3		1 <lc< td=""><td></td><td></td><td>22</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			22							
N5.0 E20.0	<lc< td=""><td></td><td>-4 2</td><td>20 <lc< td=""><td></td><td></td><td>06</td><td></td><td></td><td></td><td> </td><td></td><td></td><td></td></lc<></td></lc<>		-4 2	20 <lc< td=""><td></td><td></td><td>06</td><td></td><td></td><td></td><td> </td><td></td><td></td><td></td></lc<>			06				 			
N5.0 E20.0	<lc< td=""><td></td><td></td><td>0</td><td></td><td></td><td>34</td><td></td><td></td><td></td><td> </td><td></td><td></td><td></td></lc<>			0			34				 			
N5.0 E21.0				37			37				 			
N5.0 E22.0 N5.0 E3.0	- <lc< td=""><td></td><td></td><td>33</td><td></td><td></td><td>43</td><td></td><td></td><td></td><td>-</td><td></td><td>_</td><td></td></lc<>			33			43				-		_	
				37			65				 			
N5.0 E4.0 N5.0 E5.0				41		596 4	63				ــــــــــــــــــــــــــــــــــــــ			

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

1			DIRECT				Π-	TRANSFERABLE ALPHA/100 SQ CM BETA-GAMMA/100 SQ CM								
	A) 5) 1A /			BETA-GAMMA/100 SQ CM				LPHA	100	SQ CM	В				CM	
	ALPHA/			SME		STD		SMPL		STD		SMPL		STD	1	
OCATION/ITEM	SMPL		STD	DP'		DEV	1	DPM		DEV		DPM		DEV_		
COORDINATES	DPM		DEV ·	UF	725	47	<u> </u>									
15.0 E6.0		33	41		1866		3 <1	C	2	6	<l< td=""><td>c</td><td>0</td><td></td><td>78</td></l<>	c	0		78	
15.0 E7.0	<lc< td=""><td>-4</td><td>20</td><td></td><td></td><td></td><td>_</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-4	20				_									
15.0 E8.0	<lc< td=""><td>-4</td><td>20</td><td></td><td>518 207</td><td>41</td><td>_</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-4	20		518 207	41	_									
15.0 E9.0	<lc< td=""><td>-4</td><td></td><td><lc< td=""><td></td><td></td><td></td><td></td><td>-1</td><td>0</td><td><l< td=""><td>C</td><td>-88</td><td></td><td>68</td></l<></td></lc<></td></lc<>	-4		<lc< td=""><td></td><td></td><td></td><td></td><td>-1</td><td>0</td><td><l< td=""><td>C</td><td>-88</td><td></td><td>68</td></l<></td></lc<>					-1	0	<l< td=""><td>C</td><td>-88</td><td></td><td>68</td></l<>	C	-88		68	
N5.5 E-0.5	<lc< td=""><td>11</td><td>27</td><td></td><td>1036</td><td></td><td></td><td></td><td></td><td><u> </u></td><td>1</td><td></td><td></td><td></td><td></td></lc<>	11	27		1036					<u> </u>	1					
15.5 E-1.5	<lc< td=""><td>11</td><td>27</td><td><lc< td=""><td>155</td><td></td><td>2 <</td><td></td><td>2</td><td>6</td><td>1</td><td>C</td><td>-59</td><td></td><td>69</td></lc<></td></lc<>	11	27	<lc< td=""><td>155</td><td></td><td>2 <</td><td></td><td>2</td><td>6</td><td>1</td><td>C</td><td>-59</td><td></td><td>69</td></lc<>	155		2 <		2	6	1	C	-59		69	
N5.5 E0.5	<lc< td=""><td>-18</td><td>30</td><td></td><td>883</td><td></td><td></td><td></td><td>-1</td><td></td><td>-i</td><td></td><td>-4</td><td></td><td>75</td></lc<>	-18	30		883				-1		-i		-4		75	
V5.5 E1.5	<lc< td=""><td>-28</td><td>24</td><td></td><td>2088</td><td><u> </u></td><td></td><td>Lc</td><td>- 1</td><td> </td><td>+</td><td></td><td></td><td></td><td></td></lc<>	-28	24		2088	<u> </u>		Lc	- 1	 	+					
N5.5 E10.5	<lc< td=""><td>-9</td><td></td><td><lc< td=""><td>294</td><td>_</td><td></td><td></td><td>-1</td><td> </td><td><l< td=""><td></td><td>-13</td><td></td><td>74</td></l<></td></lc<></td></lc<>	-9		<lc< td=""><td>294</td><td>_</td><td></td><td></td><td>-1</td><td> </td><td><l< td=""><td></td><td>-13</td><td></td><td>74</td></l<></td></lc<>	294	_			-1	 	<l< td=""><td></td><td>-13</td><td></td><td>74</td></l<>		-13		74	
N5.5 E11.5	<lc< td=""><td>28</td><td>50</td><td></td><td>937</td><td></td><td>7 <</td><td></td><td></td><td> </td><td>\ -</td><td></td><td>4</td><td></td><td>76</td></lc<>	28	50		937		7 <			 	\ -		4		76	
N5.5 E12.5	<lc< td=""><td>28</td><td>50</td><td></td><td>1151</td><td></td><td>8 <</td><td>LC</td><td>-1</td><td> </td><td>-</td><td></td><td></td><td></td><td>-</td></lc<>	28	50		1151		8 <	LC	-1	 	-				-	
N5.5 E13.5	<lc< td=""><td>28</td><td>50</td><td><lc< td=""><td>-27</td><td></td><td>_</td><td></td><td></td><td>ļ</td><td>╫</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	28	50	<lc< td=""><td>-27</td><td></td><td>_</td><td></td><td></td><td>ļ</td><td>╫</td><td></td><td></td><td></td><td></td></lc<>	-27		_			ļ	╫					
N5.5 E14.5	<lc< td=""><td>18</td><td>47</td><td><lc< td=""><td>-80</td><td></td><td></td><td></td><td></td><td><u> </u></td><td>-</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	18	47	<lc< td=""><td>-80</td><td></td><td></td><td></td><td></td><td><u> </u></td><td>-</td><td></td><td></td><td></td><td></td></lc<>	-80					<u> </u>	-					
	<lc< td=""><td>9</td><td>43</td><td></td><td>455</td><td></td><td>78</td><td></td><td></td><td></td><td>╫</td><td></td><td></td><td></td><td></td></lc<>	9	43		455		78				╫					
N5.5 E15.5	<lc< td=""><td>-</td><td></td><td><lc< td=""><td>27</td><td>7 42</td><td>29</td><td></td><td></td><td>ļ</td><td>╂-</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-		<lc< td=""><td>27</td><td>7 42</td><td>29</td><td></td><td></td><td>ļ</td><td>╂-</td><td></td><td></td><td></td><td></td></lc<>	27	7 42	29			ļ	╂-					
N5.5 E16.5	<lc< td=""><td><u>-9</u></td><td></td><td><lc< td=""><td>24</td><td>1 4</td><td>54</td><td></td><td></td><td></td><td>+</td><td></td><td>24</td><td> </td><td>77</td></lc<></td></lc<>	<u>-9</u>		<lc< td=""><td>24</td><td>1 4</td><td>54</td><td></td><td></td><td></td><td>+</td><td></td><td>24</td><td> </td><td>77</td></lc<>	24	1 4	54				+		24	 	77	
N5.5 E17.5	<lc< td=""><td>-9</td><td></td><td></td><td>72</td><td></td><td>06 <</td><td>Lc</td><td>_1</td><td><u> </u></td><td>) <</td><td>Lc</td><td>21</td><td> </td><td>/ /</td></lc<>	- 9			72		06 <	Lc	_1	<u> </u>) <	Lc	21	 	/ /	
N5.5 E18.5		9		<lc< td=""><td>26</td><td></td><td>57</td><td></td><td></td><td><u> </u></td><td>1</td><td><u> </u></td><td></td><td></td><td></td></lc<>	26		57			<u> </u>	1	<u> </u>				
N5.5 E19.5	<lc< td=""><td>18</td><td></td><td></td><td>26</td><td></td><td>57</td><td></td><td></td><td></td><td>$oldsymbol{\perp}$</td><td></td><td></td><td></td><td></td></lc<>	18			26		57				$oldsymbol{\perp}$					
N5.5 E2.5	<lc< td=""><td></td><td></td><td></td><td>37</td><td>_</td><td>39</td><td></td><td></td><td>T</td><td></td><td></td><td></td><td></td><td></td></lc<>				37	_	39			T						
N5.5 E20.5	<lc< td=""><td>-9</td><td></td><td></td><td>64</td><td></td><td>98</td><td></td><td></td><td></td><td>\mathbb{L}</td><td></td><td></td><td></td><td></td></lc<>	-9			64		98				\mathbb{L}					
N5.5 E21.5	<lc< td=""><td>-9</td><td></td><td></td><td>45</td><td></td><td>78</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-9			45		78									
N5.5 E3.5	<lc< td=""><td>-9</td><td></td><td></td><td>64</td><td></td><td>98</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-9			64		98									
N5.5 E4.5	<lc< td=""><td>-9</td><td></td><td></td><td>160</td><td></td><td>89</td><td>sl c</td><td></td><td>1</td><td>0 <</td><td>Lc</td><td>4</td><td><u> </u></td><td>7</td></lc<>	-9			160		89	sl c		1	0 <	Lc	4	<u> </u>	7	
N5.5 E5.5		37					55				8 <	Lc	-13		7.	
N5.5 E6.5		37			123		89			1	1			T		
N5.5 E7.5		37			56		72				Ť					
N5.5 E8.5	<lc< td=""><td>18</td><td></td><td></td><td>40</td><td></td><td></td><td>-10</td><td></td><td>2</td><td>6 <</td><td>Lc</td><td>-46</td><td></td><td>7</td></lc<>	18			40			-10		2	6 <	Lc	-46		7	
N5.5 E9.5	<lc< td=""><td>28</td><td></td><td></td><td>80</td><td></td><td>14</td><td></td><td></td><td><u> </u></td><td>0 <</td><td></td><td>-8</td><td></td><td>7</td></lc<>	28			80		14			<u> </u>	0 <		-8		7	
N6.0 E-1.0	<lc< td=""><td>7</td><td>2 19</td><td>3</td><td>67</td><td></td><td>03</td><td><lc_< td=""><td></td><td>' </td><td>+</td><td></td><td></td><td></td><td></td></lc_<></td></lc<>	7	2 19	3	67		03	<lc_< td=""><td></td><td>' </td><td>+</td><td></td><td></td><td></td><td></td></lc_<>		' 	+					
N6.0 E-2.0		57			36		71				+			1		
N6.0 E0.0	<lc< td=""><td>(</td><td>3 2</td><td>7</td><td>57</td><td></td><td>60</td><td></td><td></td><td></td><td>6</td><td><lc< td=""><td>-59</td><td>1</td><td>7</td></lc<></td></lc<>	(3 2	7	57		60				6	<lc< td=""><td>-59</td><td>1</td><td>7</td></lc<>	-59	1	7	
N6.0 E1.0	<lc< td=""><td></td><td>6 2</td><td>7 </td><td>90</td><td></td><td>95</td><td><u><lc< u=""></lc<></u></td><td></td><td>2</td><td></td><td>·LU</td><td></td><td>' </td><td><u>-</u></td></lc<>		6 2	7	90		95	<u><lc< u=""></lc<></u>		2		·LU		' 	<u>-</u>	
N6.0 E10.0		3:		1 <lc< td=""><td></td><td>0 3</td><td>393</td><td></td><td></td><td></td><td>-</td><td></td><td></td><td>+</td><td></td></lc<>		0 3	393				-			+		
	<lc< td=""><td></td><td></td><td>oll</td><td>38</td><td></td><td>140</td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td></lc<>			oll	38		140				-					
N6.0 E11.0	<lc< td=""><td></td><td>• •</td><td>oll</td><td>72</td><td></td><td>176</td><td></td><td></td><td></td><td></td><td></td><td></td><td> </td><td></td></lc<>		• •	oll	72		176							 		
N6.0 E12.0			<u> </u>	ol	49	92 4	151				4		4	. 	7	
N6.0 E13.0	<lc< td=""><td></td><td></td><td>ol -</td><td></td><td>55</td><td>190</td><td><lc< td=""><td></td><td>2</td><td>61.</td><td><lc< td=""><td>-1:</td><td></td><td></td></lc<></td></lc<></td></lc<>			ol -		55	190	<lc< td=""><td></td><td>2</td><td>61.</td><td><lc< td=""><td>-1:</td><td></td><td></td></lc<></td></lc<>		2	61.	<lc< td=""><td>-1:</td><td></td><td></td></lc<>	-1:			
N6.0 E14.0	<lc< td=""><td></td><td></td><td>ol</td><td></td><td></td><td>465</td><td></td><td></td><td></td><td>\bot</td><td></td><td></td><td></td><td></td></lc<>			ol			465				\bot					
N6.0 E15.0	<lc< td=""><td></td><td></td><td>oll</td><td></td><td></td><td>465</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			oll			465									
N6.0 E16.0	<lc< td=""><td></td><td></td><td>7</td><td></td><td></td><td></td><td><lc< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td>-6</td><td>3 </td><td></td></lc<></td></lc<></td></lc<>			7				<lc< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td>-6</td><td>3 </td><td></td></lc<></td></lc<>		-1	0	<lc< td=""><td>-6</td><td>3 </td><td></td></lc<>	-6	3		
N6.0 E17.0	<lc< td=""><td></td><td></td><td></td><td></td><td></td><td>457</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>						457									
N6.0 E18.0	<lc< td=""><td></td><td></td><td>0</td><td></td><td></td><td>454</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			0			454									
N6.0 E19.0	<lc< td=""><td></td><td></td><td>7</td><td></td><td> 1</td><td>428</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			7		1	428									
N6.0 E2.0	<lc< td=""><td></td><td></td><td>0 <lc< td=""><td></td><td></td><td>460</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>			0 <lc< td=""><td></td><td></td><td>460</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			460									
N6.0 E20.0	<lc< td=""><td></td><td></td><td>33</td><td></td><td></td><td>460</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			33			460									
N6.0 E21.0	<lc< td=""><td></td><td></td><td>27</td><td></td><td></td><td></td><td><lc< td=""><td></td><td>-1</td><td>ol</td><td><lc< td=""><td>-2</td><td>5</td><td></td></lc<></td></lc<></td></lc<>			27				<lc< td=""><td></td><td>-1</td><td>ol</td><td><lc< td=""><td>-2</td><td>5</td><td></td></lc<></td></lc<>		-1	ol	<lc< td=""><td>-2</td><td>5</td><td></td></lc<>	-2	5		
N6.0 E22.0				11							1					
N6.0 E3.0	<lc< td=""><td>-1</td><td></td><td>10 <lc< td=""><td></td><td>04</td><td>406</td><td></td><td></td><td></td><td></td><td>· · · · · · · · · · · · · · · · · · ·</td><td></td><td></td><td></td></lc<></td></lc<>	-1		10 <lc< td=""><td></td><td>04</td><td>406</td><td></td><td></td><td></td><td></td><td>· · · · · · · · · · · · · · · · · · ·</td><td></td><td></td><td></td></lc<>		04	406					· · · · · · · · · · · · · · · · · · ·				
N6.0 E4.0		2		37		96	463	 		-+						
N6.0 E5.0	<lc< td=""><td></td><td></td><td>27</td><td></td><td>70</td><td>460</td><td></td><td></td><td>-</td><td>_</td><td><lc< td=""><td>_F</td><td>4</td><td></td></lc<></td></lc<>			27		70	460			-	_	<lc< td=""><td>_F</td><td>4</td><td></td></lc<>	_F	4		
NO.U ES.U		7		41		29		<lc< td=""><td></td><td>-1 </td><td>씍</td><td>720</td><td></td><td>-</td><td></td></lc<>		-1	씍	720		-		
N6.0 E6.0	<lc< td=""><td></td><td></td><td>33</td><td>7</td><td>25</td><td>476</td><td></td><td></td><td></td><td> </td><td></td><td></td><td>-</td><td></td></lc<>			33	7	25	476							-		
N6.0 E7.0				37		'51	479	<u></u>			_			2		
N6.0 E8.0				41 *			273			5		<lc< td=""><td></td><td>3</td><td></td></lc<>		3		
N6.0 E9.0	11			32		322		<lc< td=""><td></td><td>-1</td><td>വ</td><td><lc< td=""><td>-4</td><td>21</td><td></td></lc<></td></lc<>		-1	വ	<lc< td=""><td>-4</td><td>21</td><td></td></lc<>	-4	21		

Lc indicates less than the critical level of activity which can be said to be above background.
A negative value is the calculated result of a reading which is below the instrument-specific background.

							TRANSFERABLE								
[DIRECT			0.00		AL DL		SQ CM		BETA-GAM	TA-GAMMA/100 SQ CM		
	ALPH/				AMMA/10		CM		1PL	STD	╁	SMPL		STD	
LOCATION/ITEM	SMF		STD		MPL	STD	1		PM	DEV	1	DPM	Į	DEV	j
COORDINATES	DP	M	DEV	<u> </u>)PM		510		-1		7 <	Lc	-8		77
N6.5 E-1.5	<lc< td=""><td>2</td><td>19</td><td></td><td>751</td><td></td><td>510</td><td><u> </u></td><td>-,</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	2	19		751		510	<u> </u>	-,						
N6.5 E0.5	N/	Δ .	NA		NA	NA					+				
N6.5 E1.5	N/	Ą	NA		NA	NA		-1 -	-1	 	0 <	l c	-38		71
N6.5 E10.5	<lc< td=""><td>0</td><td>51</td><td></td><td>1040</td><td></td><td><u> </u></td><td><lc< td=""><td><u>- 1</u> -1</td><td>ļ</td><td>0 <</td><td></td><td>-17</td><td></td><td>73</td></lc<></td></lc<>	0	51		1040		<u> </u>	<lc< td=""><td><u>- 1</u> -1</td><td>ļ</td><td>0 <</td><td></td><td>-17</td><td></td><td>73</td></lc<>	<u>- 1</u> -1	ļ	0 <		-17		73
N6.5 E11.5	<lc< td=""><td>19</td><td>57</td><td></td><td>887</td><td><u> </u></td><td>596</td><td></td><td>2</td><td></td><td>6 <</td><td></td><td>17</td><td></td><td>77</td></lc<>	19	57		887	<u> </u>	596		2		6 <		17		77
N6.5 E12.5	<lc< td=""><td>-39</td><td>34</td><td></td><td>978</td><td></td><td>605</td><td><lc< td=""><td></td><td> </td><td>+</td><td></td><td></td><td>······································</td><td></td></lc<></td></lc<>	-39	34		978		605	<lc< td=""><td></td><td> </td><td>+</td><td></td><td></td><td>······································</td><td></td></lc<>		 	+			······································	
N6.5 E13.5	<lc< td=""><td>-19</td><td></td><td><lc< td=""><td>397</td><td>ļ</td><td>546</td><td></td><td></td><td> </td><td>+</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-19		<lc< td=""><td>397</td><td>ļ</td><td>546</td><td></td><td></td><td> </td><td>+</td><td></td><td></td><td></td><td></td></lc<>	397	ļ	546			 	+				
N6.5 E14.5	<lc< td=""><td>-58</td><td>21</td><td></td><td>612</td><td>}</td><td>569</td><td></td><td></td><td> </td><td>╅</td><td></td><td></td><td></td><td></td></lc<>	-58	21		612	}	569			 	╅				
N6.5 E15.5	<lc< td=""><td>-10</td><td></td><td><lc< td=""><td>336</td><td></td><td>539</td><td></td><td></td><td></td><td>╅</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-10		<lc< td=""><td>336</td><td></td><td>539</td><td></td><td></td><td></td><td>╅</td><td></td><td></td><td></td><td></td></lc<>	336		539				╅				
N6.5 E16.5	<lc< td=""><td>-29</td><td></td><td><lc< td=""><td>92</td><td></td><td>512</td><td>-1 -</td><td></td><td></td><td>6 <</td><td>1.0</td><td>-33</td><td></td><td>71</td></lc<></td></lc<>	-29		<lc< td=""><td>92</td><td></td><td>512</td><td>-1 -</td><td></td><td></td><td>6 <</td><td>1.0</td><td>-33</td><td></td><td>71</td></lc<>	92		512	-1 -			6 <	1.0	-33		71
N6.5 E17.5	<lc< td=""><td>19</td><td>57</td><td></td><td>826</td><td>_</td><td>590</td><td><lc< td=""><td></td><td><u> </u></td><td>4</td><td>·LC</td><td></td><td></td><td></td></lc<></td></lc<>	19	57		826	_	590	<lc< td=""><td></td><td><u> </u></td><td>4</td><td>·LC</td><td></td><td></td><td></td></lc<>		<u> </u>	4	·LC			
N6.5 E18.5	<lc< td=""><td>-29</td><td>39</td><td></td><td>581</td><td></td><td>565</td><td></td><td></td><td> </td><td>+</td><td></td><td></td><td></td><td></td></lc<>	-29	39		581		565			 	+				
N6.5 E19.5	<lc< td=""><td>-10</td><td>47</td><td><lc< td=""><td>397</td><td></td><td>546</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-10	47	<lc< td=""><td>397</td><td></td><td>546</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	397		546								
N6.5 E2.5	<lc< td=""><td>10</td><td>54</td><td></td><td>734</td><td>· </td><td>581</td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td><td></td><td></td></lc<>	10	54		734	·	581					<u> </u>			
N6.5 E20.5	<lc< td=""><td>-19</td><td></td><td><lc< td=""><td>336</td><td></td><td>539</td><td></td><td></td><td></td><td>╬</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-19		<lc< td=""><td>336</td><td></td><td>539</td><td></td><td></td><td></td><td>╬</td><td></td><td></td><td></td><td></td></lc<>	336		539				╬				
N6.5 E20.5 N6.5 E21.5	<lc< td=""><td>-39</td><td></td><td><lc< td=""><td>275</td><td>5</td><td>533</td><td></td><td></td><td> </td><td>-</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-39		<lc< td=""><td>275</td><td>5</td><td>533</td><td></td><td></td><td> </td><td>-</td><td></td><td></td><td></td><td></td></lc<>	275	5	533			 	-				
N6.5 E21.5 N6.5 E3.5	/LC	-48			612		569			-					
	<lc< td=""><td>- '</td><td></td><td></td><td>306</td><td>3</td><td>536</td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td></lc<>	- '			306	3	536				-				
N6.5 E4.5	<lc< td=""><td>29</td><td></td><td></td><td>703</td><td>3</td><td>578</td><td></td><td></td><td></td><td></td><td></td><td>25</td><td></td><td>78</td></lc<>	29			703	3	578						25		78
N6.5 E5.5	<lc< td=""><td>-19</td><td></td><td></td><td>198</td><td>7</td><td>696</td><td><lc< td=""><td></td><td>2</td><td>6</td><td><lc< td=""><td>25</td><td></td><td>- 10</td></lc<></td></lc<></td></lc<>	-19			198	7	696	<lc< td=""><td></td><td>2</td><td>6</td><td><lc< td=""><td>25</td><td></td><td>- 10</td></lc<></td></lc<>		2	6	<lc< td=""><td>25</td><td></td><td>- 10</td></lc<>	25		- 10
N6.5 E6.5	<lc< td=""><td>-19</td><td></td><td><lc< td=""><td>24</td><td>5</td><td>529</td><td></td><td></td><td></td><td>_</td><td></td><td></td><td><u> </u></td><td></td></lc<></td></lc<>	-19		<lc< td=""><td>24</td><td>5</td><td>529</td><td></td><td></td><td></td><td>_</td><td></td><td></td><td><u> </u></td><td></td></lc<>	24	5	529				_			<u> </u>	
N6.5 E7.5	<lc< td=""><td>10</td><td><u> </u></td><td></td><td>61:</td><td>2</td><td>569</td><td></td><td></td><td></td><td>_</td><td></td><td></td><td>ļ</td><td>73</td></lc<>	10	<u> </u>		61:	2	569				_			ļ	73
N6.5 E8.5	<lc< td=""><td>19</td><td></td><td></td><td>125</td><td>4</td><td>631</td><td><lc< td=""><td></td><td>2</td><td>6</td><td><lc< td=""><td>-21</td><td> </td><td>. 73</td></lc<></td></lc<></td></lc<>	19			125	4	631	<lc< td=""><td></td><td>2</td><td>6</td><td><lc< td=""><td>-21</td><td> </td><td>. 73</td></lc<></td></lc<>		2	6	<lc< td=""><td>-21</td><td> </td><td>. 73</td></lc<>	-21	 	. 73
N6.5 E9.5				/ <lc< td=""><td>7</td><td>8</td><td>440</td><td></td><td></td><td></td><td>4</td><td></td><td></td><td></td><td></td></lc<>	7	8	440				4				
N7.0 E-1.0	<lc< td=""><td>76</td><td></td><td><lc< td=""><td>7</td><td></td><td>440</td><td></td><td></td><td></td><td>_</td><td></td><td></td><td> </td><td></td></lc<></td></lc<>	76		<lc< td=""><td>7</td><td></td><td>440</td><td></td><td></td><td></td><td>_</td><td></td><td></td><td> </td><td></td></lc<>	7		440				_			 	
N7.0 E-2.0		VA (NA NA	1	NA	NA					_				
N7.0 E1.0		-1!		3 <lc< td=""><td>30</td><td>6</td><td>536</td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<>	30	6	536							<u> </u>	
N7.0 E10.0	<lc< td=""><td>-1: -1:</td><td></td><td>7 <lc< td=""><td>21</td><td></td><td>526</td><td></td><td></td><td></td><td></td><td></td><td></td><td>ļ</td><td></td></lc<></td></lc<>	-1: -1:		7 <lc< td=""><td>21</td><td></td><td>526</td><td></td><td></td><td></td><td></td><td></td><td></td><td>ļ</td><td></td></lc<>	21		526							ļ	
N7.0 E11.0	<lc< td=""><td>-1</td><td></td><td></td><td>52</td><td></td><td>559</td><td></td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc<>	-1			52		559							1	
N7.0 E12.0	<lc< td=""><td></td><td></td><td></td><td>48</td><td></td><td>556</td><td></td><td></td><td></td><td></td><td></td><td></td><td>ļ</td><td></td></lc<>				48		556							ļ	
N7.0 E13.0	<lc_< td=""><td>-4</td><td></td><td>1</td><td>79</td><td></td><td></td><td><lc< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td>-8</td><td><u> </u></td><td>74</td></lc<></td></lc<></td></lc_<>	-4		1	79			<lc< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td>-8</td><td><u> </u></td><td>74</td></lc<></td></lc<>		-1	0	<lc< td=""><td>-8</td><td><u> </u></td><td>74</td></lc<>	-8	<u> </u>	74
N7.0 E14.0	<lc< td=""><td></td><td><u> </u></td><td></td><td>55</td><td></td><td>562</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		<u> </u>		55		562								
N7.0 E15.0	<lc< td=""><td>1</td><td></td><td></td><td>12</td><td></td><td>516</td><td>_</td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<>	1			12		516	_						<u> </u>	
N7.0 E16.0	<lc< td=""><td>-4</td><td></td><td>8 <lc< td=""><td>70</td><td></td><td>578</td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<></td></lc<>	-4		8 <lc< td=""><td>70</td><td></td><td>578</td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<>	70		578							<u> </u>	
N7.0 E17.0	<lc_< td=""><td>-1</td><td></td><td></td><td>55</td><td></td><td>562</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc_<>	-1			55		562								
N7.0 E18.0	<lc< td=""><td>-1</td><td></td><td></td><td></td><td></td><td>553</td><td></td><td></td><td>_</td><td></td><td></td><td></td><td></td><td></td></lc<>	-1					553			_					
N7.0 E19.0	<lc< td=""><td>-2</td><td></td><td>9</td><td></td><td>9 NA</td><td></td><td>1</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-2		9		9 NA		1							
N7.0 E2.0		NA	NA 1	 	NA 36		54:	3							
N7.0 E20.0	<lc< td=""><td></td><td></td><td>3 <lc< td=""><td></td><td>97</td><td>54</td><td>_</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>			3 <lc< td=""><td></td><td>97</td><td>54</td><td>_</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		97	54	_							
N7.0 E21.0	<lc< td=""><td></td><td></td><td>4 <lc< td=""><td>100</td><td></td><td></td><td>3 <lc< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td>-2</td><td>1</td><td>7:</td></lc<></td></lc<></td></lc<></td></lc<>			4 <lc< td=""><td>100</td><td></td><td></td><td>3 <lc< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td>-2</td><td>1</td><td>7:</td></lc<></td></lc<></td></lc<>	100			3 <lc< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td>-2</td><td>1</td><td>7:</td></lc<></td></lc<>		-1	0	<lc< td=""><td>-2</td><td>1</td><td>7:</td></lc<>	-2	1	7:
N7.0 E22.0	<lc< td=""><td></td><td></td><td>8</td><td></td><td>NA NA</td><td></td><td>31 3</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			8		NA NA		31 3							
N7.0 E3.0		NA	NA .		NA A		54	al -		_					
N7.0 E4.0	<lc< td=""><td></td><td></td><td>4</td><td></td><td>28</td><td>56 56</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			4		28	56 56								
N7.0 E5.0		4		6		12	75			5	8	<lc< td=""><td>1</td><td>3</td><td>7</td></lc<>	1	3	7
N7.0 E6.0	<lc< td=""><td></td><td></td><td>4</td><td>27</td><td></td><td>60</td><td></td><td></td><td>5</td><td></td><td><lc td="" ·<=""><td>4</td><td>2</td><td>8</td></lc></td></lc<>			4	27		60			5		<lc td="" ·<=""><td>4</td><td>2</td><td>8</td></lc>	4	2	8
N7.0 E7.0	<lc< td=""><td></td><td></td><td>51</td><td></td><td>48</td><td></td><td></td><td></td><td>5</td><td></td><td><lc< td=""><td>4</td><td>6</td><td>8</td></lc<></td></lc<>			51		48				5		<lc< td=""><td>4</td><td>6</td><td>8</td></lc<>	4	6	8
N7.0 E8.0				74		95	95			2		<lc< td=""><td>-2</td><td></td><td>7</td></lc<>	-2		7
N7.0 E9.0	<lc< td=""><td></td><td></td><td>39</td><td></td><td>05</td><td></td><td>0 <lc< td=""><td></td><td>-1</td><td></td><td><lc< td=""><td>-5</td><td></td><td>7</td></lc<></td></lc<></td></lc<>			39		05		0 <lc< td=""><td></td><td>-1</td><td></td><td><lc< td=""><td>-5</td><td></td><td>7</td></lc<></td></lc<>		-1		<lc< td=""><td>-5</td><td></td><td>7</td></lc<>	-5		7
N7.5 E-0.5				18		51		0 <l0< td=""><td><u></u></td><td>- - </td><td></td><td> </td><td></td><td></td><td></td></l0<>	<u></u>	- - 		 			
N7.5 E-1.5	-1		48 4	15 <lc< td=""><td></td><td>85</td><td>46</td><td></td><td></td><td>_</td><td></td><td>+</td><td></td><td></td><td></td></lc<>		85	46			_		+			
N7.5 E0.5	<lc< td=""><td></td><td></td><td>50 <lc< td=""><td></td><td>41</td><td>45</td><td></td><td></td><td>8</td><td>10</td><td><lc< td=""><td>_6</td><td>8</td><td>6</td></lc<></td></lc<></td></lc<>			50 <lc< td=""><td></td><td>41</td><td>45</td><td></td><td></td><td>8</td><td>10</td><td><lc< td=""><td>_6</td><td>8</td><td>6</td></lc<></td></lc<>		41	45			8	10	<lc< td=""><td>_6</td><td>8</td><td>6</td></lc<>	_6	8	6
N7.5 E1.5	<lc< td=""><td></td><td></td><td>35</td><td>7</td><td>23</td><td>50</td><td></td><td></td><td></td><td>10</td><td>1 -20</td><td></td><td>+</td><td></td></lc<>			35	7	23	50				10	1 -20		+	
N7.5 E10.5	<lc< td=""><td></td><td></td><td>24 <lc< td=""><td></td><td>0</td><td>42</td><td></td><td></td><td></td><td></td><td> </td><td></td><td></td><td></td></lc<></td></lc<>			24 <lc< td=""><td></td><td>0</td><td>42</td><td></td><td></td><td></td><td></td><td> </td><td></td><td></td><td></td></lc<>		0	42					 			
N7.5 E10.5	√LC <lc< td=""><td></td><td></td><td>43</td><td>ϵ</td><td>42</td><td></td><td>8</td><td></td><td></td><td></td><td> </td><td></td><td></td><td></td></lc<>			43	ϵ	42		8				 			
	11			43		55	4-	78		1		II.			

Lc indicates less than the critical level of activity which can be said to be above background.
A negative value is the calculated result of a reading which is below the instrument-specific background.

								TRANSFERABLE								
ļ			DIRECT				-	ALPHA/			BE	TA-GAMI	MA/10	0 SQ C	M	
	ALPH	A/100 S	SQ CM	BET/	A-GAMMA/10	00 SQ C	MI	SMPL		STD		SMPL		STD		
OCATION/ITEM	SMI	PL	STD		SMPL	STD	Ä	DPM		DEV	1	DPM		DEV		
COORDINATES	DP	M]	DEV		DPM	DEV		UPW		DLV	-					
N7.5 E13.5	<lc< td=""><td>-18</td><td></td><td><lc< td=""><td>187</td><td>44</td><td></td><td><u> </u></td><td>2</td><td>6</td><td><l0< td=""><td>·</td><td>0</td><td></td><td>75</td></l0<></td></lc<></td></lc<>	-18		<lc< td=""><td>187</td><td>44</td><td></td><td><u> </u></td><td>2</td><td>6</td><td><l0< td=""><td>·</td><td>0</td><td></td><td>75</td></l0<></td></lc<>	187	44		<u> </u>	2	6	<l0< td=""><td>·</td><td>0</td><td></td><td>75</td></l0<>	·	0		75	
N7.5 E14.5	<lc< td=""><td>-9</td><td>35</td><td></td><td>1017</td><td>1</td><td>35</td><td><lc .<="" td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc></td></lc<>	-9	35		1017	1	35	<lc .<="" td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc>								
V7.5 E15.5	<lc< td=""><td>-18</td><td>30</td><td></td><td>696</td><td>1</td><td>03</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-18	30		696	1	03									
V7.5 E16.5	<lc< td=""><td>0</td><td>40</td><td></td><td>509</td><td></td><td>84</td><td></td><td></td><td></td><td>╫-</td><td></td><td></td><td></td><td></td></lc<>	0	40		509		84				╫-					
N7.5 E17.5	<lc< td=""><td>9</td><td>43</td><td></td><td>616</td><td>1</td><td>95</td><td></td><td></td><td></td><td>╂</td><td></td><td>-</td><td></td><td></td></lc<>	9	43		616	1	95				╂		-			
N7.5 E18.5	<lc< td=""><td>-9</td><td>35</td><td><lc< td=""><td></td><td></td><td>45</td><td></td><td></td><td></td><td>╂</td><td>:</td><td></td><td></td><td></td></lc<></td></lc<>	-9	35	<lc< td=""><td></td><td></td><td>45</td><td></td><td></td><td></td><td>╂</td><td>:</td><td></td><td></td><td></td></lc<>			45				╂	:				
N7.5 E19.5	<lc< td=""><td>-28</td><td>24</td><td></td><td>455</td><td></td><td>78</td><td></td><td></td><td><u> </u></td><td>1-</td><td></td><td></td><td></td><td></td></lc<>	-28	24		455		78			<u> </u>	1-					
N7.5 E2.5	<lc< td=""><td>-18</td><td>30</td><td></td><td>616</td><td></td><td>95</td><td></td><td></td><td></td><td>╁</td><td></td><td></td><td></td><td></td></lc<>	-18	30		616		95				╁					
N7.5 E2.5 N7.5 E20.5	<lc< td=""><td>9</td><td>43</td><td><lc< td=""><td></td><td></td><td>54</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	9	43	<lc< td=""><td></td><td></td><td>54</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td><td></td></lc<>			54				1					
N7.5 E20.5	<lc< td=""><td>0</td><td>40</td><td></td><td>482</td><td></td><td>81</td><td></td><td></td><td>ļ</td><td></td><td></td><td>0</td><td></td><td>75</td></lc<>	0	40		482		81			ļ			0		75	
N7.5 E3.5	<lc< td=""><td>-9</td><td>35</td><td></td><td>803</td><td></td><td></td><td><lc< td=""><td>2</td><td></td><td>1</td><td><u> </u></td><td></td><td></td><td></td></lc<></td></lc<>	-9	35		803			<lc< td=""><td>2</td><td></td><td>1</td><td><u> </u></td><td></td><td></td><td></td></lc<>	2		1	<u> </u>				
N7.5 E4.5	1	55	59		1419		72			ļ	+-					
N7.5 E5.5	#	55			669		01) <l< td=""><td>^</td><td>-4</td><td></td><td>75</td></l<>	^	-4		75	
N7.5 E6.5	#	258			857			<lc< td=""><td>-1</td><td></td><td>) <l< td=""><td></td><td>-33</td><td></td><td>7</td></l<></td></lc<>	-1) <l< td=""><td></td><td>-33</td><td></td><td>7</td></l<>		-33		7	
N7.5 E6.5 N7.5 E7.5	<lc< td=""><td>9</td><td></td><td></td><td>4819</td><td></td><td></td><td><lc< td=""><td>2</td><td>`\'</td><td>4</td><td></td><td>- 33</td><td></td><td></td></lc<></td></lc<>	9			4819			<lc< td=""><td>2</td><td>`\'</td><td>4</td><td></td><td>- 33</td><td></td><td></td></lc<>	2	`\ '	4		- 33			
N7.5 E8.5	<lc< td=""><td>-18</td><td></td><td>_</td><td>176</td><td></td><td>303</td><td></td><td></td><td>, </td><td>1 -1</td><td></td><td>-71</td><td></td><td>6</td></lc<>	-18		_	176		303			, 	1 -1		-71		6	
	/LC	0			136			<lc< td=""><td></td><td>-</td><td></td><td></td><td>-33</td><td></td><td>7.</td></lc<>		-			-33		7.	
N7.5 E9.5	<lc< td=""><td>11</td><td></td><td></td><td>108</td><td></td><td></td><td><lc< td=""><td></td><td>2</td><td>3 < L</td><td>_U</td><td>-55</td><td></td><td></td></lc<></td></lc<>	11			108			<lc< td=""><td></td><td>2</td><td>3 < L</td><td>_U</td><td>-55</td><td></td><td></td></lc<>		2	3 < L	_U	-55			
N8.0 E-1.0	11-1-6	39		<l< td=""><td>c</td><td></td><td>131</td><td></td><td></td><td></td><td>+</td><td></td><td></td><td></td><td></td></l<>	c		131				+					
N8.0 E-2.0	<lc< td=""><td>-39</td><td></td><td> <l< td=""><td></td><td></td><td>519</td><td></td><td></td><td></td><td>lacksquare</td><td></td><td></td><td></td><td></td></l<></td></lc<>	-39		<l< td=""><td></td><td></td><td>519</td><td></td><td></td><td></td><td>lacksquare</td><td></td><td></td><td></td><td></td></l<>			519				lacksquare					
N8.0 E1.0	<lc< td=""><td>-48</td><td></td><td></td><td>64</td><td>2 :</td><td>572</td><td></td><td></td><td></td><td>-</td><td></td><td>. 25</td><td><u> </u></td><td>7</td></lc<>	-48			64	2 :	572				-		. 25	<u> </u>	7	
N8.0 E10.0	<lc< td=""><td>-19</td><td></td><td></td><td>94</td><td></td><td>602</td><td></td><td></td><td></td><td>0 <1</td><td></td><td>-38</td><td>-</td><td>—'7</td></lc<>	-19			94		602				0 <1		-38	-	— ' 7	
N8.0 E11.0	- -C	19		7	137	6	643	<lc< td=""><td></td><td>`</td><td>0 <</td><td></td><td>-<u>-50</u> -4</td><td> </td><td>7</td></lc<>		`	0 <		- <u>-50</u> -4	 	7	
N8.0 E12.0	<lc< td=""><td>10</td><td></td><td></td><td>91</td><td>7</td><td>599</td><td><lc< td=""><td>-</td><td>1</td><td>0 <</td><td>_C</td><td>-4</td><td></td><td></td></lc<></td></lc<>	10			91	7	599	<lc< td=""><td>-</td><td>1</td><td>0 <</td><td>_C</td><td>-4</td><td></td><td></td></lc<>	-	1	0 <	_C	-4			
N8.0 E13.0	<lc< td=""><td>-48</td><td></td><td></td><td>58</td><td>1</td><td>565</td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td></lc<>	-48			58	1	565				-					
N8.0 E14.0	<lc< td=""><td>-19</td><td></td><td>3 < L</td><td>.c 36</td><td></td><td>543</td><td></td><td></td><td></td><td>\bot</td><td></td><td></td><td></td><td></td></lc<>	-19		3 < L	.c 36		543				\bot					
N8.0 E15.0	<lc< td=""><td>-10</td><td></td><td></td><td>45</td><td>9</td><td>553</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-10			45	9	553									
N8.0 E16.0	<lc< td=""><td>2</td><td></td><td></td><td>64</td><td>2</td><td>572</td><td></td><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td></lc<>	2			64	2	572							-		
N8.0 E17.0	<lc< td=""><td></td><td>~ <u></u></td><td>1 <</td><td>c 27</td><td>75</td><td>533</td><td></td><td></td><td></td><td>_#_</td><td></td><td></td><td></td><td></td></lc<>		~ <u></u>	1 <	c 27	75	533				_#_					
N8.0 E18.0	- <lc< td=""><td>-3</td><td><u> </u></td><td>4</td><td>73</td><td>34</td><td>581</td><td><u> </u></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-3	<u> </u>	4	73	34	581	<u> </u>								
N8.0 E19.0	<lc< td=""><td>-2</td><td><u> </u></td><td>9 <</td><td>_c 12</td><td>22</td><td>516</td><td></td><td></td><td></td><td>_</td><td></td><td></td><td>┼</td><td></td></lc<>	-2	<u> </u>	9 <	_c 12	22	516				_			┼		
N8.0 E2.0	<lc< td=""><td>-<u>-2</u> -3</td><td></td><td>4</td><td>55</td><td>50</td><td>562</td><td></td><td></td><td></td><td></td><td></td><td></td><td> </td><td></td></lc<>	- <u>-2</u> -3		4	55	50	562							 		
N8.0 E20.0	<lc< td=""><td></td><td></td><td>1</td><td>55</td><td>50</td><td>562</td><td>?</td><td></td><td></td><td>_#</td><td></td><td></td><td>+</td><td></td></lc<>			1	55	50	562	?			_#			+		
N8.0 E21.0	<lc< td=""><td>-5</td><td><u> </u></td><td>1 <1</td><td>_c 39</td><td>97</td><td>546</td><td>5</td><td></td><td></td><td>_#</td><td></td><td></td><td></td><td></td></lc<>	-5	<u> </u>	1 <1	_c 39	97	546	5			_#					
N8.0 E22.0	- \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	NA -S	NA -	-	NA	NA					_			+		
N8.0 E3.0	-11-		9 5	7 2	c 3:	36	539)			_#_			 		
N8.0 E4.0	<lc< td=""><td></td><td></td><td>3</td><td>7</td><td>34</td><td>581</td><td></td><td></td><td></td><td>_</td><td></td><td>17</td><td>, </td><td></td></lc<>			3	7	34	581				_		17	, 		
N8.0 E5.0	<lc< td=""><td></td><td></td><td>7</td><td>15</td><td>90</td><td>662</td><td>2 <lc< td=""><td></td><td>2</td><td>6</td><td></td><td></td><td></td><td></td></lc<></td></lc<>			7	15	90	662	2 <lc< td=""><td></td><td>2</td><td>6</td><td></td><td></td><td></td><td></td></lc<>		2	6					
N8.0 E6.0	<lc< td=""><td></td><td></td><td>6</td><td>★ 585</td><td></td><td>2670</td><td></td><td></td><td></td><td>11 <</td><td></td><td>-2</td><td></td><td></td></lc<>			6	★ 585		2670				11 <		-2			
N8.0 E7.0				7		01	61	7 <lc< td=""><td></td><td>2</td><td>6</td><td><<u>LC</u></td><td></td><td></td><td></td></lc<>		2	6	< <u>LC</u>				
N8.0 E8.0	<lc< td=""><td></td><td></td><td>17</td><td></td><td>89</td><td>556</td><td>3</td><td></td><td></td><td>_#</td><td></td><td></td><td></td><td></td></lc<>			17		89	556	3			_#					
N8.0 E9.0	<lc< td=""><td></td><td></td><td>19</td><td></td><td>74</td><td>50</td><td>3</td><td></td><td>5</td><td>8 </td><td><lc< td=""><td>-6</td><td>3</td><td></td></lc<></td></lc<>			19		74	50	3		5	8	<lc< td=""><td>-6</td><td>3</td><td></td></lc<>	-6	3		
N8.5 E-0.5	<lc< td=""><td></td><td></td><td>41</td><td></td><td>66</td><td>48</td><td>2</td><td></td><td></td><td>_#</td><td></td><td></td><td></td><td></td></lc<>			41		66	48	2			_#					
N8.5 E-1.5				43 <		94	46	0			_					
N8.5 E0.5	<lc< td=""><td></td><td></td><td>30</td><td></td><td>42</td><td>49</td><td>8</td><td></td><td></td><td></td><td><u></u></td><td></td><td></td><td></td></lc<>			30		42	49	8				<u></u>				
N8.5 E1.5	<lc< td=""><td></td><td></td><td>43</td><td></td><td>02</td><td>47</td><td></td><td></td><td></td><td></td><td></td><td></td><td>. </td><td></td></lc<>			43		02	47							. 		
N8.5 E10.5	<lc< td=""><td></td><td></td><td>35</td><td></td><td>357</td><td></td><td>9 <lc< td=""><td></td><td>2</td><td></td><td><lc< td=""><td></td><td>8</td><td></td></lc<></td></lc<></td></lc<>			35		357		9 <lc< td=""><td></td><td>2</td><td></td><td><lc< td=""><td></td><td>8</td><td></td></lc<></td></lc<>		2		<lc< td=""><td></td><td>8</td><td></td></lc<>		8		
N8.5 E11.5	<lc< td=""><td></td><td></td><td>40</td><td></td><td>303</td><td></td><td>4 <lc< td=""><td></td><td>2</td><td></td><td><lc< td=""><td>-1</td><td></td><td></td></lc<></td></lc<></td></lc<>			40		303		4 <lc< td=""><td></td><td>2</td><td></td><td><lc< td=""><td>-1</td><td></td><td></td></lc<></td></lc<>		2		<lc< td=""><td>-1</td><td></td><td></td></lc<>	-1			
N8.5 E12.5	<lc< td=""><td></td><td></td><td></td><td></td><td>723</td><td>50</td><td></td><td></td><td>5</td><td>8</td><td><lc< td=""><td></td><td>4</td><td></td></lc<></td></lc<>					723	50			5	8	<lc< td=""><td></td><td>4</td><td></td></lc<>		4		
N8.5 E13.5	<lc< td=""><td></td><td>18</td><td>30</td><td></td><td>155</td><td>47</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		18	30		155	47									
N8.5 E14.5	<lc< td=""><td></td><td>18</td><td>30</td><td></td><td>214</td><td>45</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		18	30		214	45									
N8.5 E15.5	<lc< td=""><td></td><td></td><td>40</td><td></td><td>402</td><td>47</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			40		402	47									
N8.5 E16.5	<lc< td=""><td></td><td>0</td><td>40</td><td></td><td>750</td><td></td><td>9 <lc< td=""><td></td><td>2</td><td></td><td><lc< td=""><td></td><td>7</td><td></td></lc<></td></lc<></td></lc<>		0	40		750		9 <lc< td=""><td></td><td>2</td><td></td><td><lc< td=""><td></td><td>7</td><td></td></lc<></td></lc<>		2		<lc< td=""><td></td><td>7</td><td></td></lc<>		7		
N8.5 E17.5	<lc< td=""><td>:</td><td>9</td><td>43</td><td></td><td>883</td><td></td><td>2 <lc< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td>1</td><td>7</td><td></td></lc<></td></lc<></td></lc<>	:	9	43		883		2 <lc< td=""><td></td><td>-1</td><td>0</td><td><lc< td=""><td>1</td><td>7</td><td></td></lc<></td></lc<>		-1	0	<lc< td=""><td>1</td><td>7</td><td></td></lc<>	1	7		
N8.5 E18.5	<lc< td=""><td>;</td><td>0</td><td>40</td><td>vity which car</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	;	0	40	vity which car											

Lc indicates less than the critical level of activity which can be said to be above background.
A negative value is the calculated result of a reading which is below the instrument-specific background.

							TRANSFERABLE								
			RECT		041414446	0.0	OCM	ALPHA				BETA-GA	MMA/1	V100 SQ CM	
		V100 SC			GAMMA/10	STI		SMF		STD		SMF		STD	
OCATION/ITEM	SMF		TD		SMPL	DE	N N	DP		DEV		DP	M	DEV	
COORDINATES	DPI	``	EV		DPM 204	PE	389	<u> </u>	-						
N8.5 E19.5	<lc< td=""><td>-18</td><td>30</td><td></td><td>-294</td><td>-</td><td>460</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-18	30		-294	-	460								
N8.5 E2.5	<lc< td=""><td>18</td><td>47</td><td></td><td>294</td><td>-</td><td>445</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	18	47		294	-	445								
N8.5 E20.5	<lc< td=""><td>-28</td><td>24</td><td></td><td>161</td><td>├</td><td>451</td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td></lc<>	-28	24		161	├	451			-					
N8.5 E21.5	<lc< td=""><td>9</td><td></td><td><lc< td=""><td>214</td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	9		<lc< td=""><td>214</td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td></lc<>	214					-					
N8.5 E3.5	<lc< td=""><td>9</td><td>43</td><td></td><td>375</td><td>_</td><td>469 442</td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td></lc<>	9	43		375	_	469 442			-					
N8.5 E4.5	<lc< td=""><td>18</td><td></td><td><lc< td=""><td>134</td><td> </td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	18		<lc< td=""><td>134</td><td> </td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	134	 									
N8.5 E5.5	<lc< td=""><td>-18</td><td></td><td><lc< td=""><td>187</td><td>┼</td><td>448</td><td></td><td>5</td><td>╁──</td><td>8 -</td><td>sl_c</td><td>59</td><td></td><td>81</td></lc<></td></lc<>	-18		<lc< td=""><td>187</td><td>┼</td><td>448</td><td></td><td>5</td><td>╁──</td><td>8 -</td><td>sl_c</td><td>59</td><td></td><td>81</td></lc<>	187	┼	448		5	╁──	8 -	sl_c	59		81
N8.5 E6.5		64	62		6130		901			 					
N8.5 E7.5	<lc< td=""><td>9</td><td>43</td><td></td><td>509</td><td>_</td><td>484</td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td></lc<>	9	43		509	_	484			-					
N8.5 E8.5	<lc< td=""><td>18</td><td></td><td><lc< td=""><td>294</td><td>_</td><td>460</td><td></td><td></td><td>┼─</td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	18		<lc< td=""><td>294</td><td>_</td><td>460</td><td></td><td></td><td>┼─</td><td></td><td></td><td></td><td></td><td></td></lc<>	294	_	460			┼─					
N8.5 E9.5	<lc< td=""><td>18</td><td>47</td><td><u></u></td><td>616</td><td></td><td>495</td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td></lc<>	18	47	<u></u>	616		495			-					
N9.0 E-1.0	<lc< td=""><td>11</td><td>27</td><td><lc< td=""><td>259</td><td>_</td><td>460</td><td></td><td></td><td>┼</td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	11	27	<lc< td=""><td>259</td><td>_</td><td>460</td><td></td><td></td><td>┼</td><td></td><td></td><td></td><td></td><td></td></lc<>	259	_	460			┼					
N9.0 E-2.0	1	20	32	<lc< td=""><td>130</td><td></td><td>446</td><td></td><td></td><td>┼</td><td></td><td></td><td></td><td></td><td></td></lc<>	130		446			┼					
N9.0 E0.0	<lc< td=""><td>-13</td><td>10</td><td></td><td>725</td><td></td><td>476</td><td>-1 -</td><td></td><td>+</td><td></td><td><lc< td=""><td>-17</td><td></td><td>76</td></lc<></td></lc<>	-13	10		725		476	-1 -		+		<lc< td=""><td>-17</td><td></td><td>76</td></lc<>	-17		76
N9.0 E1.0	<lc< td=""><td>15</td><td>33</td><td></td><td>829</td><td>_</td><td>487</td><td><lc< td=""><td></td><td>4-</td><td>- 4</td><td></td><td></td><td>1</td><td></td></lc<></td></lc<>	15	33		829	_	487	<lc< td=""><td></td><td>4-</td><td>- 4</td><td></td><td></td><td>1</td><td></td></lc<>		4-	- 4			1	
N9.0 E10.0	 	24		<lc< td=""><td>18</td><td>_</td><td>416</td><td></td><td></td><td>+</td><td></td><td></td><td></td><td>1</td><td></td></lc<>	18	_	416			+				1	
N9.0 E10.0	<lc< td=""><td>6</td><td>27</td><td></td><td>75</td><td></td><td>479</td><td></td><td></td><td>+</td><td></td><td><lc< td=""><td>-67</td><td>-</td><td>71</td></lc<></td></lc<>	6	27		75		479			+		<lc< td=""><td>-67</td><td>-</td><td>71</td></lc<>	-67	-	71
N9.0 E12.0	<lc< td=""><td>15</td><td>33</td><td></td><td>85</td><td></td><td>490</td><td><lc< td=""><td></td><td>≟ </td><td>- 0</td><td><u> </u></td><td><u> </u></td><td>1</td><td></td></lc<></td></lc<>	15	33		85		490	<lc< td=""><td></td><td>≟ </td><td>- 0</td><td><u> </u></td><td><u> </u></td><td>1</td><td></td></lc<>		≟	- 0	<u> </u>	<u> </u>	1	
N9.0 E12.0	+	42	45		33	7	434							1	
N9.0 E13.0 N9.0 E14.0	<lc< td=""><td>-4</td><td>20</td><td></td><td>64</td><td>_</td><td>468</td><td></td><td></td><td>+-</td><td></td><td></td><td></td><td> -</td><td></td></lc<>	-4	20		64	_	468			+-				 -	
N9.0 E14.0	- - -	24	37		36	3	437							-	
	<lc< td=""><td>-4</td><td>20</td><td><lc< td=""><td>-5</td><td>2</td><td>387</td><td></td><td></td><td></td><td></td><td></td><td></td><td> </td><td></td></lc<></td></lc<>	-4	20	<lc< td=""><td>-5</td><td>2</td><td>387</td><td></td><td></td><td></td><td></td><td></td><td></td><td> </td><td></td></lc<>	-5	2	387							 	
N9.0 E16.0	<lc< td=""><td>-13</td><td>10</td><td></td><td>51</td><td>8</td><td>454</td><td></td><td></td><td></td><td></td><td></td><td></td><td>+</td><td></td></lc<>	-13	10		51	8	454							+	
N9.0 E17.0	<lc< td=""><td>-4</td><td>20</td><td><lc< td=""><td>31</td><td>1</td><td>431</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-4	20	<lc< td=""><td>31</td><td>1</td><td>431</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	31	1	431								
N9.0 E18.0	<lc< td=""><td>6</td><td></td><td><lc< td=""><td></td><td>5</td><td>428</td><td></td><td></td><td></td><td></td><td></td><td>-5</td><td><u>- </u></td><td>7</td></lc<></td></lc<>	6		<lc< td=""><td></td><td>5</td><td>428</td><td></td><td></td><td></td><td></td><td></td><td>-5</td><td><u>- </u></td><td>7</td></lc<>		5	428						-5	<u>- </u>	7
N9.0 E19.0	<lc< td=""><td>6</td><td>27</td><td></td><td>98</td><td>5</td><td>503</td><td><lc< td=""><td></td><td>2 </td><td>6</td><td><lc< td=""><td></td><td>-</td><td></td></lc<></td></lc<></td></lc<>	6	27		98	5	503	<lc< td=""><td></td><td>2 </td><td>6</td><td><lc< td=""><td></td><td>-</td><td></td></lc<></td></lc<>		2	6	<lc< td=""><td></td><td>-</td><td></td></lc<>		-	
N9.0 E2.0	<lc< td=""><td>-4</td><td></td><td>/<lo< td=""><td>7</td><td>8</td><td>403</td><td></td><td></td><td></td><td></td><td></td><td></td><td>- </td><td></td></lo<></td></lc<>	-4		/ <lo< td=""><td>7</td><td>8</td><td>403</td><td></td><td></td><td></td><td></td><td></td><td></td><td>- </td><td></td></lo<>	7	8	403							- 	
N9.0 E20.0		6		/ <l0< td=""><td></td><td>)4</td><td>406</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l0<>)4	406								
N9.0 E21.0	<lc< td=""><td>-4</td><td></td><td>) < Lc</td><td></td><td>11</td><td>431</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-4) < Lc		11	431								
N9.0 E22.0	<lc< td=""><td>33</td><td></td><td> <lc< td=""><td></td><td>55</td><td>413</td><td></td><td>٠.</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	33		<lc< td=""><td></td><td>55</td><td>413</td><td></td><td>٠.</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>		55	413		٠.						
N9.0 E3.0	-	6	2		4	15	443								
N9.0 E4.0	<lc< td=""><td>24</td><td>3</td><td></td><td>57</td><td>70</td><td>460</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	24	3		57	70	460								
N9.0 E5.0		33		1 < L			419								
N9.0 E6.0		-4		0 < L		31	416								
N9.0 E7.0	<lc< td=""><td>-4 -4</td><td>1</td><td>0 -</td><td></td><td>40</td><td>446</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-4 -4	1	0 -		40	446								
N9.0 E8.0	<lc< td=""><td></td><td></td><td>1</td><td></td><td>18</td><td>454</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>			1		18	454								
N9.0 E9.0		33		9 < L		78	440								
N9.5 E-0.5	<lc< td=""><td>2</td><td></td><td>2 <l< td=""><td></td><td>33</td><td>457</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td></l<></td></lc<>	2		2 <l< td=""><td></td><td>33</td><td>457</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td></l<>		33	457								<u> </u>
N9.5 E-1.5		20		0 < L		07	439					<u> </u>			
N9.5 E0.5	<lc< td=""><td>28</td><td></td><td></td><td></td><td>27</td><td>429</td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td><td>_ </td><td></td></lc<>	28				27	429					<u> </u>		_ 	
N9.5 E1.5	<lc< td=""><td>-18</td><td></td><td></td><td>·</td><td>19</td><td></td><td><lc< td=""><td></td><td>2</td><td>- 6</td><td><lc< td=""><td></td><td>4</td><td></td></lc<></td></lc<></td></lc<>	-18			·	19		<lc< td=""><td></td><td>2</td><td>- 6</td><td><lc< td=""><td></td><td>4</td><td></td></lc<></td></lc<>		2	- 6	<lc< td=""><td></td><td>4</td><td></td></lc<>		4	
N9.5 E10.5		37		4		28	475					1			
N9.5 E11.5	<lc< td=""><td>9</td><td></td><td>3</td><td></td><td>41</td><td>454</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	9		3		41	454								
N9.5 E12.5	<lc< td=""><td>C</td><td></td><td>0 <l< td=""><td></td><td>62</td><td>489</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<></td></lc<>	C		0 <l< td=""><td></td><td>62</td><td>489</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></l<>		62	489								
N9.5 E13.5		46		7		94	46								
N9.5 E14.5	<lc< td=""><td>ç</td><td></td><td>3 <l< td=""><td></td><td>54</td><td>43</td><td></td><td></td><td>_</td><td></td><td></td><td></td><td></td><td></td></l<></td></lc<>	ç		3 <l< td=""><td></td><td>54</td><td>43</td><td></td><td></td><td>_</td><td></td><td></td><td></td><td></td><td></td></l<>		54	43			_					
N9.5 E15.5	<lc< td=""><td>-18</td><td></td><td>30 <l< td=""><td>.C</td><td>102</td><td>47</td><td></td><td></td><td>5</td><td></td><td>3 <lc< td=""><td></td><td>25</td><td></td></lc<></td></l<></td></lc<>	-18		30 <l< td=""><td>.C</td><td>102</td><td>47</td><td></td><td></td><td>5</td><td></td><td>3 <lc< td=""><td></td><td>25</td><td></td></lc<></td></l<>	.C	102	47			5		3 <lc< td=""><td></td><td>25</td><td></td></lc<>		25	
N9.5 E16.5	<lc< td=""><td>(</td><td></td><td>10</td><td></td><td></td><td>54</td><td></td><td></td><td>一十</td><td>· · · · · · · · · · · · · · · · · · ·</td><td></td><td></td><td></td><td></td></lc<>	(10			54			一十	· · · · · · · · · · · · · · · · · · ·				
N9.5 E17.5	<lc< td=""><td>-9</td><td></td><td>35</td><td></td><td>51</td><td></td><td>-</td><td></td><td>一十</td><td></td><td></td><td></td><td></td><td></td></lc<>	-9		35		51		-		一十					
N9.5 E18.5		NA	NA	_#_	NA_		NA	-							
N9.5 E19.5		NA	NA		NA		NA 43			-+					
N9.5 E2.5	<lc< td=""><td>(</td><td>9</td><td>43 < l</td><td></td><td>107</td><td>43</td><td>- -</td><td></td><td>\dashv</td><td></td><td></td><td></td><td></td><td></td></lc<>	(9	43 < l		107	43	- -		\dashv					
N9.5 E20.5	1	NA	NA		NA_		NA	-				1			
N9.5 E21.5	_ _	NA	NA		NA		NA E	2 1 2		-1		0 <lc< td=""><td></td><td>38</td><td></td></lc<>		38	
N9.5 E3.5	<lc< td=""><td></td><td>9</td><td>43</td><td>11</td><td>098</td><td>54</td><td>3 <lc< td=""><td></td><td></td><td></td><td><u>- 11</u></td><td></td><td></td><td></td></lc<></td></lc<>		9	43	11	098	54	3 <lc< td=""><td></td><td></td><td></td><td><u>- 11</u></td><td></td><td></td><td></td></lc<>				<u>- 11</u>			

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

-		DIDEAT				TRANSFERABLE						
		DIRECT	DET.	A-GAMMA/10	00 SO CM			BETA-GAMMA/				
	ALPHA/100		REIA		ISTD	SMPL	ISTD	SMPL	STD			
LOCATION/ITEM	SMPL	STD		SMPL DPM	DEV	DPM	DEV	DPM	DEV			
COORDINATES	DPM	DEV	-1-	187								
N9.5 E4.5	<lc -9<="" td=""><td></td><td><lc< td=""><td>161</td><td>445</td><td></td><td></td><td></td><td></td></lc<></td></lc>		<lc< td=""><td>161</td><td>445</td><td></td><td></td><td></td><td></td></lc<>	161	445							
N9.5 E5.5	<lc 0<="" td=""><td></td><td><lc< td=""><td>241</td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc>		<lc< td=""><td>241</td><td></td><td></td><td></td><td></td><td></td></lc<>	241								
N9.5 E6.5	<lc -9<="" td=""><td></td><td><lc< td=""><td>187</td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc>		<lc< td=""><td>187</td><td></td><td></td><td></td><td></td><td></td></lc<>	187								
N9.5 E7.5	<lc 18<="" td=""><td></td><td><lc< td=""><td>214</td><td></td><td>*</td><td></td><td></td><td></td></lc<></td></lc>		<lc< td=""><td>214</td><td></td><td>*</td><td></td><td></td><td></td></lc<>	214		*						
N9.5 E8.5	<lc -28<="" td=""><td></td><td><lc< td=""><td>54</td><td></td><td></td><td>1</td><td></td><td></td></lc<></td></lc>		<lc< td=""><td>54</td><td></td><td></td><td>1</td><td></td><td></td></lc<>	54			1					
N9.5 E9.5	<lc c<="" td=""><td>.40</td><td><lc< td=""><td></td><td>1 400</td><td>1</td><td></td><td></td><td></td></lc<></td></lc>	.40	<lc< td=""><td></td><td>1 400</td><td>1</td><td></td><td></td><td></td></lc<>		1 400	1						

Bliss and Laughlin Steel Characterization Survey of Elevated Locations in the Special Finishing Area Identified by Floor Monitor Scans

							7044	OFF BARLS					
		DIRECT			00 SO CM	A1 PF		SQ CM	BETA-GAMMA/100 SQ CM				
	ALPHA/100		RFI	A-GAMMA/1		SM		STD		SMPL	STD		
LOCATION/ITEM	SMPL	STD		SMPL	STD	DF		DEV		DPM I	DEV		
COORDINATES	DPM	DEV	L	DPM	DEV	Ur	5		<lc< td=""><td>12</td><td>76</td></lc<>	12	76		
N 3.7 E 9.35	15	26	L/	42270	2126		224	50		1734	181		
N 7.6 E 8.1	3165	335		135430	3755		72	28		258	98		
N 8.1 E 7.2	181	81		280257	5384		17	14	1	152	89		
N 8.5 E 6.7	1129	200		29019	1776	<u> </u>		16		184	92		
N 6.7 E 5.7	42	41		7 17213	1393		23		<lc< td=""><td>33</td><td>78</td></lc<>	33	78		
N 8.2 E 0.1	98	60	13	218953		<lc< td=""><td>0</td><td>0</td><td></td><td>33</td><td>78</td></lc<>	0	0		33	78		
1, 0.2	15	26		14777	1300	<lc< td=""><td>0</td><td>0</td><td><lc< td=""><td>25</td><td>77</td></lc<></td></lc<>	0	0	<lc< td=""><td>25</td><td>77</td></lc<>	25	77		
N 8.3 E 0.9	33	36		55387	2422	<lc_< td=""><td>0</td><td>0</td><td><lc< td=""><td></td><td>77</td></lc<></td></lc_<>	0	0	<lc< td=""><td></td><td>77</td></lc<>		77		
N 4.8 E 11	88	57	1	71985	2752		2	6	<lc< td=""><td>20</td><td>73</td></lc<>	20	73		
N 4.5 E 16.5	 	19	1	6559	919		2	6	<lc< td=""><td>-12</td><td>/3</td></lc<>	-12	/3		
N 3.4 E 17	<lc 6<="" td=""><td>1</td><td><u> </u></td><td>\ </td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc>	1	<u> </u>	\ 									

Lc indicates less than the critical level of activity which can be said to be above background.
A negative value is the calculated result of a reading which is below the instrument-specific background.

Bliss Laughlin Steel Characterization Area in Grid E16, 5-point Survey

		DUDECT			·		FERABLE			
	11 DU 14 (400 C	DIRECT	BETA-GAMMA/1	00 SQ CM	ALPHA/100 SQ CM				V100 SQ CN	
00000000000000000000000000000000000000	ALPHA/100 S	STD	SMPL	STD	SMPL		STD	SMI	ľ	STD
LOCATION/ITEM	SMPL	DEV	DPM	DEV	DPM		DEV	DP	M	DEV
COORDINATES	DPM	26	562	478						
10 E3	15	32	589	481				<u> </u>		
11 E3	24	41	562	478						
12 E3	42		669	489						
10.5 E 3.5	24	32		436						
V 1.5 E 3.5	42	41	<lc 187<br="">1526</lc>	572		5	8	<lc< td=""><td>25</td><td>77</td></lc<>	25	77
10 E4	24	32	3641	738		2	6	<lc< td=""><td>37</td><td>78</td></lc<>	37	78
V1 E4	15		402	460						
12 E4	<lc 6<="" td=""><td>19</td><td>642</td><td>487</td><td> </td><td></td><td></td><td></td><td></td><td></td></lc>	19	642	487	 					
N 0.5 E 4.5	<lc 6<="" td=""><td>19</td><td></td><td>451</td><td>1</td><td></td><td></td><td></td><td></td><td>· .</td></lc>	19		451	1					· .
N 1.5 E 4.5	15		200	522	<lc< td=""><td>0</td><td>1 0</td><td><lc< td=""><td>33</td><td>78</td></lc<></td></lc<>	0	1 0	<lc< td=""><td>33</td><td>78</td></lc<>	33	78
NO E5	52		1	481	+					
N1 E5	42		589	543	<lc< td=""><td>0</td><td>1 0</td><td><lc< td=""><td>12</td><td>76</td></lc<></td></lc<>	0	1 0	<lc< td=""><td>12</td><td>76</td></lc<>	12	76
N2 E5	24			517		0	1 0	<lc< td=""><td>0</td><td>74</td></lc<>	0	74
QC	33	36	937	317	1720	<u>~</u>	<u> </u>	Щ		

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

Appendix B COST ESTIMATE

Bliss & Laughlin Cost Estimate Alternative 2 Institutional Controls Cost in FY1998\$

				-	mal Lost
			d Cad		ADV4H
HPI Element	<u>Krimita</u>	(51	Y98)	74.5	Constantoncy)-
		\$	302,537	\$	347,917
XX	Bliss & Laughlin Project	Š		\$	-
XX	Studies and Design	\$	-	\$	
XXX	Htrw Construction Activities	Š		\$	-
1XX	Htrw Remedial Action (Construction)	\$		\$	
1XX01	Mobilization And Preparatory Work	Š	-	\$	-
1XX02	Monitoring, Sampling, Testing, And Analysis	\$	-	\$	-
1XX0201	RA	\$	-	\$	-
1XX0202	Exc/Transp	S	-	\$	-
1XX03	Site Work	S	-	\$	
1XX0301	Site Work - Preliminary	\$		\$	-
31XX0302	Site Work - Sustaining	S	-	\$	
31XX04	On Cum Removal And Destruction	S		\$	
31XX05	Surface Water Collection And Control	\$		\$	
1XX06	Croundwater Collection And Control	S		\$	
31XX07	Air Pollution/Gas Collection And Control	Ś		\$	
31XX08	Solids Collection And Containment	\$	-	\$	
31XX0801	Excavation	\$		\$	
31XX0802	Backfill	\$	-	\$	
31XX09	Liquids/Sediments/Sludges Collection And Containment	\$	-	\$	
31XX10	Drums/Tanks/Structures/Misc Demolition And Removal	\$		\$	
31XX11	Biological Treatment	\$		\$	
31XX12	Chemical Treatment	\$		\$	
31XX13	Physical Treatment	S	-	\$	
31XX14	Thermal Treatment	S	-	\$	
31XX15	Stabilization/Fixation/Encapsulation	Š	-	\$	
31XX16	(Reserved For Future Use)	S	-	\$	
31XX17	Decontamination And Decommissioning (D&D)	5	-	\$	
31XX18	Disposal (Other Than Commercial)	\$	-	\$	
31XX1801	Transportation to Storage/Disposal Facility	\$	-	\$	
31XX1802	Disposal Fees and Taxes	\$	-	\$	
31XX19	Disposal (Commercial)	\$		\$	
31XX1901	Transportation to Storage/Disposal Facility	\$		\$	
31XX1902	Disposal Fees and Taxes	\$	-	\$	
31XX20	Site Restoration	\$		\$	
31XX21	Demobilization	S		\$	
31XX22	General Requirements (Optional Breakout)	\$	-	\$	
31XX2201	Supervision, Management & Administration	\$		\$	
31XX2202	ICSM RA	\$		\$	
31XX9X	Other (Use Numbers 90-99)	S		\$	
332XX	Construction (Edc)	Š		\$	
33XX	Supervision & Admin (S&A) (Construction Management)	<u> \$</u>	302,537	\$	347,9
34XXX		\$	302,537		347,9
342XX	THE PARTICULAR AND MAINTENANCE (FOST CONSTRUCTION)	\$	88,599		101,8
342XX01	MONITORING, SAMPLING, TESTING, AND ANALYSIS	\$	191,520	\$	220,2
342XX02	ICSM O&M	1 \$	22,418		25,7
342XX03	Project Management Supervision & Admin (S&A) (Construction Management)	- \$		- S	

Contingency is a standard 15% unless otherwise noted.

Bliss & Laughlin Cost Estimate Alternative 3 Building Decontamination Cost in FY1998\$

					ntal Cost
			GI Cost		(SFY98)
WIII Liement			gr.v.081	(147)	Constaurance
		\$	305,664		351,514
3XXX	IBliss and Laughlin Project	\$	- 3		
32XX	Studies and Design	\$	290,437		334,003
33XXX	Htrw Construction Activities	\$		<u> </u>	303,639
331XX	Htrw Remedial Action (Construction)	\$		\$	5,439
331XX01	Mobilization And Preparatory Work	\$	1070.11	<u> </u>	17,307
331XX02		\$		\$	16,997
331XX0201	RA	\$		\$	309
331XX0202	Exc/Transp	\$		<u>\$</u>	68,143
331XX03	Site Work	\$		\$	57,500
331XX0301	Site Work - Preliminary	\$		\$	10,643
331XX0302	Site Work - Sustaining	\$		\$	
331XX04	Oe-Cwm Removal And Destruction	\$	-	\$	
331XX05	Surface Water Collection And Control	\$	-	\$	·
331XX06	Groundwater Collection And Control	\$		\$	
331XX07	Air Pollution/Gas Collection And Control	\$	-	\$	
331XX08	Solids Collection And Containment	\$	-	\$	-
331XX0801	Excavation	\$	-	\$	
331XX0802	Backfill Liquids/Sediments/Sludges Collection And Containment	\$	-	\$	
331XX09	Drums/Tanks/Structures/Misc Demolition And Removal	\$	-	\$	
331XX10	Drums/Tanks/Structures/Misc Demonds/// 413	\$	-	\$	
331XX11	Biological Treatment	\$	-	\$	
331XX12	Chemical Treatment	\$	-	\$	
331XX13	Physical Treatment	\$		\$	
331XX14	Thermal Treatment	\$		\$	
331XX15	Stabilization/Fixation/Encapsulation	\$		\$	4,296
331XX16	(Reserved For Future Use) Decontamination And Decommissioning (D&D)	\$	3,736	\$	4,290
331XX17	Decontamination And Decontinussioning (5.55)	\$		\$	
331XX18	Disposal (Other Than Commercial)	\$		\$	
331XX1801	Transportation to Storage/Disposal Facility	\$	-	\$	6,186
331XX1802	Disposal Fees and Taxes	\$	5,379	\$	2,253
331XX19	Disposal (Commercial)	\$	1,959	\$	3,933
331XX1901	Transportation to Storage/Disposal Facility	\$	3,420	\$	3,900
331XX1902	Disposal Fees and Taxes	\$	-	\$	5,180
331XX20	Site Restoration	\$	4,504	\$	67,754
331XX21	Demobilization General Requirements (Optional Breakout)	\$	58,917	\$	66,531
331XX22	Supervision, Management & Administration	\$	57,853		1,224
331XX2201	Supervision, Management & Administration	\$	1,064		129,334
331XX2202	ICSM RA	\$	112,464		123,007
331XX9X	Other (Use Numbers 90-99)	\$	-	\$	30.364
332XX	Engineering During Construction (Edc) Supervision & Admin (S&A) (Construction Management)	\$	26,403		17,511
333XX		\$	15,227	_	15,919
34XXX	HTRW (POST CONSTRUCTION) HTRW OPERATION AND MAINTENANCE (POST CONSTR	U \$	13,843		4.249
342XX	MONITORING, SAMPLING, TESTING, AND ANALYSIS		3,695		612
342XX01	MONITURING, SAMPLING, TESTITO,	\$	532		11,058
342XX02	ICSM O&M	\$	9,615		1,59
342XX03	Project Management Supervision & Admin (S&A) (Construction Management)	5	1,384	\$	1,39

Contingency is a standard 15% unless otherwise noted.

This Appendix is not available in electronic format. Contact Wendee Ryan to request a copy.